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# PERFORMANCE OF A TRANSONIC FAN STAGE DESIGNED FOR A LOW MERIDIONAL VELOCITY RATIO

by Royce D. Moore, George W. Lewis, Jr., and Walter M. Osborn

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#### SUMMARY

This report presents both the aerodynamic design parameters and the performance of a transonic fan stage having a meridional velocity ratio of 0.8 across the tip of the stage. The stage was designed for a pressure ratio of 1.57 at a flow of 29.5 kilograms per second and a tip speed of 426 meters per second. Detailed radial surveys were obtained over the stable operating range from 50 to 100 percent of design speed.

The stage peak efficiency (0.81) at design speed occurred at a pressure ratio of 1.58 and a flow of 28.7 kilograms per second. The stage stall margin was 11 percent, based on conditions at peak efficiency and stall. Rotor peak efficiency (0.84) occurred at a pressure ratio of 1.61 and the same flow as stage peak efficiency.

#### INTRODUCTION

The axial-flow fan and compressor research program for advanced airbreathing engines being conducted at Lewis is primarily directed toward reducing the size and weight of fans and compressors while maintaining high levels of performance. In support of this objective, experimental studies are being conducted to evaluate the effects of blade solidity, blade aspect ratio, blade loading, area margin above choke, blade airfoil shape, weight flow per unit annulus area, velocity ratio, and blade spacing on efficiency and flow range. The aerodynamic performance of the axial-flow fan stage designed for a stage tip velocity ratio of 0.8 is presented herein. Performance of a similar stage having a tip meridional velocity ratio of 1.0 was reported in reference 1. The velocity ratio was varied by changing the stage tip contour while maintaining the same hub contour. Both stages were designed for a pressure ratio of 1.57 and a tip speed of 425 meters per second. This report presents the aerodynamic design parameters and the overall and blade-element performance. Data were obtained at a near-stall point for six rotative speeds from 50 to 100 percent of design speed and over the stable operating

range of 70, 90, and 100 percent of design speed.

Blade-element data were obtained for the rotor and the stator at 11 radial positions. The stage discussed in this report has been designated stage 20-17 (rotor 20 and stator 17). The data in this report are presented in tabular and in machine-plotted form. The symbols and equations are given in appendixes A and B, and the definitions and units used for the tabular data are presented in appendix C.

#### AERODYNAMIC DESIGN

Three computer programs (refs. 2 and 3) were used to design this compressor stage: the streamline analysis program, the blade geometry program, and the blade coordinate program. Only a brief description of each is presented herein.

The streamline-analysis program was used to calculate the flow-field parameters at several axial locations, including planes approximating the blade leading and trailing edges for both the rotor and stator. The weight flow, rotative speed, flow path geometry, and radial distributions of total pressure are inputs in this program. Total loss, which is calculated within the program, is based on a calculated shock loss and a profile loss. Profile loss as a function of diffusion factor and radial position is an input. The program accounts for both streamline curvature and entropy gradients; boundary-layer blockage factors are also included.

The distribution of velocity vector, total pressure, and total temperature calculated in the streamline-analysis program are used in the blade-geometry program to compute blade-geometry parameters. The blade-geometry parameters are used in the blade coordinate program (ref. 4) to compute blade elements on conical surfaces passing through the blade. The blade elements are then stacked on a line passing through their centers of gravity, and Cartesian blade coordinates, which are used directly in fabrication, are computed.

The overall design parameters for stage 20-17 are listed in table I, and the flow path is shown in figure 1. This stage was designed for an overall pressure ratio of 1.57 at a weight flow of 29.5 kilograms per second (196.4 kg/sec/m<sup>2</sup> of annulus area). The design tip speed was 426 meters per second. The inlet relative Mach number is 1.4 at the rotor tip. Since the stage was designed for a tip solidity of 1.3 for both rotor and stator, the rotor had 44 blades with an aspect ratio of 2.5, and the stator had 48 blades with an aspect ratio of 2.4.

The blade-element design parameters for rotor 20 are presented in table II. This rotor was designed for a radially constant total-pressure ratio of 1.60. The stator blade-element design parameters are given in table III. The blade geometry is presented in table IV for rotor 20 and in table V for stator 17. Both the rotor and stator used multiple-circular-arc blade shapes.

#### APPARATUS AND PROCEDURE

#### Compressor Test Facility

The compressor stage was tested in the Lewis single-stage compressor facility (described in detail in ref. 4 and shown in fig. 2 herein). Atmospheric air enters the test facility at an inlet on the roof of the building and flows through the flow measuring orifice and into the plenum chamber upstream of the test stage. It then passes through the experimental compressor stage and into the collector from which it is exhausted to the atmosphere.

#### **Test Stage**

Photographs of the rotor and stator are shown in figures 3 and 4. Each rotor blade has a vibration damper located at about 57 percent of span from the outlet rotor tip. The maximum thickness of the damper was 0.215 centimeter. The radial tip clearance of the rotor was a nominal 0.050 centimeter at ambient, nonrotating conditions. The axial spacing between the rotor hub trailing edge and the stator hub leading edge was 3.428 centimeters, to provide for instrumentation between rotor and stator.

#### Instrumentation

The compressor weight flow rate was measured using a calibrated thin-plate orifice. The orifice temperature was determined from an average of two Chromel/constantan thermocouples. Orifice pressures were measured by calibrated transducers.

Radial surveys of the flow were made upstream of the rotor, between the rotor and stator, and downstream of the stator (fig. 1). Photographs of the survey probes are shown in figure 5. Total pressure, total temperature, and flow angle were measured with the combination probe (fig. 5(a)), and the static pressure was measured with an 8° C-shaped wedge probe (fig. 5(b)). Each probe was positioned with a null-balancing, stream-directional-sensitive control system that automatically alined the probe to the direction of flow. The thermocouple was Chromel/constantan. The probes were alined in an air-calibration tunnel. Two combination probes and two wedge static probes were used at each of the three measuring stations.

Inner- and outer-wall static-pressure taps were located at the same axial stations as the survey probes. The circumferential locations of both types of survey probes and of the inner- and outer-wall static-pressure taps are shown in figure 6. The combination probe downstream of the stator (station 3) traversed circumferentially one stator

blade passage (7.5°) counterclockwise from the nominal value shown. An electronic speed counter, in conjunction with a magnetic pickup, measured rotative speed (rpm). Strain gages mounted on both the rotor and stator blades monitored stresses and vibrations. The estimated errors of the data based on inherent accuracies of the instrumentation and recording system are as follows:

Weight flow, kg/sec			•	•		•	•		•		•		•	•	•	•	•	•	•	•	•	. ±0.3
Rotative speed, rpm									•	•	•	•	•	•	•	•	•	•			•	. ±30
Flow angle, deg							•	•		•	•	•	•	•	•		•	•	•	•	•	±1
Temperature, K																						
Rotor-inlet total pressure, N/cm <sup>2</sup> .																		*:				±0.01
Rotor-outlet total pressure, N/cm <sup>2</sup> .																						
Stator-outlet total pressure, N/cm <sup>2</sup>																						
Rotor-inlet static pressure, N/cm <sup>2</sup>																						±0.04
Rotor-outlet static pressure, N/cm <sup>2</sup>																						±0.07
Stator-outlet static pressure, N/cm <sup>2</sup>	,																					±0.07

An indication of the consistency of the data can be observed by comparing the integrated weight flows at each measuring station with the orifice weight flow in table VI.

#### **Test Procedure**

The stage survey data were taken over a range of weight flows from maximum flow to the near stall. At 70, 90, and 100 percent of design speed, radial surveys were taken at five weight flows. At 50, 60, and 80 percent of design speed, radial surveys were taken for the near-stall weight flow only. Data were recorded at 11 radial positions for each speed and weight flow.

At each radial position the combination probe behind the stator was traversed circumferentially to nine locations across the stator gap. The wedge probe was set at midgap because previous studies showed that the static pressure across the stator gap was constant. The pressure, temperature, and flow angle were recorded at each circumferential position. At the last circumferential position pressure, temperature, and flow angle were also recorded at stations 1 and 2. All probes were then traversed to the next radial position, and the circumferential traverse procedure was repeated.

At each of the six rotative speeds the back pressure on the stage was increased by closing the sleeve valve in the collector until a stall was indicated by a sudden drop in stage-outlet total pressure. This pressure was measured by a probe at midpassage and was recorded on an X-Y plotter. Stall was corroborated by large increases in the blade stresses on both rotor and stator along with a sudden increase in noise.

#### Calculation Procedure

The measured total temperatures and pressures were corrected for Mach number and streamline slope. These corrections were based on the instrument probe calibrations given in reference 5. The stream static pressures were corrected for Mach number and streamline slope based on an average calibration for the wedge probes used.

Because of the physical construction of the C-shaped static-pressure wedges, it was not possible to obtain static-pressure measurements at 5, 10, and 95 percent of span. The static pressure at 95 percent span was obtained by assuming a linear variation in static pressure between the values at the inner wall and the probe measurement at 90 percent span. A similar variation was assumed between the static-pressure measurements at the outer wall and the 30 percent span to obtain the static pressure at 5 and 10 percent span.

At each radial position for station 3, averaged values of the nine circumferential measurements of pressure, temperature, and flow angle were obtained. The nine total temperatures were mass averaged to obtain the stator-outlet total temperature. The nine total pressures were energy averaged (i. e., converted to their enthalpy equivalent and then mass-averaged). The measured pressures, temperatures, and flow angles were used to calculate axial and tangential velocities at each circumferential position. Mass averages of these velocities were used to calculate the flow angles at each radial position presented herein. To obtain the overall performance, the radial values of total temperatures were mass-averaged, and radial values of total pressures were energy-averaged. At each measuring station, the integrated weight flow was computed based on the survey data. The data, measured at the three measuring stations, were translated to the blade leading and trailing edges by the method presented in reference 4.

The weight flow at stall was obtained in the following manner: During operation at near-stall, the sleeve valve was closed in small decrements. After each decrement the weight flow was obtained. The weight flow obtained just before stall occurred is called the stall weight flow. The pressure ratio at stall was obtained by extrapolating the total pressure obtained from the survey data to the stall weight flow.

Orifice weight flow, total pressures, static pressures, and temperatures were all corrected to sea-level conditions based on the rotor inlet conditions.

#### RESULTS AND DISCUSSION

The results from this investigation will be presented in three main sections. The overall performances for the rotor and the stage are given first. Radial distributions of several performance parameters are then presented for the rotor and stator followed by the blade-element data. Because the data presented are machine plotted, an oc-

casional point will be omitted because it falls outside the range of the parameters shown in the figure. A brief comparison of these results and those from a high-velocity ratio stage is included. The plotted data, together with some additional performance parameters, are also tabulated: The overall performance data are given in table VI; and the blade-element data are presented for the rotor in table VII and for the stator in table VIII. The definitions and units used in the tables are listed in appendix C.

#### Overall Performance

The overall performance for rotor 20 and for stage 20-17 are presented in figures 7 and 8 for speeds from 50 to 100 percent of design. Design-point values are shown as solid symbols in both figures. The stall line (dashed line) shown in figure 8 was determined using the method discussed in the section Calculation Procedure.

Rotor. - The design-speed peak efficiency for rotor 20 was 0.838, which occurred at a weight flow of 28.7 kilograms per second. Although the pressure ratio at peak efficiency was only slightly greater than the design value, it occurred at a flow less than the design value. At 70 percent of design speed, efficiencies up to 0.87 were obtained for this rotor.

Stage. - At design speed the stage peak efficiency of 0,813 occurred at the same weight flow as peak efficiency for the rotor. The measured pressure ratio (1.582) was slightly higher than the design value (1.574). And the calculated stall margin was approximately 11 percent based on conditions at stall and peak efficiency. At the lower speeds efficiencies ranged up to 0.84.

#### Radial Distributions

The radial distributions of several parameters are presented for design speed in figure 9 for rotor 20 and in figure 10 for stator 17. The data are presented for three weight flows: maximum flow, peak efficiency, and near stall. The design values are shown by the solid symbols. A line is faired through the peak efficiency data. Temperature-rise efficiency, temperature ratio, pressure ratio, suction-surface incidence angle, meridional velocity ratio, deviation angle, total loss parameter, total loss coefficient, and diffusion factor are presented as functions of percent span from the blade tip.

Rotor. - As the weight flow was reduced, the pressure ratio and temperature ratio increased across the entire rotor blade span with the larger increases occurring in the tip region. The blade loading (diffusion factor) also continued to increase with decreasing weight flow. The effect of the damper (57 percent span) on efficiency is evident at

all three weights.

At the peak efficiency weight flow of 28.7 kilograms per second, the pressure ratio was greater than design from the tip to 50 percent span and was less than design from there to the hub. The efficiency shows a large deviation from design from the region of the damper to the hub. There is a radial shift in the flow toward the blade tip with higher than design meridional velocity ratios from the tip to 30 percent span.

Stator. - At the peak efficiency condition the stator deviation angles were essentially equal to design except in the hub and tip regions. In the stator hub region, there was a large increase in losses from the 90 to 95 percent span indicating probable separation. This occurred at all three flows. The losses in the tip region were significantly greater that design.

#### Variation with Incidence Angle

The variation of selected rotor and stator blade-element performance parameters with incidence angle are presented in figures 11 and 12. The data are presented for 70, 90, and 100 percent of design speed at blade elements located at 5, 10, 30, 50, 70, 90, and 95 percent spans. Design values are shown by solid symbols.

Rotor. - The rotor blade elements were designed for a suction surface incidence angle of zero. At the design incidence angle the pressure ratio was higher than design at 5, 10, and 30 percent spans apparently because the flow turns more in these regions as indicated by the less-than-design deviation angles. At 50 percent span the pressure ratio and deviation angles are equal to design values. At 70, 90, and 95 percent span the blades under turned the flow (higher than design deviation angles); therefore the pressure ratio was less than design.

At 5 and 10 percent span the minimum loss incidence angle was not defined. At 30 percent span the minimum loss was approximately equal to design; however, it occurred at less than design incidence angle. At 50, 70, and 90 percent span minimum loss occurred near design incidence angle of zero; however, the values were significantly greater than design values. At 95 percent span minimum loss occurred at a greater than design incidence angle and its value was also greater than design.

Stators. - Except at the 5 and 95 percent span locations, minimum losses were equal to or less than design and generally occurred at negative incidence angles. At the 5 percent span location, there were high losses and deviation angles over the incidence angle range. At the 10 and 95 percent span, there was an increase in losses at the low incidence angles. Deviation angles exceeded design values at 5, 10, 90, and 95 percent span locations.

#### Comparison with Higher-Velocity-Ratio Stage

The performance of stage 20-17 may be compared with that of stage 11-4 of reference 1, which had a velocity ratio of 1.0 across the stage tip. The velocity ratio was reduced to 0.8 in stage 20-17 by changing the outer flow path contour while keeping the same inner flow path contour. The radial distribution of blade solidity, blade chord, leading and trailing edge thicknesses, maximum thickness, X-factors, and rotor blade minimum area ratios were held constant between the stages. The axial locations of the transition point and maximum thickness were also held constant. The stages were designed for a pressure ratio of 1.57 at a nominal specific flow of 198 kilograms per second per square meter of annulus area and a nominal tip speed of 425 meters per second.

The change in stage tip meridional velocity ratio had very little effect on overall performance. At design speed and flow the stage efficiency was essentially the same for both stages. The pressure ratio was slightly higher for the stage with the 1.0 velocity ratio. The same changes were observed for the two rotors. The stall margin based on conditions at the peak efficiency point and the stall point for the 1.0 velocity ratio stage was 19 percent but was only 11 percent for the 0.8 velocity ratio stage. However, if stall margin is based on conditions at the design flow point and stall point, both stages would have a stall margin of 19 percent, and the efficiency for the 0.8 velocity ratio stage would be less than 0.5 percentage point below its peak value.

#### SUMMARY OF RESULTS

This report presents both the aerodynamic design parameters and the performance of a transonic fan stage having a meridional velocity ratio of 0.8 across the stage tip. This stage was designed for a pressure ratio of 1.57 at a flow of 29.5 kilograms per second and a tip speed of 426 meters per second. Detailed radial surveys of the flow conditions in front of the rotor, between the rotor and stator, and downstream of the stator were made over the stable operating flow range at rotative speeds from 50 to 100 percent of design speed. This investigation yielded the following principle results:

- 1. At design speed the stage peak efficiency of 0.81 occurred at a flow of 28.7 kilograms per second and a pressure ratio of 1.58. Stage stall margin was 11 percent based on the flow and pressure ratio at peak efficiency and stall.
- At design speed a rotor peak efficiency of 0.84 occurred at a pressure ratio of 1.61 and the same flow as for stage peak efficiency.
  - 3. At the design incidence angle the measured rotor pressure ratio in the tip re-

gion was higher than design as a result of more turning (deviation angles less than design). In the hub region there was less turning and lower pressure ratio.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, May 11, 1978,
505-04.

## APPENDIX A

## SYMBOLS

Aan	annulus area at rotor leading edge, m <sup>2</sup>
$\mathbf{A_f}$	front'd area at rotor leading edge, m <sup>2</sup>
c <sub>p</sub>	specific heat at constant pressure, 1004 J/kg-K
c	aerodynamic chord, cm
D	diffusion factor
i <sub>mc</sub>	mean incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, deg
iss	suction-surface incidence angle, angle between inlet air direction and iine tangent to blade suction surface at leading edge, deg
J	mechanical equivalent of heat
N	rotative speed, rpm
P	total pressure, N/cm <sup>2</sup>
p	static pressure, N/cm <sup>2</sup>
r	radius, cm
SM	stall margin
T	total temperature, K
U	wheel speed, m/sec
v	air velocity, m/sec
w	weight flow, kg/sec
z	axial distance referenced from rotor blade hub leading edge, cm
$\alpha_{\mathbf{c}}$	cone angle, deg
$\alpha_{\mathbf{s}}$	slope of streamline, deg
β	air angle, angle between air velocity and axial direction, deg
$\beta_{\mathbf{c}}^{\mathbf{c}}$	relative meridional air angle based on cone angle, arctan (tan $\beta_{\rm m}' \cos \alpha_{\rm c}/\alpha s \alpha_{\rm s}$ ), deg
γ	ratio of specific heats (1.40)

- o ratio of rotor-inlet total pressure to standard pressure of 10, 13 N/cm<sup>2</sup>
- $\delta^{0}$  deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, deg
- η efficiency
- θ ratio of rotor-inlet total temperature to standard temperature of 288, 2 K
- $\kappa_{me}$  angle between blade mean camber line and meridional plane, deg
- κ<sub>ss</sub> angle between the blade suction surface at leading edge and the meridional plane, deg
- σ solidity, ratio of chord to spacing
- $\overline{\omega}$  total-loss coefficient
- $\overline{\omega}_{p}$  profile-loss coefficient
- $\overline{\omega}_{s}$  shock-loss coefficient

#### Subscripts:

- ad adiabatic (temperature rise)
- id ideal
- LE blade leading edge
- m meridional direction
- mom momentum rise
- p polytropic
- ref reference
- TE blade trailing edge
- z axial direction
- θ tangential direction
- 1 instrumentation plane upstream of rotor
- 2 instrumentation plane between rotor and states:
- 3 instrumentation plane downstream of stator

#### Superscript:

relative to blade

#### APPENDIX B

#### **EQUATIONS**

Suction-surface incidence angle:

$$i_{ss} = (\beta_c^{\prime})_{LE} - \kappa_{ss}$$
 (B1)

Mean incidence angle:

$$i_{mc} = (\beta'_c)_{LE} - (\kappa_{mc})_{LE}$$
 (B2)

Deviation angle:

$$\delta^{O} = (\beta_{c}')_{TE} - (\kappa_{mc})_{TE}$$
 (B3)

Diffusion factor:

$$D = 1 - \frac{V_{TE}'}{V_{LE}'} + \left| \frac{(rV_{\theta})_{TE} - (rV_{\theta})_{LE}}{(r_{TE} + r_{LE})\sigma(V_{LE}')} \right|$$
(B4)

Total loss coefficient:

$$\overline{\omega} \approx \frac{(\mathbf{P'_{id}})_{TE} - \mathbf{P'_{TE}}}{\mathbf{P'_{LE}} - \mathbf{P_{LE}}}$$
(B5)

Profile loss coefficient:

$$\overline{\omega}_{\rm p} = \overline{\omega} - \overline{\omega}_{\rm S}$$
 (B6)

Total loss parameter:

$$\frac{\overline{\omega} \cos (\beta_{\mathbf{m}}^{'})_{\mathbf{TE}}}{2\sigma}$$
 (B7)

Profile-loss parameter:

$$\frac{\overline{\omega}_{\mathbf{p}} \cos (\beta'_{\mathbf{m}})_{\mathbf{TE}}}{2\sigma}$$
 (B8)

Adiabatic (temperature rise) efficiency:

$$\eta_{\text{ad}} = \frac{\left(\frac{\mathbf{P}_{\text{TE}}}{\mathbf{P}_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{\mathbf{T}_{\text{TE}}}{\mathbf{T}_{\text{LE}}} - 1} \tag{B9}$$

Momentum - rise efficiency:

$$\eta_{\text{mom}} = \frac{\left(\frac{\mathbf{P}_{\text{TE}}}{\mathbf{P}_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{(\mathbf{UV}_{\theta})_{\text{TE}} - (\mathbf{UV}_{\theta})_{\text{LE}}}{\mathbf{T}_{\text{LE}}gJC_{p}}}$$
(B10)

Equivalent weight flow:

$$\frac{\mathbf{w}\sqrt{\theta}}{\delta}$$
 (B11)

Equivalent rotative speed:

$$\frac{N}{\sqrt{\theta}}$$
 (B12)

Mass flow per unit annulus area;

$$\frac{\underline{\mathbf{w}}\sqrt{\theta}}{\delta}$$
Aan (B13)

Mass flow per unit frontal area:

$$\frac{W\sqrt{\theta}}{\frac{\delta}{A_f}}$$
 (B14)

Head-rise coefficient:

$$\frac{gJC_{\mathbf{p}}T_{\mathbf{LE}}}{U_{\mathbf{tip}}^{2}}\left[\left(\frac{P_{\mathbf{TE}}}{P_{\mathbf{LE}}}\right)^{(\gamma-1)/\gamma}-1\right]$$
(B15)

Flow coefficient:

$$\left(\frac{v_z}{v_{tip}}\right)_{LE}$$
 (B16)

Stall margin:

$$SM = \left[ \frac{\left(\frac{P_{TE}}{P_{LE}}\right)_{stall}}{\left(\frac{P_{TE}}{P_{LE}}\right)_{ref}} \times \frac{\left(\frac{w\sqrt{\theta}}{\delta}\right)_{ref}}{\left(\frac{w\sqrt{\theta}}{\delta}\right)_{stall}} - 1 \right] \times 100$$
(B17)

Polytropic efficiency:

$$\eta_{\mathbf{p}} = \frac{\ln\left(\frac{\mathbf{P}_{\mathbf{TE}}}{\mathbf{P}_{\mathbf{LE}}}\right)^{(\gamma-1)/\gamma}}{\ln\left(\frac{\mathbf{T}_{\mathbf{TE}}}{\mathbf{T}_{\mathbf{LE}}}\right)}$$
(B18)

#### APPENDIX C

#### DEFINITIONS AND UNITS USED IN TABLES

ABS absolute

AERO CHORD aerodynamic chord, cm

AREA RATIO ratio of actual flow area to critical area (where local Mach number

is one)

BETAM meridional air angle, deg

CONE ANGLE angle between axial direction and conical surface representing

blade element, deg

DELTA INC difference between mean camber blade angle and suction-surface

blade angle at leading edge, deg

DEV deviation angle (defined by eq. (B3)), deg

D-FACT diffusion factor (defined by eq. (B4))

EFF adiabatic efficiency (defined by eq. (B9))

IN inlet (leading edge of blade)

INCIDENCE incidence angle (suction surface defined by eq. (B1) and mean by

eq. (B2))

KIC angle between blade mean camber line at leading edge and merid-

ional plane, deg

KOC angle between blade mean camber line at trailing edge and merid-

ional plane, deg

KTC angle between blade mean camber line at transition point and me-

ridional plane, deg

LOSS COEFF loss coefficient (total defined by eq. (B5) and profile by eq. (B6))

LOSS PARAM loss parameter (total defined by eq. (B7) and profile by eq. (B8))

MERID meridional

MERID VEL R meridional velocity ratio

OUT outlet (trailing edge of blade)

PERCENT SPAN percent blade span from tip at rotor outlet

PHISS suction-surface camber ahead of assumed shock location, deg

PRESS pressure, N/cm<sup>2</sup>

PROF profile

RADII radius, cm

REL relative to blade

RI inlet radius (leading edge of blade), cm

RO outlet radius (trailing edge of blade), cm

RP radial position

RPM equivalent rotative speed, rpm

SETTING ANGLE angle between aerodynamic chord and meridional plane, deg

SOLIDITY ratio of aerodynamic chord to blade spacing

SPEED speed, m/sec

SS suction surface

STREAMLINE SLOPE slope of streamline, deg

TANG tangential

TEMP temperature, K

TI thickness of blade at leading edge, cm

TM thickness of blade at maximum thickness, cm

TO thickness of blade at trailing edge, cm

TOT total

TOTAL CAMBER difference between inlet and outlet blade mean camber line

angle, deg

VEL velocity, m/sec

WT FLOW equivalent weight flow, kg/sec

X FACTOR ratio of suction-surface camber ahead of assumed shock loca-

tion of multiple-circular-arc blade section to that of double

circular-arc blade section

ZIC axial distance from inlet to blade leading edge, cm

ZMC axial distance from inlet to blade maximum thickness point, cm

ZOC axial distance from inlet to blade trailing edge, cm

ZTC axial distance from inlet to transition point, cm

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## TABLE I. - DESIGN OVERALL PARAMETERS FOR STAGE 20-17

ROTOR	TOTA	AL.	PRE	SS	SE	RA	TI	٥.					1.601
STAGE													
ROTOR													
STAGE	TOT.	AL.	TEN	PE	147	L'RE	R	TI	٥.				. 1.163
ROTOR	AD I	13:	110	E	7	CIE	10	٧.					. 0.881
STAGE	AD !	B	TIC	5	7	CIE	No	٧.					0.847
ROTOR	POL	YTR	I PU	CE	FF	:::	EN.	.Y.					. 0.688
STAGE	POL	TR	CPI	0 8	FF	:01	EN.	٢.					. 0.856
ROTOR	HEAD	9 6	SISE	Ci	EF	FIC	IE	NT.					. 0.229
STACE	HEAD	9	RISE	C.	EF	FIC	IE!	٧.					. 0.220
FLON (	CEFF	-10	HEN	Τ.									0.449
NT FLO	A P	5	UN	7 7	30	174	L	SE	١.				146.843
NT FLO	A P	R	UNI	1 3	11.		5	SE	4.				196.411
HT FLO	. H												29.484
RPM .												16	100.000
													426.226

TABLE II. - DESIGN BLADE-ELEMENT PARAMETERS FOR ROTOR 20

	RAD	11		BETAM		BETAM		L TEMP		
RP	IN		IN	OUT		OUT	IN		IN	R1110
TIP	25.281	24.614	-0.	45.7 43.4		64.6	208.2	1.204	10.13	
2	24.156		0.	41.9		62.6		1.181	10.15	
3	21.813		õ.	40.8		58.1		1,164	10.13	
ī	19.385	19.601	٥.	42.0	58.9	51.8			10.13	
5	16.764	19.044	0.	42.5		49.8		1.155	10.13	1.601
6	16.451		0.	42.7	57.7	48.7	280.2		10.:3	
7	18.136		a.	43.0		47.5			10.13	
8			0.	43.2		46.3		1.154	10.13	1.661
9	16.651		0.	44.1		42.5			10.13	
10	14.130	14.568	0. 0.	47.7	51.8	27.1	200.2	1.154	10.13	1.60
HUB	12.700	14.031	٥.	50.6	49.4	15.3	288.2		10.13	
			•	30.0	-,,-		200.2			
	±8\$	VEL	REL	VEL	MERI	D VEL	TAN	S VEL	W-€EL	SPEED
RP.	IN	JUT	100	OUT	18		IN	DUT	18	
TIP		194.1	464.9		185.0			138.9	426.2	
1	166.4		45:.5		168.4			132.6		4:5.3
3	19:.9	193.0		311.8	193.9	143.7		128.9	40 3	405.0
4	136.9	224.9	416.8 581.6	240.1	196.3	152.3	3. 3.	128.6	3.6.8	368.0 333.5
	196.6	207.6	372.5	257.0	190.0	153.1		140.2	\$15.4	32:.1
ě	190.5	208.9	367.9	232.5	196.3	153.5		141.6	31:.1	
5	196.1	210.4	363.2	228.1	196.0	153.9		145.4	305.8	
	1:5.	211.9	359.5	225.7	195.7	154.4	0.	145.2	3::.4	327.:
÷	94.2	21 2	344.2	213.7	194.2	155.8	٥.	151.:	284.1	232.9
::	. 8.	255.7	503.3	179.0	187.7	158.5	٥.	174.4	250.2	255.5
11	65.	242.5			185.7		٥.	185.1	226.1	
H.8	185.6	249.9	282.2	164.5	183.8	158.6	٥.	195.1	214.1	250.0
		ACH NO		ACH NO			STREAM		MERID	PE4K SS
RP.	IN	JUT	IN	007	IN	DUT	IN	ou:	VEL R	MACH NO
TIP	1N 2.563	au1 a.555	IN 1.409	0.871	IN 0.563	0.575	-2.68	0U1 -1.59	VEL R	1.52d
TIP	2.563 0.572	0.535 0.535	1.409 1.388	0.07 0.871 0.873	IN 0.563 0.572	0.373 0.388	1N -2.68 -2.24	001 -1.59 -1.43	VEL R	1.526 1.519
TIP	1N 0.563 0.572 0.580	0.535 0.535 0.535	1N 1.409 1.588 1.366	0.871 0.875 0.867	IN 0.563	0.575 0.569 0.400	1N -2.68 -2.24	0U1 -1.59 -1.43 -1.14	VEL R 5.750 0.744 0.753	1.52¢ 1.519 1.510
11P	2.563 0.572	0.535 0.535	1.409 1.388	0.07 0.871 0.873	1N 0.563 0.572 0.580	0.575 0.569 0.400 0.419	1N -2.68 -2.24	001 -1.59 -1.43	VEL R 5.753 6.744 6.753 6.766 6.773	MACH 13 1.526 1.519 1.513 1.490 1.477
TIP 1 2 3 4 5	2N 0.563 0.572 0.580 0.597 0.599 0.598	3.535 0.535 0.535 0.51 3.553 0.578 0.587	1N 1.409 1.388 1.366 1.268 1.161 1.153	0.07 0.071 0.073 0.067 0.791	IN 0.563 0.572 0.580 0.597 0.599 0.598	0.373 0.368 0.400 0.419 0.430 0.435	1N -2.68 -2.24 -1.70 1.22 4.65 5.68	0UT -1.59 -1.43 -1.14 1.06 3.98 4.80	VEL R 0.750 0.744 0.760 0.760 0.773	MACH 13 1.526 1.519 1.513 1.490 1.477
TIP 1 2 3 4 5 6	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597	301 0.535 0.535 0.52 3.553 0.578 0.587	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119	0.07 0.671 0.667 0.667 0.695 0.670 0.658	IN 0.563 0.572 0.580 0.597 0.599 0.598 0.597	0.373 0.368 0.400 0.419 0.430 0.435 0.434	1N -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43	0UT -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23	VEL R 5.750 0.744 5.765 0.766 0.773 0.779	MACH 1.5 1.526 1.519 1.510 1.497 1.477 1.476 1.476
TIP 1 2 3 4 5 6	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597	0.535 0.535 0.535 0.52. 0.553 0.578 0.587 0.597	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105	0.07 0.871 0.873 0.867 0.791 0.695 0.670 0.658 0.646	1N 0.565 0.572 0.580 0.597 0.599 0.598 0.597 0.596	0.373 0.368 0.400 0.419 0.430 0.435 0.434	1N -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00	007 -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66	VEL R 0.750 0.744 0.765 0.766 0.775 0.779 0.782	MACH 13 1.526 1.519 1.510 1.493 1.477 1.476 1.476
TIP 1 2 3 4 5 6 7 8	IN 3.563 6.572 6.583 6.597 6.598 6.597 6.596 6.595	0.555 0.555 0.535 0.52. 0.553 0.578 0.587 0.591 0.596 0.600	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105	0UT 0.871 0.873 0.867 0.791 0.695 0.670 0.658 0.646 0.634	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.596	0.47 0.373 0.369 0.400 0.419 0.430 0.435 0.434 0.436	1N -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59	007 -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11	VEL R c. 750 c. 744 c. 755 c. 766 c. 773 c. 779 c. 782 c. 783 c. 789	MACH 13 1.526 1.519 1.510 1.493 1.477 1.476 1.476 1.476
TIP 1 2 3 4 5 6 7 8 9	IN 3.563 6.572 6.580 6.597 6.598 6.597 6.596 6.595	0.555 0.555 0.535 0.52. 0.553 0.578 0.587 0.591 0.596 0.600 0.616	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046	0.07 0.871 0.873 0.867 0.791 0.695 0.670 0.658 0.634 0.634	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.596 0.595	0.430 0.430 0.430 0.435 0.436 0.436 0.437 0.442	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47	007 -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54	VEL R 0.755 0.744 0.765 0.775 0.779 0.782 0.789 0.789	1.526 1.519 1.510 1.510 1.490 1.477 1.476 1.476 1.476 1.477
TIP 1 2 3 4 5 6 7 8 9 10	IN 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.596 0.590 0.590	0.535 0.535 0.535 0.52. 0.553 0.578 0.597 0.591 0.596 0.616 0.673	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105	0UT 0.871 0.873 0.867 0.791 0.695 0.670 0.658 0.646 0.634	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.596	0.47 0.373 0.389 0.400 0.419 0.430 0.434 0.435 0.434 0.437	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54	VEL R c. 750 c. 744 c. 755 c. 766 c. 773 c. 779 c. 782 c. 783 c. 789	1.526 1.519 1.510 1.510 1.490 1.477 1.476 1.476 1.476 1.477 1.481
TIP 1 2 3 4 5 6 7 8 9 10 11	IN 3.563 6.572 6.580 6.597 6.598 6.597 6.596 6.595	0.535 0.535 0.535 0.52. 0.553 0.578 0.597 0.591 0.696 0.605 0.616 0.675 0.694	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887	0UT 0.871 0.873 0.667 0.695 0.670 0.658 0.646 0.634 0.598 0.599 0.488	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.595 0.595 0.569	0.47 0.375 0.389 0.400 0.419 0.430 0.434 0.436 0.437 0.442 0.455	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47	007 -1.58 -1.43 -1.14 1.86 3.98 4.80 5.23 5.66 6.11 7.54 11.97	VEL R 0.755 0.744 0.765 0.766 0.775 0.769 0.769 0.769 0.684	1.526 1.519 1.510 1.490 1.477 1.476 1.476 1.476 1.476 1.476 1.477 1.481 1.403
TIP 1 2 3 4 5 6 7 8 9 10 11	1N 3.563 0.572 5.580 0.597 0.599 0.596 0.595 0.595 0.565 0.565	0.535 0.535 0.52. 0.553 0.578 0.597 0.591 0.600 0.616 0.673 0.694 0.717	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.671 0.673 0.667 0.791 0.695 0.670 0.658 0.634 0.596 0.486 0.472	1N 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.569	0.47 0.373 0.589 0.400 0.419 0.435 0.434 0.436 0.437 0.455 0.455	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24	VEL R 0.755 0.744 0.765 0.766 0.775 0.769 0.789 0.884 0.864 0.864	1.526 1.519 1.510 1.490 1.477 1.476 1.476 1.476 1.477 1.481 1.403 1.365 1.329
7 P 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.563 0.572 0.580 0.597 0.599 0.596 0.595 0.595 0.565 0.565 0.557	0.535 0.535 0.52. 0.553 0.578 0.597 0.591 0.600 0.616 0.673 0.694 0.717	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0UT 0.871 0.873 0.667 0.695 0.670 0.658 0.646 0.634 0.598 0.599 0.488	1N 0.563 0.572 0.580 0.597 0.599 0.598 0.597 0.595 0.595 0.569	0.47 0.373 0.589 0.400 0.419 0.435 0.434 0.436 0.437 0.455 0.455	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24	007 -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58	VEL R 0.755 0.744 0.765 0.765 0.779 0.782 0.789 0.802 0.844 0.854 0.865	MACH 1.5 1.526 1.519 1.510 1.490 1.477 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.328
TIP 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.565 0.565 0.557	0.535 0.535 0.535 0.52. 0.553 0.597 0.591 0.596 0.600 0.616 0.673 0.694 0.717	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.871 0.873 0.867 0.791 0.659 0.670 0.654 0.654 0.654 0.654 0.599 0.488 0.472	IN 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.569	0.47 0.373 0.589 0.400 0.419 0.435 0.434 0.436 0.437 0.442 0.455	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58	VEL R 0.755 0.744 0.765 0.775 0.779 0.789 0.882 0.884 0.864 0.865 LOSS P	MACH 1.5 1.526 1.519 1.510 1.490 1.477 1.476 1.476 1.477 1.481 1.405 1.365 1.328
TIP 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.563 0.572 0.580 0.597 0.599 0.596 0.595 0.595 0.565 0.565 0.557	0.535 0.535 0.535 0.52. 3.553 0.597 0.597 0.596 0.600 0.616 0.673 0.694 0.717	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.871 0.873 0.867 0.791 0.695 0.670 0.658 0.634 0.598 0.599 0.468 0.472	1N 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.569	0.01 0.373 0.368 0.400 0.419 0.433 0.434 0.436 0.437 0.442 0.455 0.454 0.455	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24	007 -1.59 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58	VEL R 0.755 0.744 0.765 0.765 0.779 0.782 0.789 0.802 0.844 0.854 0.865	MACH 1.5 1.526 1.519 1.510 1.490 1.477 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.328
TIP 2 3 4 5 6 7 8 9 10 11 HUB	IN 3.563 0.572 5.580 0.597 0.599 0.595 0.595 0.595 0.595 0.565 0.557	0.535 0.535 0.535 0.52. 3.553 0.597 0.596 0.600 0.616 0.673 0.694 0.717	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.873 0.867 0.667 0.695 0.670 0.658 0.654 0.598 0.599 0.488 0.472	IN 0.563 0.572 0.580 0.597 0.598 0.596 0.595 0.595 0.595 0.563 0.563 0.557	0.07 0.373 0.368 0.400 0.419 0.433 0.434 0.436 0.455 0.455 0.795 0.795	IN -2.68 -2.24 -1.73 1.22 4.65 5.68 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58	VEL R 0.755 0.744 0.765 0.765 0.775 0.789 0.602 0.602 0.604 0.654 0.655 LOSS P 101 0.059 0.032 0.026	1.526 1.526 1.519 1.510 1.477 1.476 1.476 1.477 1.476 1.477 1.481 1.365 1.365 1.328
TIP 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.563 0.572 5.580 0.597 0.599 0.595 0.595 0.595 0.595 0.565 0.557 PERCENT SPAN 0.500 50.00 50.00 50.00	0.535 0.535 0.535 0.52. 0.553 0.597 0.591 0.596 0.616 0.673 0.694 0.717 INCI MEAN 2.5 2.6 3.0 4.1	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.873 0.873 0.867 0.791 0.695 0.670 0.658 0.654 0.598 0.599 0.488 0.472 DEV	IN 0.563 0.572 0.580 0.597 0.598 0.595 0.595 0.595 0.563 0.563 0.557 D-FACT 0.420 0.412 0.427	0.47 0.373 0.389 0.400 0.419 0.430 0.433 0.434 0.455 0.454 0.455	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C TOT 0.235 0.191 0.156 0.094	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 00FF PROF 0.148 0.078 0.035	VEL R 0.755 0.744 0.765 0.765 0.765 0.769 0.862 0.864 0.865 LOSS P TUT 0.059 0.059 0.059	1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.365 1.328
TIP 23456789111HUB	IN 3.563 0.572 5.580 0.597 0.599 0.599 0.569 0.565 0.557 PERCENT SPAN 3.500 50.00 50.00 50.00	0.535 0.535 0.535 0.52. 0.553 0.597 0.591 0.596 0.600 0.616 0.673 0.694 0.717 INCL MEAN 2.5 2.6 3.0 4.1 5.2	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.873 0.867 0.667 0.695 0.670 0.658 0.658 0.598 0.599 0.488 0.472 DEV	IN 0.563 0.572 0.580 0.597 0.599 0.598 0.595 0.595 0.595 0.563 0.563 0.557	0.77 0.373 0.389 0.400 0.419 0.430 0.435 0.434 0.455 0.455 0.455 0.795 0.795 0.795	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C TOT 0.235 0.191 0.156 0.094 0.068	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 00FF PROF 0.148 0.078 0.035 0.025	VEL R 0.755 0.744 0.755 0.760 0.775 0.765 0.789 0.682 0.684 0.685 LOSS P TOT 0.059 0.032 0.026 0.017 0.012	1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.476 1.476 1.477 1.481 1.365 1.365 1.328
TIP 23456789111HUB	IN 3.563 0.572 5.580 0.597 0.599 0.599 0.599 0.569 0.565 0.557 PERCENT SPAN 3. 5.00 55.00 55.00 55.00	0.535 0.535 0.535 0.52. 0.553 0.578 0.591 0.596 0.603 0.616 0.673 0.614 0.717 INCI MEAN 2.5 2.6 3.0 4.1 5.2	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.871 0.873 0.867 0.791 0.659 0.659 0.654 0.654 0.599 0.488 0.472 DEV	IN 0.563 0.572 0.580 0.597 0.598 0.598 0.595 0.595 0.595 0.563 0.563 0.557 D=FACT 0.435 0.412 0.412 0.412 0.427 0.462	0.77 0.373 0.389 0.400 0.419 0.430 0.435 0.434 0.455 0.454 0.455 0.796 0.795 0.796 0.919 0.925	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C TOT 0.235 0.191 0.156 0.094 0.068	007 -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 00FF PROF 0.148 0.035 0.025 0.025	VEL R 0.755 0.744 0.755 0.760 0.775 0.762 0.762 0.763 0.763 0.662 0.644 0.654 0.655 LOSS P TOT 0.059 0.032 0.026 0.012 0.012	1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.403 1.365 1.365 1.328
TIP 23456789111HUB	IN 3.563 0.572 5.580 0.597 0.599 0.598 0.597 0.596 0.595 0.563 0.557 PERCENT SPAN 3. 5. 0.00 55.00 57.50	0.535 0.535 0.535 0.52. 0.553 0.587 0.591 0.596 0.600 0.616 0.673 0.694 0.717 INCI MEAN 2.5 2.6 3.0 4.1 5.2 5.5	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855 DENCE SS 0.0 -0.0 0.0 0.0	0.01 0.871 0.873 0.867 0.791 0.695 0.658 0.654 0.654 0.598 0.472 0.488 0.472	IN 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.563 0.557 0-FACT 0.435 0.412 0.412 0.412 0.473 0.478	0.47 0.373 0.589 0.400 0.419 0.435 0.434 0.435 0.455 0.455 0.796 0.796 0.796 0.796 0.878 0.978	IN -2.68 -2.24 -1.73 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C TOT 0.235 0.191 0.156 0.094 0.065 0.065	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 0.078 0.026 0.026 0.026	VEL R 0.755 0.744 0.765 0.779 0.782 0.789 0.802 0.804 0.864 0.865 LOSS P TOT 0.059 0.032 0.026 0.012	MACH 1.5 1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.328 ARAM PROF 0.024 0.018 0.018 0.005 0.005
TIP 234567891011HUB	IN 0.563 0.572 0.580 0.572 0.588 0.597 0.598 0.597 0.596 0.595 0.595 0.565 0.565 0.557 PERCENT SPAN 0.500 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55.00 55	0.535 0.535 0.535 0.52. 3.553 0.597 0.596 0.600 0.616 0.673 0.694 0.717 INCI MEAN 2.6 3.0 4.1 5.2 5.5 5.6 5.7	1N 1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.090 1.046 0.920 0.887 0.855 DENCE SS 0.0 -0.0 0.0 0.0	0.01 0.871 0.873 0.867 0.791 0.695 0.658 0.654 0.654 0.598 0.472 0.488 0.472	IN 0.563 0.572 0.580 0.597 0.598 0.595 0.595 0.595 0.563 0.563 0.557 D=FACT 0.462 0.412 0.427 0.462 0.473 0.473	0.41 0.373 0.589 0.400 0.419 0.435 0.436 0.437 0.442 0.455 EFF 0.706 0.755 0.796 0.925 0.925 0.931	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24  LOSS C TOT 0.235 0.191 0.196 0.068 0.065 0.065	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 0.025 0.025 0.026 0.025	VEL R 0.755 0.744 0.765 0.775 0.789 0.789 0.802 0.804 0.864 0.865 LOSS P TOT 0.032 0.032 0.012 0.012	MACH 1.5 1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.326
TIP 234567891011HUB RTP 25456789	IN 0.563 0.572 0.580 0.597 0.599 0.599 0.595 0.595 0.595 0.595 0.595 0.595 0.565 0.557 PERCENT SPAN 0.500 50.00 55.00 55.00 55.00 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60	0.535 0.535 0.535 0.52. 3.553 0.597 0.596 0.600 0.616 0.673 0.694 0.717 INCI MEAN 2.5 2.6 3.0 4.1 5.2 5.5 5.5	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855  DENCE SS 0.0 -0.0 0.0 0.0 0.0	0.07 0.873 0.873 0.867 0.791 0.695 0.654 0.634 0.598 0.634 0.598 0.472 DEV 5.4 4.8 4.4 2.9 2.6 2.9 2.9 2.9 2.9	IN 0.563 0.572 0.580 0.597 0.598 0.597 0.596 0.595 0.595 0.563 0.557 0-FACT 0.435 0.412 0.412 0.412 0.473 0.478	0.47 0.373 0.589 0.400 0.419 0.435 0.434 0.435 0.455 0.455 0.796 0.796 0.796 0.796 0.878 0.978	IN -2.68 -2.24 -1.70 1.22 4.65 5.88 6.43 7.00 7.59 9.47 15.94 18.03 20.24 LOSS C TOT 0.235 0.191 0.156 0.094 0.068 0.065 0.065 0.065 0.065	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 0.078 0.026 0.026 0.026	VEL R 1.755 0.744 0.765 0.775 0.779 0.789 0.802 0.844 0.864 0.865 LOSS P TOT 0.059 0.032 0.026 0.017 0.012 0.012 0.011 0.011	MACH 1.5 1.526 1.519 1.510 1.497 1.476 1.476 1.476 1.476 1.476 1.477 1.481 1.405 1.365 1.328 ARAM PROF 0.024 0.018 0.018 0.005 0.005
TIP 23456789111HUB RTP 2545678911	IN 3.563 0.572 5.580 0.597 0.599 0.599 0.599 0.565 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 0.595 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0.595 0.595 0.595 0.595 0.595 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.505 0.5	0.535 0.535 0.535 0.52. 0.553 0.597 0.596 0.600 0.616 0.673 0.694 0.717 INCI MEAN 2.6 3.0 4.1 5.2 5.5 5.7 5.9 6.3	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855	0.07 0.873 0.873 0.667 0.791 0.695 0.654 0.634 0.598 0.634 0.598 0.472 DEV 5.4 4.8 4.4 2.9 2.6 2.9 2.9 2.9 2.9 2.9	IN 0.563 0.572 0.580 0.597 0.598 0.598 0.595 0.595 0.595 0.563 0.563 0.557 D-F4CT 0.420 0.412 0.427 0.478 0.478 0.478 0.488 0.504 0.543	0.01 0.373 0.588 0.400 0.419 0.433 0.436 0.437 0.442 0.455 0.454 0.455 0.796 0.796 0.925 0.925 0.931 0.935	IN -2.68 -2.24 -1.73 1.22 4.65 5.68 6.43 7.59 9.47 15.94 18.05 20.24 LOSS C TOT 0.235 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.059 0.056 0.074	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.66 6.11 7.54 11.97 13.24 14.58 0.035 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 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1.477 1.403 1.365 1.328 ARAM PROF 0.018 0.013 0.005 0.005 0.005 0.005 0.005
TIP 234567891011HUB RTP 25456789	IN 0.563 0.572 0.580 0.597 0.599 0.599 0.595 0.595 0.595 0.595 0.595 0.595 0.565 0.557 PERCENT SPAN 0.500 50.00 55.00 55.00 55.00 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 57.50 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60	0.535 0.535 0.535 0.52. 3.553 0.597 0.596 0.600 0.616 0.673 0.694 0.717 INCI MEAN 2.5 2.6 3.0 4.1 5.2 5.5 5.5	1.409 1.388 1.366 1.268 1.161 1.133 1.119 1.105 1.090 1.046 0.920 0.887 0.855  DENCE SS 0.0 -0.0 0.0 0.0 0.0	0.07 0.873 0.873 0.867 0.791 0.695 0.654 0.634 0.598 0.634 0.598 0.472 DEV 5.4 4.8 4.4 2.9 2.6 2.9 2.9 2.9 2.9	IN 0.563 0.572 0.580 0.597 0.599 0.595 0.595 0.595 0.563 0.563 0.557 D-FACT 0.420 0.412 0.420 0.412 0.473 0.483 0.488 0.504	0.07 0.373 0.589 0.400 0.419 0.433 0.434 0.435 0.454 0.455 0.795 0.796 0.919 0.925 0.925 0.934 0.934	IN -2.68 -2.24 -1.70 1.22 4.65 5.68 6.43 7.59 9.47 15.94 18.05 20.24 LOSS C TOT 0.235 0.191 0.196 0.065 0.065 0.065 0.065 0.065 0.059 0.056	0UT -1.58 -1.43 -1.14 1.06 3.98 4.80 5.23 5.06 6.11 7.54 11.97 13.24 14.58 0.035 0.025 0.025 0.025 0.025 0.025 0.025 0.025	VEL R 1.755 0.744 0.755 0.760 0.775 0.779 0.789 0.802 0.804 0.864 0.865 LOSS P TOT 0.059 0.032 0.026 0.017 0.012 0.012 0.012 0.011 0.011	MACH 1.5 1.526 1.519 1.510 1.497 1.476 1.476 1.477 1.481 1.403 1.365 1.328  ARIM PROF 0.024 0.018 0.013 0.005 0.005 0.005 0.005

TABLE III, - DESIGN BLADE-ELEMENT PARAMETERS FOR STATOR 17

	810	* *	120	BETAM	120	DETAM	TOTA	L TEMP	1072	PRESS
RP.	IN.	OUT	!N	DUT		OUT		RATIO	!N	RATIO
TIP	25.146	25.146	44.7	0.	44.7	0.			16.22	0.976
1	24.587	24.600	42.0	-0.				1.000	16.22	0.922
2	24.057	24,110	40.3		40.3		340.2	1.000	16.22	0.985
3	21.962		38.6	0.	38.6	0.	335.3	1.000	16.22	0.989
4	19.882	20.160	39.4	0.	39.4			1.000	16.22	0.997
5	19.364	19.670	39.8	0.	39.8	0.	333.0	1.000	16.22	0.986
6	19.364	19.426	40.0	0.	40.0	0.		1.000	16.22	0.986
7	18.646	19.182	40.2	0.	40.2	0.		1.300	16.22	0.986
	18.588		40.5	0.	40.5	0.		1.000	16.22	0.985
9			41.2	0.	41.2	0.	332.2		16.22	0.984
10	15.750	16.298	44.5	0.	44.5	٥.		1.300	16.22	0.973
11	15.238	15.815	45.7	0.	45.7 47.1	0.		1.000	16.22	1.959
HUB	14,752	15.240	47.1	-0.	47.1	-0.	333.6	1.000	16.22	0.942
	ABS	VEL	REL	VEL	MERI	D VEL	TAN	G VEL	WHEEL	
RP	IN	OUT	IN	DUT	1N	DUT	IN	OUT	IN	DUT
TIP	198.2	151.4	198.2	151.4	140.9			0.	٥.	٥.
1		155.8		155.8	147,4		132.9		0.	٥.
3	199.4	155.6	199.4	155.6	152.2	155.6		0.	0.	
3	205.5	158.8	205.3	158.8	160.5		128.3	0.	٥.	٥.
i	212.6	163.3	212.8	160.3	164.4	160.3		0.	2.	Q.
2	215.2	160.		160.	165.3	160.7		0.	٥.	0.
5 6 7 8	216.5	161.0		161.0	165.7	161.0	159.2	٥.	Q.	٥.
	219.1	161.3	217.8	161.3	166.2	161.3	140	0.	a. a.	٤. ٥.
9	223.5	62.5	223.5	162.5	168.1	161.7	142.2	٥.	3.	š.
13	239.4	158.7	259.4	158.7		150 7	167.7	o.	à.	õ.
11	245.1	155.1	245.0	155.1	171.1		175.5	ů.	5.	ě.
H.8		149.6		149.6		149.6		-0.	ů.	ā.
									* -	• •
	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO	STREAML	NE SLOPE	MERID	PE4K SS
RP.	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO	STREAM I	NE SLOPE		PEAK SS
RP T:P			IN							MACH NO 3.85:
TIP	IN 0.547 0.551	OUT	1N 0.547 0.551	0.412 0.422	IN 0.389 0.409	0.412 0.422	0.15 0.75	-0.55 0.02	VEL R 1.075 1.044	MACH NO 3.850 0.827
TIP	IN 0.547 0.551 0.556	0.412	1N 0.547 0.551 0.556	0.412 0.422 0.428	IN 0.389 0.409 0.434	0.412 0.422 0.428	0.15 0.75 1.26	-0.53 0.02 0.44	VEL R	MACH NO 0.850 0.827 0.814
1 P	IN 0.547 0.551 0.556 0.578	0.412 0.422 0.428 0.441	IN 0.547 0.551 0.556 0.578	0.412 0.422 0.428 0.441	IN 0.389 0.409 0.424 0.452	0.412 3.422 0.428 0.441	0.13 0.75 1.26 2.65	0.07 -0.53 0.02 0.44 1.67	VEL R 1.075 1.044 1.022 0.989	MACH NO 3.85: 0.827 0.814 0.815
1 P	IN 0.547 0.551 0.556 0.578 0.602	0.412 0.422 0.428 0.441 0.447	1N 0.547 0.551 0.556 0.578 0.602	0.412 0.422 0.428 0.441 0.447	IN 0.389 0.409 0.424 0.452 0.465	0.412 0.422 0.428 0.441 0.447	(N 0.13 0.75 1.26 2.65 4.50	0.55 0.02 0.44 1.67 2.65	VEL R 1.075 1.044 1.022 0.989 0.975	M4CH NG 0.85: 0.827 0.814 0.615 0.841
1 P	IN 0.547 0.551 0.556 0.578 0.602 0.610	0.412 0.422 0.428 0.441 0.447 0.448	IN 0.547 0.551 0.556 0.578 0.602 0.610	0UT 0.412 0.422 0.428 0.441 0.447 0.448	IN 0.389 0.409 0.424 0.452 0.465 0.468	0.412 3.422 0.428 0.441 0.447	(N 0.13 0.75 1.26 2.83 4.50 4.96	0.07 -0.53 0.02 0.44 1.67 2.65 2.69	VEL R 1.075 1.044 1.022 0.989 0.975 0.975	MACH NO 0.85: 0.827 0.814 0.615 0.841 0.851
TIP 1 2 3 4 5 6	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614	OUT 0.412 0.422 0.428 0.441 0.447 0.448 0.449	IN 0.389 0.409 0.424 0.452 0.465 0.468 0.470	0.412 3.422 0.428 0.441 0.447 0.448 0.449	1N 0.13 0.75 1.26 2.63 4.50 4.96 5.21	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00	VEL R 1.075 1.044 1.022 0.989 0.975 0.975	MACH NC 0.850 0.827 0.814 0.615 0.841 0.851 0.856
TIP 1 2 3 4 5 6	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614	0.412 0.412 0.422 0.428 0.441 0.447 0.448 0.449	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618	0.412 0.422 0.428 0.441 0.447 0.448 0.449	IN 0.389 0.409 0.424 0.452 0.465 0.468 0.470	0.412 0.412 0.428 0.441 0.447 0.448 0.449	0.15 0.75 1.26 2.65 4.50 4.96 5.21 5.46	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12	VEL R 1.075 1.044 1.022 0.989 0.975 0.975 0.972	MACH NO 0.85: 0.827 0.814 0.815 0.841 0.851 0.866
TIP 1 2 3 4 5 6	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622	0.412 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622	OUT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450	IN 0.389 0.409 0.424 0.452 0.465 0.468 0.470 0.472	0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72	0.07 -0.53 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24	VEL R 1.075 1.044 1.022 0.989 0.975 0.975 0.972 0.971	MACH NO 0.85: 0.827 0.814 0.815 0.841 0.851 0.856 0.861
T:P 1 2 3 4 5 6 7 8 9	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622 0.636	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636	OUT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451	IN 0.389 0.409 0.424 0.452 0.465 0.470 0.472 0.473 0.478	0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57	0.07 -0.53 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967	MACH NC 0.85: 0.827 0.814 0.615 0.841 0.856 0.866 0.865
TIP 1 2 3 4 5 6 7 8 9 10	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454 0.443	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454	IN 0.389 0.409 0.424 0.452 0.469 0.470 0.472 0.473 0.478 0.478	0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.21 5.72 6.57 9.30	0.07 -0.55 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929	MACH NC 0.85: 0.827 0.814 0.615 0.841 0.856 0.861 0.866 0.865 0.958
T:P 1 2 3 4 5 6 7 8 9	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.618 0.622 0.636 0.685 0.702	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.443	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.636 0.702	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.453	IN 0.389 0.409 0.424 0.452 0.469 0.470 0.472 0.473 0.478 0.499	0.412 0.422 0.428 0.441 0.447 0.449 0.450 0.451 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30	0.07 -0.55 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.975 0.972 0.971 0.970 0.967 0.929	MACH NO 0.85: 0.827 0.814 0.815 0.851 0.856 0.856 0.865 0.958 0.966
TIP 1 2 3 4 5 6 7 8 9 10	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454 0.443	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454	IN 0.389 0.409 0.424 0.452 0.469 0.470 0.472 0.473 0.478 0.478	0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30	0.07 -0.55 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929	MACH NO 0.85: 0.827 0.814 0.815 0.851 0.856 0.856 0.865 0.958 0.966
T:P 1 2 3 4 5 6 7 8 9	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454 0.443 0.416	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636 0.636 0.636 0.702	0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.454 0.454 0.454 0.454	IN 0.389 0.409 0.424 0.452 0.465 0.468 0.470 0.472 0.473 0.478 0.489 0.490 0.491	0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.454	1N 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.967 0.967	MACH NC 0.850 0.827 0.814 0.815 0.841 0.856 0.866 0.866 0.865 0.986 1.020
T:P 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622 0.636 0.685 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.451 0.443 0.443 0.416	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.453	IN 0.389 0.409 0.424 0.452 0.469 0.470 0.472 0.473 0.478 0.499	0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.454	1N 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.63	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.967 0.967 0.967 0.968 0.875	MACH NC 0.650 0.627 0.614 0.615 0.851 0.851 0.866 0.866 0.966 1.020
T:P 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.618 0.622 0.636 0.702 0.721 PERCENT SPAN	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.429 0.450 0.451 0.454 0.443 0.416	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.451 0.454 0.452 0.416	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.472 0.473 0.478 0.499 0.490 0.491	0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83	0UT -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.875	MACH NC 0.850 0.827 0.814 0.615 0.851 0.856 0.866 0.865 0.958 0.958
T:P 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.636 0.702 0.721 PERCENT SPAN 0.	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.453 0.452 0.416	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636 0.622 0.636 0.622 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416	IN 0.389 0.409 0.424 0.452 0.465 0.470 0.472 0.473 0.478 0.499 0.490 0.491	0.412 0.412 0.428 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.432 0.416	IN 0.13 0.75 1.26 2.83 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.675 LOSS P TOT 0.056	MACH NC 0.850 0.827 0.814 0.615 0.851 0.856 0.866 0.865 0.958 0.996 1.020 ARAM PROF 0.056
TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.685 0.702 0.721 PERCENT SPAN 0.900	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.451 0.451 0.454 0.452 0.416 INCE	1N 0.547 0.551 0.556 0.578 0.602 0.610 0.614 0.622 0.636 0.622 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.465 0.470 0.472 0.473 0.478 0.490 0.491 D-FACT	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.443 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.875 LOSS P TOT 0.056 0.033	MACH NC 0.850 0.827 0.814 0.615 0.851 0.856 0.866 0.865 0.958 1.020 ARAM PROF 0.056 0.038
TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.635 0.702 0.721 PERCENT SPAN 3.00 10.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.451 0.451 0.454 0.452 0.416 INCE MEAN 6.1 6.2	1N 0.547 0.551 0.556 0.578 0.612 0.614 0.622 0.636 0.622 0.721 0.721 DENCE SS 0.0	0UT 0.412 0.422 0.428 0.441 0.447 0.449 0.451 0.454 0.454 0.454 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.472 0.473 0.478 0.499 0.491 D-FACT	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.454 0.454	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83	0.07 -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.875 LOSS P TOT 0.056 0.033 0.023	MACH NC 3.850 0.827 0.814 0.815 0.856 0.856 0.866 0.865 0.966 1.020 ARAM PROF 0.038 0.038 0.038
TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.685 0.702 0.721 PERCENT SPAN 30.00 30.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.453 0.452 0.416 INCI MEAN 6.1 6.2 6.2	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.449 0.451 0.454 0.454 0.454 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.469 0.472 0.473 0.478 0.478 0.499 0.491 D-FACT 0.513 0.403 0.403 0.403	0.412 3.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454 0.416	IN 0.15 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83	0UT -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62 4.62	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.875 LOSS P TOT 0.033 0.029 0.033	MACH NC 3.850 0.827 0.814 0.815 0.856 0.856 0.866 0.865 0.966 1.020 ARAM PROF 0.338 0.029 0.029
TIP 1 2 3 4 5 6 7 8 9 10 111 HUB RP TIP 1 2 3 4	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.702 0.721 PERCENT SPAN 0.500 10.00 30.00 50.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.452 0.416 INCI MEAN 6.1 6.2 6.2 6.2 6.2	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.449 0.451 0.454 0.454 0.454 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.469 0.472 0.473 0.478 0.478 0.499 0.491 D-FACT 0.513 8.463 8.463 8.463	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.416 EFF	IN 0.15 0.75 1.26 2.65 4.50 4.96 5.21 5.72 6.57 9.30 10.06 10.85 CO TOT 0.141 0.099 0.077 0.055 0.063	0UT -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.077 0.098 0.077 0.098 0.077	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.972 0.970 0.967 0.929 0.936 0.875 LOSS P TOT 0.056 0.039 0.029 0.019	MACH NC 0.850 0.827 0.814 0.815 0.851 0.856 0.866 0.865 0.996 1.020 ARAM PROF 0.238 0.239 0.219 0.019
TIP 1 2 3 4 5 6 7 8 9 10 111 HUB RP TIP 1 2 3 4	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.685 0.702 0.721 PERCENT SPAN 30.00 30.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.453 0.452 0.416 INC! MEAN 6.1 6.2 6.2 6.2 6.2	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.702 0.721 DENCE SS 0.0 0.0 0.0	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.454 0.454 0.454 0.454 0.454 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.473 0.478 0.499 0.491 D-FACT 0.513 8.403 8.463 8.463 8.463	0.412 3.422 0.428 0.441 0.447 0.448 0.449 0.450 0.451 0.454 0.416	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.85 CO TOT 0.141 0.098 0.062 0.062	0UT -0.53 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.055 0.060 0.062	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.972 0.972 0.976 0.967 0.929 0.936 0.875 LOSS P TOT 0.056 0.053 0.033 0.039 0.019	MACH NC 0.850 0.827 0.814 0.815 0.841 0.856 0.856 0.956 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958
TIP 1 2 3 4 5 6 7 8 9 10 111 HUB RP TIP 1 2 3 4	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.636 0.636 0.702 0.721 PERCENT SPAN 0.500 50.00 50.00 55.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.454 0.452 0.416 INCI MEAN 6.1 6.2 6.2 6.2 6.2	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.622 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.449 0.451 0.454 0.454 0.454 0.416 DEV	IN 0.389 0.409 0.424 0.452 0.469 0.472 0.473 0.478 0.478 0.499 0.491 D-FACT 0.513 8.463 8.463 8.463	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.416	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83 LOSS CITOT 0.141 0.098 0.077 0.055 0.062 0.063	0UT -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.077 0.098 0.077 0.098 0.077	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.972 0.970 0.967 0.929 0.936 0.875 LOSS P TOT 0.056 0.039 0.029 0.019	MACH NC 0.850 0.827 0.814 0.815 0.851 0.856 0.866 0.865 0.996 1.020 ARAM PROF 0.238 0.239 0.219 0.019
TIP 1 2 3 4 5 6 7 8 9 10 11 HUB RP TIP 1 2 3 4 5 6 7 8	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.685 0.702 0.721 PERCENT SPAN 0.00 50.00 50.00 55.00 57.50 60.50	0UT 0.412 0.422 0.428 0.447 0.448 0.449 0.450 0.451 0.454 0.452 0.416 INC! MEAN 6.1 6.2 6.2 6.2 6.2 6.2 6.2	1N 0.547 0.551 0.556 0.578 0.602 0.614 0.622 0.636 0.636 0.702 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416 0.454 0.432 0.416	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.473 0.478 0.489 0.491 0.491 0.491 0.491 0.443 8.463 8.463 8.463 8.463 8.463	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.416	IN 0.13 0.75 1.26 2.65 4.50 4.96 5.21 5.46 5.72 6.57 9.30 10.06 10.83 LOSS CITOT 0.141 0.098 0.077 0.095 0.062 0.063 0.064	0UT -0.55 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.065 0.065 0.065 0.065 0.063	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.936 0.675 LOSS P TOT 0.056 0.034 0.039 0.019	MACH NC 0.850 0.827 0.814 0.815 0.841 0.856 0.856 0.956 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958
TIP 1 2 3 4 5 6 7 8 9 10 11 HUB RP TIP 1 2 3 4 5 6 7 8 9	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.685 0.702 0.721 PERCENT SPAN 0.00 50.00 55.00 55.00 57.50 62.50 70.00	0UT 0.412 0.422 0.428 0.447 0.448 0.449 0.450 0.451 0.454 0.452 0.416 INC! MEAN 6.1 6.2 6.2 6.2 6.2 6.1 6.1	1N 0.547 0.551 0.556 0.578 0.612 0.614 0.622 0.636 0.622 0.721 0.721 0.721	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416 0.454 0.432 0.416	IN 0.389 0.409 0.424 0.452 0.466 0.470 0.472 0.473 0.478 0.489 0.490 0.491  D-FACT 0.513 0.483 0.441 0.444 0.447 0.445 0.445 0.450 0.456	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.416	IN 0.15 0.75 1.26 2.85 4.50 4.96 5.72 6.57 9.30 10.06 10.83 LOSS CITOT 0.141 0.008 0.077 3.055 0.063 3.064 0.065 0.367	0UT -0.53 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.065 0.063 0.063 0.063 0.065 0.067	VEL R 1.075 1.044 1.022 0.989 0.975 0.971 0.970 0.967 0.929 0.936 0.675 LOSS P TOT 0.056 0.034 0.029 0.019 0.019	MACH NC 3.850 0.827 0.814 0.615 0.851 0.856 0.856 0.865 0.958 0.996 1.020 ARAM PROF 0.038 0.029 0.019 0.019 0.019 0.019
TIP 1 2345678910111HUB RPPT1 2345678910	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.685 0.702 0.721 PERCENT SPAN 30.00 50.00 55.00 57.50 60.30 62.50 70.00 90.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.451 0.451 0.453 0.451 0.454 0.453 0.416 INCE MEAN 6.1 6.2 6.2 6.2 6.1 6.1 6.1 6.1	1N 0.547 0.551 0.556 0.578 0.612 0.614 0.622 0.636 0.622 0.721 DENCE SS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416 DEV 14.2 12.3 11.1 0.4 0.8 0.8 0.8 0.8 0.8 0.8	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.472 0.473 0.478 0.489 0.490 0.491 D-FACT 0.513 0.483 0.463 0.441 0.447 0.448 0.447 0.448 0.456 0.456 0.509	0.412 3.422 0.428 0.441 0.447 0.448 0.450 0.451 0.454 0.432 0.416	IN 0.15 0.75 1.26 2.85 4.50 4.96 5.72 6.57 9.30 10.06 10.83 LOSS CI 0.141 0.098 0.077 3.095 0.063 3.064 0.065 0.067 0.110	0UT -0.53 0.02 0.44 1.67 2.65 2.68 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.098 0.077 0.098 0.077 0.095 0.063 0.063 0.064 0.065	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.0875 LOSS P TOT 0.056 0.033 0.029 0.019 0.019 0.019 0.019	MACH NC 0.850 0.827 0.814 0.615 0.851 0.856 0.856 0.956 0.956 1.020 ARAM PROF 0.038 0.029 0.019 0.019 0.019 0.019 0.019
T:P 1 2 3 4 5 6 7 8 9 10 11 HUB RP T:P 2 3 4 5 6 7 8 9 10 11	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.614 0.622 0.636 0.636 0.685 0.702 0.721 PERCENT SPAN 30.00 50.00 55.00 57.50 60.30 62.50 70.00 95.30	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.450 0.451 0.451 0.454 0.453 0.451 0.454 0.453 0.451 6.1 6.2 6.2 6.2 6.1 6.1 6.1 6.1	IN 0.547 0.551 0.556 0.578 0.612 0.614 0.622 0.636 0.622 0.721 DENCE SS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0UT 0.412 0.422 0.428 0.441 0.447 0.454 0.451 0.454 0.454 0.453 0.454 0.454 0.454 0.454 0.454 0.454 0.456 0.451 0.454 0.456 0.451 0.456 0.451 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.456 0.	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TIP 1 2345678910111HUB RPPT1 2345678910	IN 0.547 0.551 0.556 0.578 0.602 0.614 0.618 0.622 0.636 0.685 0.702 0.721 PERCENT SPAN 30.00 50.00 55.00 57.50 60.30 62.50 70.00 90.00	0UT 0.412 0.422 0.428 0.441 0.447 0.448 0.449 0.451 0.451 0.453 0.451 0.454 0.453 0.416 INCE MEAN 6.1 6.2 6.2 6.2 6.1 6.1 6.1 6.1	1N 0.547 0.551 0.556 0.578 0.612 0.614 0.622 0.636 0.622 0.721 DENCE SS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0UT 0.412 0.422 0.428 0.441 0.447 0.450 0.451 0.454 0.454 0.452 0.416 DEV 14.2 12.3 11.1 0.4 0.8 0.8 0.8 0.8 0.8 0.8	IN 0.389 0.409 0.424 0.452 0.468 0.470 0.472 0.473 0.478 0.489 0.490 0.491 D-FACT 0.513 0.483 0.463 0.463 0.463 0.463 0.463 0.465 0.465 0.465 0.465 0.465	0.412 3.422 0.428 0.441 0.447 0.454 0.453 0.454 0.454 0.456 0.456 0.456 0.456 0.456 0.456	IN 0.15 0.75 1.26 2.85 4.50 4.96 5.72 6.57 9.30 10.06 10.83 LOSS CI 0.141 0.098 0.077 3.095 0.063 3.064 0.065 0.067 0.110	0UT -0.53 0.02 0.44 1.67 2.65 2.88 3.00 3.12 3.24 3.62 4.55 4.62 4.62 0.065 0.062 0.063 0.063 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.	VEL R 1.075 1.044 1.022 0.989 0.975 0.972 0.971 0.970 0.967 0.929 0.0875 LOSS P TOT 0.056 0.033 0.029 0.019 0.019 0.019 0.019	MACH NC 0.850 0.827 0.814 0.615 0.851 0.856 0.856 0.956 0.956 1.020 ARAM PROF 0.038 0.029 0.019 0.019 0.019 0.019 0.019

TABLE IV. - BLADE GEOMETRY FOR ROTOR 20

	PERCENT	843	110	BLA	DE ANGL	ES	DELTA	CONE
<b>B</b> P	SPIN		RJ	KIC	KTC	KOC	INC	ANGLE
TIP				63.94	65.97	59.17	2.52	
7	5.	24.724	24.614	62.90	62.83	58.74	2.77	-2.925
2	12.	24, 156	24 057	61.85	61.62	58 16	3.05	-2.520
3	52	21.810	21 629	57.80	56.14	55.16	4.11	0.434
ž	50.	14.385	19.601	57.80 53.76	50.05	49.12	5 19	4 227
	55	18 764	19 044	52.71	48 42	4. 35	5 46	5 281
	56	18 451	18 766	52.71 52.18	47 50	45 90	5 50	5 834
5	50.	18 136	18 467	51 64	46 73	44 57	5 78	6 330
8		17 814	18 209	51.64 51.09	45 85	43 20	5 96	6 974
9	**	16 951	17 174	49 43	48 22	30 54	5 25	0.977
10	40	14 130	15 145	49.43	16 11	20.60	7 %	14 611
11	05	13 439	14 566	45 40	T4 05	14 38	7 4	16.271
HUB	100	12 785	14 031	43.40	12 A.	7 80	7.64	17.597
			14.031	•2.12	32.40	30	7.64	17.397
		THICK				MENS: ON		
RP	1:	TM		ZIC	ZMC	ZTC	ZOC	
T:P	2.051	0.153	3.051	1.017	2.032	2.43?	3.00	
*	3.35	0.165	0.051	0.960	2.034	2.409	3.135	
3	351	1.175	0.351	0.942	2.055	2.376	3.175	
	0.051	0.217	0.351	0.760	2.057	2.204	3.340	
4	2.35	0.261	0.051	0.609	2.057	1.957	5.534	
5	3.351	1.272	0.05	0.565	2.035	1.882	3.500	
6	2.:5:	0.276	0.051	0.539	2.034	1.842	3.6:9	
	:.:5"	0.284	0.051	0.514	2.055	1.800	3.649	
	51	1.297	0.051	0.490	2.032	1.757	3.6 8	
÷		0.5	0.051	5.415	2.025	1.617	3.775	
•	:.:5'	0.359	0.05	0.163 3.384	1.991	1.161	4.058	
* *	5	0.572	0.05	3.384	1.977	1.021	4.129	
~.8	:.:5:	1.585	0.05	3.000	1.961	0.875	4.196	
	4ERJ	SETTING	TOTAL		x		AREL	
RP	CHORD	NOLE	CAMBER	SOLIDITY	FACTOR		RATIO	
T:P	4.6 6			1.298			1.045	
1	4.0.0	62.19	4.16	1.327	0.710	3.82	1.044	
3	4.6 6	61.10	5.69	1.500	0.775	4.20		
3	4.65		2.64	1.500	1.025	6.30	1.041	
4	4.680	51.68	4.64	1.681	1,140			
5	4.683	48.98		1.735			1.040	
6	4.686		6.30	1.765	1.158			
7	4.688	-	7.07	1.795	1.165	9.77	1.040	
6	4.691	46.19	7.81	1.824	1.167	10.06	1.041	
9				1.925	1,175	10.91	1.042	
10	4.784		24.09	2.289	1.135	12.65	1.046	
11	4.820		29.07	2.412	1.151	13.07	1.048	
HUB	4.062	25.78	34.82	2.547	1.130	13.46	1.050	

TABLE V. - BLADE GEOMETRY FOR STATOR 17

	000000			Di A	DE INCL	ec.	DELTA	FRAC
RP	PERCENT	R:	RO	VIC.	DE ANGL	KOC		
TIP					E0 24	-14.15		0.057
		25.146	24 500	35.90	20.00	-12 11	6.14	
1				35.90	27.05		6.16	
2		24.057				-0.40	6.18	2.467
3		21.962						
4		19.882			28.25		6.16	
5		19.364		33.70				
6		19.105			26.84			
7		18.846			29.05			4.852
8		18.588				8.72	6.14	5.077
9	70.	17.812	18.215	35.15	30.01	-8.66	6.13	5.805
10	97.	15.750	16.298	38.48 39.76	32.94	-8.79	6.07	7.976
11	95.	15.238	15.815	39.76	34.02			8.430
HUB	100.	14,752	15.240	41.21	<b>35</b> .22	-9.14	6.03	7.472
	D: 100	THICKN	eccc		XIAL DI	MENICIA	ue	
RP.	TI ADE	IN	TO	ZIC			Z0C	
TIP					ZMC	ZTC		
1	0.051	0.279			9.388		11.507	
	0.051	0.279	0.051	7.578	9.395			
2	0.051	1.279	0.351	7.556	9.400		11.507	
3	0.651	1.2.9	0.251	7.537			11.536	
4	0.051	2.2.9	0.051	7.545	9.405		11.506	
5	0.051	0.2.9	0.051	7.546			11.505	
•	0.051	0.279	0.051	7.547	9.404		11.504	
	0.051	0.2.9	0.051	7.549	9.405		11.504	
	2.251	1.2 9	0.051	7.551	9.403	8.625	11.534	
9	1.:5	1.2.9	0.051	7.559	9.431	8.601	11.503	
	0.351	0.279	0.051	7.595	9.394		11.5.0	
11	51	1.279	0.051	7.607			11.499	
₩.8	2.251	0.279	0.051	7.624	9.387	8.549	11,497	
	AERO	SETTING	TOTAL		x		AREA	
50				SOLIDITY		PHISS	RAT:0	
T:P	4.179	19.35			0.600	13.51	1.359	
1	4.178	17.85	48.20	1.298	0.600	11.95	1.311	
3	4.160		45.20		0.600	10.86	1.290	
3	-4.165	15.86	41.80	1.449	0.600	9.31	1.244	
4	4.169		42.16		0.633	8.87		
5	4.191		42.51		0.633	8.63		
6	4.192	16.52	42.69	1.662	0.600	8.60	1,195	
?	4.195		42.88		0.600	8.78	1,168	
8	4.194	16.73	43.08	1,708		8.76		
9	4,199	17.10						
10	4.216	18.70	47.27	2.010				
11	4.220	19.32	48.69	2.076				
HUB	4.209					9. 31	1.114	
			34.33	20				

#### TABLE VI. - OVERALL PERFORMANCE FOR

#### STAGE 20-17

#### (a) 50 Percent of design speed.

READ ING NUMBER			285
ROTOR TOTAL PRESSURE RATIO		 	1.150
STAGE TOTAL PRESSURE RATIO		 	1,125
DATAS TATAL TEMPERATURE SERVICE			
CRACE BOR. BENDERAL DE DARIO	-		
ROTOR TEMP. RISE EFFICIENCY			
STAGE TOPP, RISE EFFICIENCY			
ROTOR MOMENTUM RISE EFFICIENCY.		 	0.820
ROTOR HEAD, RISE COEFFICIENT		 	0.226
STAGE HEAD RISE COEFFICIENT			0.216
FLOW COEFFICIENT			0.299
7.5.4.000			8.677
AT FLOW PER UNIT FRONTAL AREA .			56.56
AT FLOW PER UNIT ANNULUS AREA .			76.52
AT FLOW AT DRIFTCE			11.76
AT FLOW AT ROTOR INLET		 	** 63
ALL LEGEN ALL MOTOR TREET,		 	11.92
AT FLOW AT ROTOR OUTLET		 	12.14
MT FLOW AT STATOR OUTLET			12.71
ROTATIVE SPEED			8042.4
DESCRIPTION OF SECTION OF SECTION			
PERCENT OF DESIGN SPEED		 	- 50.0

#### (b) 60 Percent of design speed,

READING NUMBER				. 2855
ROTOR TOTAL PRESSURE RATIO				1,191
STAGE TOTAL PRESSURE RATTO				1.1"9
ROTOR TOTAL TEMPERATURE RATE	0 .			1.064
STAGE TOTAL TEMPERATURE RATE	0 .			1.064
ROTOR TEMP. RISE EFFICIENCY				0.799
STAGE TEMP. RISE EFFICIENCY				0.755
ROTOR MOMENTUM RISE EFFICIEN	KΥ.			0.821
ROTOR HEAD RISE COEFFICIENT				0.220
STAGE HEAD RISE COEFFICIENT				0.215
FLOW COEFFICIENT				0.50
AT FLOW PER UNIT FRONTAL ARE				71,11
MT FLOW PER UNIT ANNULUS ARE	Α,			95.11
AT FLOW AT DRIFTCE				14.29
MT FLOW AT ROTOR INLET				14.50
				14.85
AT FLOW AT STATOR OUTLET .		 *		15.36
ROTATIVE SPEED				9628.7
PERCENT OF DESIGN SPEED				. 59.8

#### (c) 70 Percent of design speed,

READING NUMBER	a	@	0	9	0	G	. 2917	265.1	265:	2830	2829
ROTOR TOTAL PRESSURE MATLO .			9				1,161	1.198	1.232	1.258	1
							1.130	1,168	1.221	1.244	1.355
ROTOR TOTAL TEL PERATURE RATIO								1.061	1.071	1.081	1,292
STAGE TOTAL TEMPERATURE RATIO							1,243	1.260	1.070	1.080	1.090
ROTOR TEXP. RISE EFFICIENCY .			Ī					0.872	0.859	0.858	0.700
STAGE TOP. RISE EFFICIENCY .	•				•		0.757	1.65	0.836	0.604	0.743
ROTOR MOI ENTUM RISE EFFICIENCY			*				0.005	1.924	1,906	0.864	0.804
WALLAND LINE PROPERTY OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRES	*						0.013				
ROTOR HEAD RISE COEFFICIENT .							0.155	0.175	0.201	0.219	0.232
STAGE HEAD RISE COEFFICIENT .							0.115	8.164	0.195	0.200	0.21"
FLOA COEFFICIENT								3.413	0.5	0.345	0.50
AT FLOW PER UNIT FRONTAL AREA							115,75	126.92	98.92	91.99	62.60
AT FLOW PER UNIT ANNULUS AREA	Ċ						152.12	145.21	152.51	123.04	112.50
A P AU IS ABIRIAR							22.05				
AT FLOW AT ORIFICE	*	10				*	66.63	21.4	19.86	10.4	16.63
AT FLOW AT ROTOR INLET							25.21	31. 6	20.15	18.72	16,79
MT FLOW AT ROTOR OUTLET							25.32	22.04	20.52	19.22	1"
AT FLOW AT STATOR OUTLET							25.67	22.82	20.75	19.42	4
ROTATIVE SPEED	_	-				-	11264.2	11,756.	11228.2		-17 2
BEDERNY OF BERLEN CAPES			*		*						
PERCENT OF DESIGN SPEED							. 70.1	69.9	69. "	71.4	* * *

#### TABLE VI. - Concluded,

#### (d) 80 Percent of design speed,

WELL VER							. 6 4
ATTR TO L PREOSURE ALTE		_				-	0.8%
S'AJE "I'A PRESSURE RATIO .		-	-			-	1,850
STATE OF THE STATE OF STATE							7,179
STATE TO A "EMERY " WE SA" !!							1,116
STOR TEST, RISE ETTICIENCY .							7 6.1
STATE TOWN RISE ETFICIENCY .							1. "6,
ALTER MOVEN OF RISE EFFICIENC	٧.	9.	90			.99	4.04
ACTUS HEAD RISE CONTRICTEN" .							3.55
STATE HEAD RISE COUNTRICIENT .						-	0 9.97
Lincoln					-		
" THE PER IN. FRONTAL AREA	0						90.50
" F. L. PER IN! THE LIS AREA							129,18
				-		9	
a Time of MITHER	9		0			9	0.83
" Take 1" 80" OR TALE"							19.6
at Face at Aprile Softer					-	-	19.95
	9	.00					
A FLOW AT STATOR OUTLET				-			21.56
ACTATIVE SPEED							12956.3
	-	*	-	-	-		
PERCENT OF DESIGN SPECT	00						. 80.5

#### (c) 90 Percent of design speed,

REACING N. MEER	G				2821	2821	38	38.74	2859
ROTOR TOTAL PRESSURE RATIO			9		1.36	1.428			1.49
STADE TOTAL PRESSURE RATIO					1.344	1,415	1.454	1.464	1,455
ACTUA "C"AL TEMPERATURE RATIO .					1,129	1.125	1.15"	1.14"	1,151
STAGE "CTAL TEMPERATURE RATIO .					1,119	1.124	1,150	1,145	1,149
AUTUR "EMP. RISE EFFICIENCY					1.84	1.656	2.655	2.652	0.809
STALE TEMP. RISE EFFICIENCY					1.806	0.059	0.650	1.793	1.758
ROTOR MOMENTUM RISE EFFICIENCY.					0.072	0.895	0.005	3.846	0.818
ROTOR HEAD RISE COEFFICIENT					2.176	0.208	0.226	1.256	0.240
STAGE HEAD RISE COEFFICIENT						0.202	0.210	1.234	0.222
FLOW COEFFICIEN					1.456	0.419	0.596	2.360	1.550
AT FLOW PER UNIT FRONTAL AREA.					158.62	154.21	128.53	118,94	112.18
AT FLOW PER UNIT ANNULUS AREA .					*65.46	179.52	1	159.28	150.05
" FLOW A" DRIFICE					2".6"	36.65	5. %	25.66	22.52
AT FLOW AT ROTOR INLET					28.2"	27.50	36.2	34.36	22.89
AT FLOW AT ROTOR DUTLET					26.50	27.78	26.6	24.77	25.59
AT FLOW AT STATOR DUTLET					29.51	28.72	27.56	25.65	24.76
ACTATIVE SPEED				w	14619.1	14579.0	:4592.1	14571.9	14500.8
PERCENT OF DESIGN SPEED		œ			. 91.0	90.6	90.6	90.5	90.1

#### (f) 100 Percent of design speed,

READING NUMBER						261.4	28.8	2913	2914	261
ROTOR TOTAL PRESSURE RATIO						1,416	1,556	1.614	1.642	1.665
STAGE TOTAL PRESSURE RATIO						.503	1.515	1.502	1,612	1,615
ROTOR TOTAL TEMPERATURE RATIO.		-			_	1.15	1.15	1.179	1.182	1,10,
STAGE TOTAL TEMPERATURE RATIO.				•	•	1,150	1,156	1,172	1,179	1,16"
ACTUR TEMP. RISE EFFICIENCY	*	*	*	*	*	- 100	4.65	6.6.7	0.657	1.834
40.04 5 4155 5 101540	*					81 77				
STAGE TEMP. RISE EFFICIENCY						1. 49	1.808	6.6:3	0.007	1.784
RUTOR MOMENTUM RISE EFFICIENCY					9	1.0	1.065	6.069	0.865	4.85
ROTOR HEAD RISE COEFFICIENT						A	1.210	0.234	0.242	1.250
STADE HEAD RISE COEFFICIENT						0.156	0.201	4.223	1.229	1.00
FLOR COEFFICIEN						1.4%	428	0.412	1.41	2.5
* P * BPD A ** PD:A** +DP *										
" FLOW PER LAST FRONTAL AREA.					9	148.62	14".25	142.77	159.88	155,44
A" FLOR PER INIT ANNILUS AREA.						100.5	196,96	190.96	187.19	178.54
" FLIA " CRIFICE						.9.66	29.5"	26.67	28.09	26.8
A" FLOW A" ROTOR INCE"						51.75				
M . Prim M . Lin Put 1 400		9		9		2016	29.9.	29.19	28.55	9.00 52
A" FLOW AT ROTOR OUTLE"						50.23	50.25	29.40	28.96	38.14
AT FLOW AT STATOR OUTLET						51.43	51.55	\$1.60	51.55	29.64
30"4":\E SPEED						12121 6				
PERIOD PARTIES AND THE					(8)	645.16	16106.4	16163.9	16118.0	6. 8.5
FERGEN" OF SESSON SPEED		*	w	*	*	99.9	100.0	100.0	100.1	99.9

## TABLE VII, - BLADE-ELEMENT DATA AT BLADE EDGES FOR ROTOR 20

## (a) 50 Percent of design speed, reading 2837

F: 254561.89.11	RADI: (N 0.07 24.734 24.615 24.155 24.356 21.811 21.829 19.385 19.621 18.766 19.345 18.451 18.766 17.818 18.209 16.852 17.374 14.152 15.146 13.439 14.567	285 8ET20 (N 001) -0.0 46. -0.0 45. -0.0 47. -0.0 50. -0.0 51. -0.0 53. -0.0 55. -0.0 47. -0.0 48.	0N 001 8 72.7 65.5 0 71.8 60.8 7 69.4 58.6 0 67.5 52.9 1 66.8 51.9 8 66.4 52.1 2 56.1 51.5 8 65.7 50.7 5 64.6 45.4 1 60.5 50.6	1314L TEMP 1N RATIO 369.0 1.055 366.6 1.052 368.0 1.243 266.0 1.243 267.6 1.045 267.6 1.045 267.6 1.343 267.6 1.343 267.6 1.343	TOTAL PRESS IN RATTO 1.1257 1.1336 1.1326 1.1326 1.1325 1.1322 1.1421 1.1522 1.1522 1.1622 1.1722 1.1822 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1922 1.1022 1.1022 1.1022 1.1022 1.1022 1.10
P. 25.45.61 8	485 VEL	FEL VEL (N 0/17 218.6 149.1 214.4 152.6 196.2 157.1 176.7 112.9 176.1 105.2 176.9 96.2 164.7 93.6 157.1 92.1 156.5 88.6 129.8 85.4	67.1 74.4 69.6 71.7 68.5 66.1 67.9 65.2 68.6 62.0 67.7 68.1 67.6 56.5 67.5 64.7	-0.0 T8.9 -0.0 60.5 -0.0 61.0 -0.0 60.7	**EE. SPEE:    A
F. 23.45.61.69.41	485 MACH NO 1 2.192 0.289 1.198 0.294 1.204 0.265 1.202 0.294 1.203 0.294 1.203 0.292 1.203 0.292 1.199 0.501 1.199 0.527 1.189 0.551	REL MACH NO IN 0/7 0.644 0.430 0.632 0.441 0.579 0.399 0.522 0.308 0.508 0.309 0.495 0.279 0.496 0.273 0.496 0.273 0.495 0.258 0.405 0.258 0.385 0.249	IN 001 0.192 0.193 0.198 0.215 0.204 0.208 0.202 0.198 0.202 0.199 0.203 0.175 0.203 0.172 0.199 0.188 0.199 0.222		MER: PELF 3:
RP 1 25 4 5 6 7 8 9 10 11	PERCENT INC. SPAN MEAN 5.00 9.8 10.00 9.9 30.00 11.6 50.00 13.5 55.00 14.1 57.50 14.3 60.00 14.5 62.50 14.7 70.00 15.2 90.00 17.2	SS	0.446 0.679 0.406 0.731 0.411 0.908 0.488 0.811 0.520 0.801 0.539 0.785 0.560 0.777 0.568 0.776 0.549 0.806 0.487 0.923	LOSS COEFF TOT PROF 0.256 0.256 0.192 0.192 0.137 0.137 0.160 0.160 0.177 0.177 0.195 0.195 0.209 0.209 0.214 0.214 0.194 0.194 0.093 0.093 0.115 0.115	LOSS PARAM TOT PROF 0.040 0.040 0.034 0.034 0.024 0.024 0.029 0.029 0.031 0.031 0.034 0.034 0.036 0.036 0.037 0.037 0.035 0.035 0.017 0.017 0.022 0.022

TABLE VII, - Continued,
(b) 60 Percent of design speed; reading 2835

P. 25450165	16.650 17.574	185 8011M 18 001 -0.0 40.4 -0.0 43.2 -0.0 47.6 -0.0 50.6 -0.0 50.6 -0.0 50.6 -0.0 50.6 -0.0 47.4 -0.0 40.4	1% 307 72.3 65.1 71.3 60.8 68.9 58.6 66.8 53.2 66.3 51.9 65.9 51.7 65.6 51.0 65.2 50.1 64.0 44.5 59.9 28.9	10 1 100 268.5 1.081 268.6 1.75 268.3 1.62 268.3 1.62 268.9 1.66 267.9 1.66 267.9 1.66 267.8 1.66 267.8 1.65 267.8 1.055 267.6 1.055	PRESS R4 :::  5
P. 25450 60	485 VEL 19.5 120.5 62.7 122.5 64.8 117.0 65.9 120.6 65.1 121.2 65.1 121.2 65.1 121.2 65.2 121.5 62.5 121.5 62.5 121.5 62.5 121.5	REL VEL (N 0.1 261.7 177.1 257.5 182.5 255.7 165.0 212.6 134.9 206.5 124.7 203.6 19.7 201.0 114.7 197.9 111.5 189.3 111.0 164.6 106.3 156.7 103.1	85.1 74.1 82.9 72 82.9 71.5 85.0 79.1 82.5 95.1	-0.0 95.1 -0.0 97.4 -0.0 98.0	249.5 248.2 243.8 242.8 219.9 221.1 195.5 197.5 189.1 191.8 185.1 186.6 179.6 183.6 179.6 183.6 179.6 183.6
\$ - 2 M - 4 B - 61 B - 6 - 61		REL MACH NO IN OUT 0.772 0.506 0.761 0.523 0.697 0.476 0.629 0.389 0.611 0.360 0.602 0.346 0.594 0.331 0.565 0.322 0.560 0.321 0.463 0.300	MERIO MACH NO IN 001 0.235 0.229 0.244 0.255 0.251 0.246 0.248 0.233 0.246 0.222 0.246 0.214 0.245 0.208 0.245 0.206 0.245 0.229 0.244 0.271 0.234 0.280		MERIO PEL 35 EL 9 MICH 13 5 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963 1963
\$P : 254551 8 9	PERCENT INCI SPAN MEAN 5.00 9.4 10.00 9.4 30.00 11.1 50.00 13.0 95.00 13.6 57.50 13.7 60.00 14.0 62.50 14.2 70.00 15.4 95.00 15.4	DENCE DEV 55 6.6 4.4 6.4 2.6 7.0 5.4 7.8 4.1 8.1 5.0 8.2 5.9 8.3 6.4 8.3 6.8 8.4 5.8 8.1 8.1	0-FACT EFF 0.453 0.668 0.411 0.727 0.412 0.818 0.492 3.811 0.528 0.833 0.546 0.790 0.566 0.792 0.574 0.783 0.550 0.820 0.494 0.942 0.493 0.935	LOSS COEFF TOT PROF 0.257 0.257 0.203 0.203 0.155 0.153 0.162 0.162 0.180 0.180 0.194 0.194 0.196 0.196 0.209 0.209 0.185 0.185 0.072 0.072 0.092 0.092	LUSS PARAM TOT PROF 0.044 0.044 0.037 0.037 0.023 0.025 0.029 0.129 0.032 0.032 0.034 0.034 0.034 0.034 0.037 0.037 0.034 0.034 0.014 0.014 0.016 0.016

## (c) 70 Percent of design speed; reading 2829

		285 BETAM 2N 007 -0.0 50. -0.0 45. -0.0 50. -0.0 52. -0.0 53. -0.0 54. -0.0 55. -0.0 55. -0.0 48. -0.0 49.	1N 007 172.3 63.2 171.4 61.0 18.9 58.1 18.66.8 52.5 18.66.2 51.4 18.65.9 51.4 18.65.5 51.1 18.65.2 49.9 18.65.2 49.9 18.65.2 49.9 18.65.2 44.3 18.65.2 49.9 18.65.2 44.3 18.65.2 44.3	TSTAL TEMP IN RATIO 289.2 1.114 288.8 1.106 288.2 1.089 287.8 1.086 287.8 1.086 287.8 1.086 287.8 1.085 287.8 1.082 287.7 1.078	TOTAL PRESS 10.13 1.288 10.13 1.291 10.13 1.274 10.15 1.269 10.15 1.269 10.14 1.259 10.14 1.259 10.14 1.259 10.14 1.258 10.15 1.265 10.15 1.278
P 25456 88.	#85 VEL 1N OUT 92.9 142.2 96.1 143.9 97.5 143.9 97.5 143.9 97.5 143.1 97.4 142.4 97.5 143.4 97.5 143.6 97.5 143.6 97.5 143.6 97.5 143.6 97.5 143.6	REL VEL (N 0UT 305.7 202.0 300.6 206.2 275.9 127.0 249.0 151.7 241.5 141.2 238.5 135.9 235.1 130.9 231.7 126.7 221.5 127.5 192.9 121.9 183.7 117.8	96.1 100.0 99.3 98.7 98.0 92.3 97.5 88.0 97.5 84.9 97.4 82.3 97.3 81.6 97.5 91.2 97.3 105.3	-0.0 117.9 -0.0 116.0 -0.0 117.2	PED SPEED IN CUT 291.2 289.9 284.8 285.7 257.4 257.7 228.9 251.4 220.9 224.2 217.7 221.4 214.0 218.1 210.5 214.9 198.8 205.0 166.6 178.6 158.1 172.2
6 · 25 4 5 · 21 · 8 · 21 ·	ABS MACH NO 1N OLT 1.275 0.401 1.284 0.408 1.294 0.414 1.289 0.415 1.289 0.410 1.289 0.410 1.289 0.411 1.289 0.425 1.289 0.456 1.277 0.489	REL MACH NO (N OUT 0.904 0.573 0.890 0.585 0.738 0.435 0.716 0.425 0.707 0.390 0.697 0.376 0.687 0.364 0.657 0.367 0.572 0.353 0.544 0.342	IN 0UT 0.275 0.258 0.284 0.284 0.294 0.282 0.291 0.265 0.289 0.252 0.289 0.243 0.289 0.234 0.289 0.234 0.289 0.263 0.289 0.305		MERIC PEAR SS JEL & MACH NO 0.984 .5: 1.041 .297 0.995 .266 0.942 .222 0.903 .2:3 0.973 .2:3 0.973 .197 0.936 .146 1.082 .027
234561.89	PERCENT INC. SPAN MEAN 5.00 9.4 10.00 9.5 30.00 11.1 50.00 15.1 95.00 13.5 57.50 13.7 60.00 13.9 62.50 14.1 70.00 14.5 90.00 15.2 95.00 16.2	SS 6.6 4.5 6.5 2.8 7.0 3.0 7.9 3.4 9.0 4.5 8.1 5.5 8.2 6.5 8.2 6.6 8.2 5.6 7.9 9.3 6.8 7.1	0.471 0.659 0.440 0.711 0.442 0.804 0.524 0.801 0.552 0.794 0.568 0.787 0.582 0.782 0.594 0.782 0.563 0.824	LOSS COEFF TOT PROF 0.263 0.279 0.253 0.251 0.155 0.154 0.163 0.165 0.196 0.196 0.206 0.206 0.215 0.215 0.219 0.219 0.186 0.186 0.069 0.069 0.096 0.096	LOSS PARAM TOT PROF 0.048 0.047 0.042 0.041 0.027 0.027 0.035 0.035 0.035 0.035 0.036 0.036 0.039 0.038 0.039 0.039 0.035 0.035 0.015 0.015 0.018 0.018

## (d) 70 Percent of design speed; reading 2830

RP 1 2 3 4 5 6 7 8 9 10 11	21.811 21.829 19.385 19.601 18.766 19.045	-0.0 37.0 -0.0 36.6 -0.0 39.1 -0.0 42.9 -0.0 45.6 -0.0 47.2 -0.0 48.4 -0.0 48.4 -0.0 45.9 -0.0 45.7	1N 0U 69.9 60.9 68.9 59.9 66.4 58.5 64.2 52.8 63.6 51.2 63.3 50.5 63.0 50.2 62.6 48.8 61.4 44.0 57.5 29.7	TOTAL TEMP IN RATIO 289.0 :.095 288.8 :.089 268.2 :.079 267.8 :.078 267.7 :.080 267.8 :.079 267.9 :.079 267.8 :.077 267.7 :.072 267.7 :.072	TOTAL PRESS IN RATIO 10.11 1.271 10.13 1.276 10.14 1.252 10.14 1.251 10.14 1.249 10.14 1.245 10.14 1.241 10.13 1.248 10.13 1.258 10.13 1.272
P 23456 85	ABS VEL (N CUT 107.1 142.5 110.3 143.9 112.6 135.9 110.8 140.8 110.8 140.8 110.5 142.4 109.7 142.3 109.6 141.6 109.4 142.9 108.8 147.8 108.5 161.0 102.3 171.8	237.4 144.0 227.2 143.1 198.3 129.5	110.3 99.7 109.7 96.7 109.6 94.1 109.4 94.8 108.8 102.6 106.5 112.5	-0.0 85.8 -0.0 95.9 -0.0 101.7 -0.0 104.5 -0.0 106.0 -0.0 106.1 -0.0 106.1	291.8 291.6 291.8 291.6 285.9 264. 257.7 257.9 229.2 231.8 222.3 225.6 218.1 221.8 214.7 218.9 213.7 215.3 199.4 225.6 167.2 199.2 158.7 2.6
RP - 25 4 5 61 8 9 9 1	ABS MACH NO 1N OUT 0.317 0.407 0.327 0.412 0.335 0.390 0.329 0.405 0.328 0.410 0.326 0.409 0.326 0.408 0.325 0.411 0.325 0.411 0.325 0.411 0.325 0.428 0.326 0.409	REL MACH NO 1N OUT 0.922 0.668 0.909 0.658 0.583 0.757 0.491 0.737 0.458 0.717 0.423 0.705 0.414 0.675 0.413 0.589 0.376 0.561 0.363	MERID MACH NO 1N 0.517 0.325 0.327 0.335 0.303 0.329 0.297 0.326 0.275 0.325 0.275 0.325 0.225 0.325 0.325 0.325 0.326 0.304 0.337		MERIC PELC 03 .E. 4 M41-4 03 .063 .259 .048 .249 .0936 .222 .0931 .65 .004 .75 .082 .65 .085 .159 .0866 .128 .0946 .121 .057 .0988

## (e) 70 Percent of design speed; reading 2831

R-25456: 895	24.724 24.615 24.155 24.056 21.811 21.829 19.385 19.601 18.766 19.045 19.451 18.766 18.136 18.486 17.818 18.209 16.850 17.374	-0.0 29.8 -0.0 32.2 -0.0 36.4 -0.0 38.1 -0.0 39.8	3N 00T 68.1 59.9 67.2 60.1 64.4 58.6 62.0 53.0 61.4 50.5 61.0 50.0 60.7 49.7 60.3 48.3 59.1 44.3 55.5 29.6	TOTAL TEMP IN RATIO 268.9 1.083 288.9 1.074 288.3 1.067 287.9 1.068 287.8 1.070 287.8 1.072 287.8 1.072 287.6 1.072 287.7 1.069 287.7 1.070 287.7 1.075	PRESS 1N 92*:0 10.13 1.244 10.13 1.238 10.14 1.223 10.14 1.222 10.14 1.223 10.13 1.218 10.13 1.218 10.13 1.226 10.14 1.226 10.15 1.258
P- 25456 89	ABS VEL 1N OUT 16.7 145.0 119.5 140.9 122.6 153.8 121.2 158.8 121.5 142.6 120.1 141.7 119.6 142.5 119.6 142.5 119.6 142.5 119.6 142.5	REL VEL IN OUT 312.8 246.5 307.7 245.0 284.1 217.0 258.3 185.5 251.6 176.5 248.0 169.5 244.7 162.1 2. 4 160.1 238 157.5 202.0 138.1 192.3 133.3	120.5 112.3 120.1 108.9 119.8 104.9 119.6 106.5 118.4 112.8 114.4 120.2	-0.0 110.3	WHEEL SPEED 1N 0.77 290.2 288.9 283.6 262.4 256.3 256.5 226.1 230.6 221.8 224.1 216.9 220.6 213.3 217.4 209.6 214.2 198.1 204.3 166.5 178.4 157.7 171.5
RP: 254567899111	ABS MACH NO 1N OUT 0.347 0.416 0.355 0.406 0.365 0.386 0.361 0.401 0.359 0.412 0.359 0.412 0.356 0.411 0.352 0.426 0.340 0.474 0.327 0.505	REL MACH NO IN OUT 0.929 0.707 0.914 0.705 0.846 0.626 0.769 0.536 0.749 0.510 0.739 0.490 0.729 0.468 0.719 0.462 0.687 0.456 0.601 0.402 0.572 0.388	MER 10 MACH NO IN 001 0.347 0.355 0.355 0.352 0.365 0.327 0.369 0.324 0.358 0.314 0.357 0.303 0.356 0.352 0.327 0.340 0.349 0.327 0.360		MER: DPEAR SS .EL R MACH NO 1.059 1.21 1.025 1.99 1.924 1.81 1.921 1.48 1.932 1.37 1.906 1.23 1.906 1.23 1.953 1.089 1.050 1.992 1.124 1.967
RP 1 25 4 5 67: 0 9 11	PERCENT INC SPAN MEAN 5.00 5.2 10.00 5.3 30.00 6.6 50.00 8.3 55.00 8.7 57.50 8.9 60.00 9.1 62.50 9.2 70.00 9.8 90.00 11.0	2.4 1.1 2.5 1.9 2.5 3.4 3.1 3.9 3.2 3.5 3.3 4.2 3.3 5.1	D-FACT EFF 0.303 0.779 0.287 0.854 0.320 0.879 0.577 0.864 0.400 0.855 0.421 0.828 0.445 0.800 0.445 0.812 0.425 0.866 0.440 0.918 0.444 0.910	LOSS CCEFF TOT PROF 0.135 0.134 0.083 0.082 0.071 0.071 0.095 0.093 0.107 0.107 0.132 0.132 0.158 0.158 0.151 0.151 0.112 0.112 0.088 0.088 0.113 0.113	LOSS PARAM TOT PROF 0.026 0.025 0.015 0.015 0.012 0.012 0.017 0.017 0.024 0.024 0.024 0.024 0.026 0.026 0.027 0.027 0.021 0.021 0.017 0.017 0.022 0.022

#### (f) 70 Percent of design speed; reading 2832

RP 1 23 4 5 6 7 8 9 9 11 11	24.724 24.615 24.155 24.056 21.811 21.829 19.385 19.601 18.766 19.045 16.451 16.766	-0.0 25.4 -0.0 24.0 -0.0 29.4 -0.0 30.6 -0.0 32.1 -0.0 34.1 -0.0 33.1	IN CUT 66.6 59.7 65.5 60.3 62.5 58.2 59.8 52.9 59.1 50.6 58.7 49.5 58.3 48.8 58.0 47.8 56.7 44.0 53.1 29.7	TOTAL TEMP IN RATIO 289.1 1.366 288.9 1.359 287.9 1.359 287.8 1.361 287.6 1.361 287.7 1.361 287.7 1.361 287.7 1.361 287.7 1.361	TOTAL PRESS 10.09 1.200 10.13 1.19 10.14 1.165 10.14 1.166 10.14 1.92 10.14 1.169 10.14 1.203 10.14 1.203 10.13 1.224 10.12 1.241
P - 254561 8 3	ABS VEL (N 001 126.5 147.2 129.6 140.9 133.7 136.8 130.9 140.9 130.2 144.1 131.6 144.9 131.6 144.9 131.6 151.6 135.2 166.0 135.2 166.0	REL VEL 1N 001 318.1 265.3 312.4 261.5 269.9 235.5 264.6 203.3 257.8 195.5 254.0 189.0 250.8 181.1 247.4 180.2 238.1 176.9 208.4 153.0 198.7 148.0	MERID VEL IN OUT 126.5 133.8 129.6 129.4 133.7 124.2 132.9 122.7 132.2 124.0 131.6 119.3 131.6 127.5 125.2 132.9 119.8 136.3	-0.0 83.8 -0.0 82.4 -0.0 102.7	WHEEL SPEED IN COLT 291.6 290.5 284.3 285.1 257.1 257.3 228.7 231.5 221.2 224.5 217.1 220.8 213.4 217.5 209.7 214.3 199.0 205.2 166.6 178.6 156.5 172.4
R - 254561 89991	ABS MACH NO 1N OUT 0.576 0.426 0.386 0.409 0.399 0.398 0.397 0.409 0.395 0.421 0.395 0.421 0.395 0.421 0.395 0.421 0.395 0.425 0.390 0.441 0.375 0.490 0.357 0.520	REL MACH NO IN OUT 0.946 0.767 0.931 0.758 0.865 0.684 0.790 0.591 0.770 0.568 0.758 0.549 0.749 0.525 0.739 0.523 0.711 0.515 0.621 0.446 0.592 0.432	MERID MACH NO IN OUT 0.576 0.597 0.561 0.395 0.361 0.395 0.366 0.393 0.346 0.392 0.392 0.390 0.370 0.373 0.398 0.357 0.398		MERID PEAR SS JEL 4 MACH NO 1.058 1.78 0.998 1.62 0.929 1.48 0.923 1.20 0.938 1.09 0.931 1.09 0.931 1.094 0.922 1.088 0.975 1.068 1.061 0.975 1.138 0.957
R1 254567 8901	PERCENT INC SPAN MEAN 5.00 3.7 10.00 3.6 30.00 4.7 50.00 6.1 55.00 6.5 57.50 6.6 60.00 6.7 62.50 6.9 70.00 7.3 90.00 8.6 95.00 9.8	0.9 0.9 0.6 2.2 0.6 3.0 0.9 3.7 1.0 3.6 1.0 4.2 1.1 5.2 1.3 8.9	D-FACT EFF  0.239	LOSS COEFF TOT PROF 0.090 0.090 0.062 0.061 0.049 0.049 0.075 0.075 0.080 0.080 0.097 0.097 0.131 0.131 0.122 0.122 0.079 0.079 0.085 0.085 0.110 0.110	LOSS PARAM TOT PROF 0.017 0.017 0.011 0.011 0.009 0.009 0.014 0.014 0.015 0.015 0.018 0.018 0.024 0.024 0.022 0.022 0.015 0.015 0.016 0.016 0.021 0.021

#### (g) 70 Percent of design speed; reading 2917

	RADII	ABS B						TOTAL	
RP	IN OUT		OUT	IN	OUT	IN.	RAT!O	1N	RATIO
1	24.724 24.615		15.9		60.4	209.6		10.09	1.132
3	24.155 24.056		16.1	64.0	60.6	209.2		10.13	1.150
3	21.811 21.829		17.4	61.0	57.9	283.1	1.041	10.14	1.131
4	19.385 19.601	-0.0	22.5	58.1	52.1	237.9		10.13	1.143
5 6 7	18.766 19.045		25.4	57.5	50.3	287.8	1.047	10.14	1.145
6	18.451 18.766	-0.0	24.9	56.9	49.2	207.4	1.049	10.14	1.147
	18.136 18.486		27.2	56.3	46.1	267.7	1.053	10.13	1.149
8	17.818 18.209		27.0	55.9	47.4	227.4	1.052	10.14	1.149
9	16.850 17.574			54.5	43.8	287.6		10.13	1.166
10	14.130 15.146		32.2		29.2		1.059	10.13	1.201
11	13.409 14.587	-0.0	35.4	50.0	23.6	267.6	1.063	10.13	1.209
			_						
	ABS VEL	REL V			D VEL		G VEL		SPEED
RP.	IN OUT		OUT	IN	OUT	IN	OUT	IN	OUT
1	136.6 147 9		88.5	136.6	142.2	-0.0	40.4	292.4	291.1
3	139.7 143.6		81.1		138.0	-0.1	39.8	285.8	284.7
•	142.1 141.4	293.6 2	55.7	142.1		-0.1	42.3	256.8	
	142.7 147.9	270.1 2	22.7	142.7	136.8	-0.1	56.1	229.3	
?	142.2 149.7	263.5 2	15.2	142.2	137.4	-0.1	59.4	221.8	225.1
•	142.4 150.7		09.2				63.5	218.3	222.0
5	143.2 151.2 142.7 151.2		201.6		154.6		69.0	215.0	
ş		254.4 1	99.2	142.7	134.8 141.2 150.3	-0.1	68.5	210.6	215.2
10	142.2 157.6 137.9 177.5	244.8	95.5	142.2	141.2	-0.1	70.1	199.2	
11	152.8 185.6		72.2					166.7	
• •	132.0 103.0	206.5 1	63.5	132.6	149.6	-0.0	106.5	158.1	171.9
	ABS MACH NO	REL MAC	H NO	MERID M	ACH NO			MERID	PEAK SS
RP	IN OUT								
	10	IN	001	IN	GU:			VEL R	MACH NO
			0UT	IN 0.407	0.416			VEL R	
1	0.407 0.432	0.962 0	.842	0.407	0.416			1.041	1.136
1	0.407 0.432 0.417 0.420	0.962 0 0.949 0	.842	0.407	0.416			1.041	1.136
1	0.407 0.432 0.417 0.420 0.425 0.414	0.962 0 0.949 0 0.878 0	.842 .822 .743	0.407 0.417 0.425	0.416 0.404 0.595			1.041 0.988 0.949	1.136
2 3 4	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433	0.962 0 0.949 0 0.878 0 0.808 0	.842 .822 .743 .652	0.407 0.417 0.425 0.427	0.416 0.404 0.595 0.401			1.041 0.988 0.949 0.959	1.136 1.128 1.118 1.098
2 3 4	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.435 0.426 0.438	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0	.842 .822 .743 .652	0.407 0.417 0.425 0.427 0.426	0.416 0.404 0.395 0.401 0.402			1.041 0.988 0.949 0.959 0.966	1.136 1.128 1.118 1.098 1.087
2 3 4	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.435 0.426 0.438	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.781 0	.842 .822 .743 .652	0.407 0.417 0.425 0.427 0.426 0.427	0.416 0.404 0.395 0.401 0.402			1.041 0.988 0.949 0.959	1.136 1.128 1.118 1.098 1.087
1 2 3 4 5 6 7 8	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.781 0 0.774 0	.842 .822 .743 .652 .630 .613 .589	0.407 0.417 0.425 0.427 0.426 0.427	0.416 0.404 0.395 0.401 0.402 0.400 0.393			1.041 0.988 0.949 0.959 0.966 0.959	1.136 1.128 1.118 1.098 1.087 1.083
1 2 3 4 5 6 7 8 9	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.781 0 0.774 0 0.762 0	.842 .822 .743 .652 .630 .613 .589 .582	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414			1.041 0.988 0.949 0.959 0.966 0.959	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046
1 2 3 4 5 6 7 8 9	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.755 0	.842 .822 .743 .652 .630 .613 .589 .582 .573	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414			1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958
1 2 3 4 5 6 7 8 9	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.755 0	.842 .822 .743 .652 .630 .613 .589 .582	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414			1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046
1 2 3 4 5 6 7 8 9	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0	.842 .822 .743 .652 .630 .613 .589 .582 .573 .506	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.441			1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937
1 2 3 4 5 6 7 8 9 10 11	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT ING	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.762 0 0.755 0 0.647 0	.842 .822 .743 .652 .630 .613 .589 .582 .573	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.441	LOSS C		1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937
1 2 3 4 5 6 7 8 9 10 11	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAL	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413 0.397	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.441 0.439	TOT	PROF	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937
1 2 3 4 5 6 7 8 9 10 11	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAD 5.00 2.1	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.772 0 0.753 0 0.647 0 0.617 0	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413 0.397	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.44: 0.439	TOT 0.060	PROF 0.060	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937
1 2 3 4 5 6 7 8 9 10 11 RP 1 2	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAD 5.00 2.1	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.772 0 0.753 0 0.647 0 0.617 0	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.426 0.413 0.597 D-FACT 0.154 0.163	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.44: 0.439 EFF 0.615 0.65	TOT 0.060 0.042	PROF 0.060 0.042	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAD 5.00 2.1 10.00 2.1 30.00 3.1	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.762 0 0.755 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 5 -0.9	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.413 0.397 D-FACT 0.154 0.163 0.184	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.439 EFF 0.615 0.653 0.872	TOT 0.060 0.042 0.045	PROF 0.060 0.042 0.045	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.008	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.008
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAD 5.00 2.1 30.00 3.1 50.00 4.4	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 5 -0.9 4 -0.8	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.429 0.428 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.439 EFF 0.815 0.863 0.872 0.848	TOT 0.060 0.042 0.045 0.067	PROF 0.060 0.042 0.045 0.067	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.008	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAD 5.00 2.1 10.00 2.1 50.00 4.4 55.00 4.4	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 3 -0.8 5 -0.8	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.439 EFF 0.815 0.865 0.872 0.848 0.840	TOT 0.060 0.042 0.045 0.067 0.075	PROF 0.060 0.042 0.045 0.067 0.075	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.008 0.012	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014
1 23 4 5 6 7 8 9 10 11 RP 1 23 4 5 6	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539  PERCENT INC SPAN HEAN 5.00 2.1 10.00 2.1 30.00 3.1 55.00 4.4 55.00 4.4	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 5 -0.9 4 -0.8 5 -0.8 7 -0.9	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249 0.267	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.439 EFF 0.815 0.863 0.872 0.848 0.840 0.816	TOT 0.060 0.042 0.045 0.067 0.075 0.091	PROF 0.060 0.042 0.045 0.067 0.075 0.091	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.008 0.012	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014 0.017
1 23 4 5 6 7 8 9 10 11 RP 1 23 4 5 6 7	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539 PERCENT INC SPAN HEAN 5.00 2.1 10.00 2.1 30.00 3.1 55.00 4.6 57.50 4.6 60.00 4.7	0.962 0 0.949 0 0.878 0 0.808 0 0.789 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 -0.9 -0.8 -0.8 -0.8 -0.8 -0.8 -0.9 -0.9 -0.9 -0.9 -0.8 -0.9 -0.9 -0.9 -0.8 -0.8 -0.8 -0.9 -0.9 -0.8 -0.8 -0.8 -0.9 -0.9 -0.9 -0.8 -0.8 -0.8 -0.9 -0.9 -0.9 -0.8 -0.8 -0.9 -0.9 -0.9 -0.8 -0.9 -0.9 -0.9 -0.8 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249 0.267 0.295	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.459 EFF 0.815 0.865 0.872 0.848 0.840 0.816 0.769	TOT 0.060 0.042 0.045 0.067 0.075 0.091 0.125	PROF 0.060 0.042 0.045 0.067 0.075 0.091 0.123	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.012 0.014 0.017	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014 0.017 0.023
1 23 4 5 6 7 8 9 10 11 RP 1 2 3 4 5 6 7 8	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539  PERCENT INC SPAN HEAN 5.00 2. 10.00 3. 50.00 4. 65.00 4. 60.00 4. 62.50 4.6	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 3 -0.8 5 -0.8 7 -0.9 7 -1.0 8 -1.0	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249 0.267 0.295 0.292	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.439 EFF 0.815 0.863 0.872 0.848 0.840 0.816 0.769 0.775	0.060 0.042 0.045 0.067 0.075 0.091 0.123	PROF 0.060 0.042 0.045 0.067 0.075 0.091 0.123 0.122	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.012 0.014 0.017 0.023	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014 0.017 0.023 0.023
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4 5 6 7 8 9	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539  PERCENT INC SPAN HEAN 5.00 2.1 10.00 2.1 30.00 3.1 50.00 4.4 655.00 4.6 60.00 4.7 62.50 4.6 70.00 5.1	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 1 -0.9 3 -0.8 5 -0.8 7 -0.9 7 -1.0 8 -1.0 -1.2	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV 1.7 2.4 2.7 3.0 3.3 3.4 3.5	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249 0.267 0.295 0.292 0.277	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.394 0.414 0.439 EFF 0.815 0.863 0.848 0.840 0.816 0.769 0.775 0.883	707 0.060 0.042 0.045 0.067 0.075 0.091 0.123 0.122 0.066	PROF 0.060 0.042 0.045 0.067 0.075 0.091 0.123 0.122 0.066	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.012 0.014 0.017 0.023 0.023	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014 0.017 0.023 0.012
1 23 4 5 6 7 8 9 10 11 RP 1 2 3 4 5 6 7 8	0.407 0.432 0.417 0.420 0.425 0.414 0.427 0.433 0.426 0.438 0.427 0.441 0.429 0.442 0.428 0.442 0.426 0.462 0.413 0.521 0.397 0.539  PERCENT INC SPAN HEAN 5.00 2. 10.00 3. 50.00 4. 65.00 4. 60.00 4. 62.50 4.6	0.962 0 0.949 0 0.878 0 0.808 0 0.769 0 0.774 0 0.762 0 0.753 0 0.647 0 0.617 0  CIDENCE N SS 1 -0.7 -0.9 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.9 -0.9 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8	.842 .822 .743 .652 .650 .613 .589 .582 .573 .506 .479 DEV	0.407 0.417 0.425 0.427 0.426 0.427 0.428 0.426 0.413 0.397 D-FACT 0.154 0.163 0.104 0.238 0.249 0.267 0.295 0.292	0.416 0.404 0.395 0.401 0.402 0.400 0.393 0.414 0.441 0.439 EFF 0.815 0.863 0.872 0.848 0.840 0.816 0.769 0.775	0.060 0.042 0.045 0.067 0.075 0.091 0.123	PROF 0.060 0.042 0.045 0.067 0.075 0.091 0.123 0.122	1.041 0.988 0.949 0.959 0.966 0.959 0.940 0.945 0.993 1.090 1.126 LOSS P TOT 0.011 0.008 0.012 0.014 0.017 0.023	1.136 1.128 1.118 1.098 1.087 1.083 1.077 1.068 1.046 0.958 0.937 ARAM PROF 0.011 0.008 0.012 0.014 0.017 0.023 0.023

## (h) 80 Percent of design speed; reading 2814

RP : 254561 85511		007 4.615 4.056 4.829 9.601 9.045 9.766 9.486 9.209	:N -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	007 47.4 44.9 48.0 51.6 54.0 55.3	71.8 71.8 70.7 68.1 66.2 65.6 65.2 64.9 64.4 63.2 59.0	001 61.8 60.2 58.6 52.6 52.5 52.5 52.5 51.1 45.5	291.3 287.6 297.1 287.1 287.1 287.3 286.9 286.8	RATIO 1.133 1.130 1.121	1N 10.36 10.12 10.14 10.14 10.14 10.14 10.14 10.14	PRESS 1.4:3 1.4:3 1.4:9 1.3:35 1.356 1.349 1.343 1.346 1.356 1.356 1.356
P-25456 69	110.2 114.2 118.6 115.7 115.7 115.7 115.7 115.4	EL 001 66.7 67.4 68.5 65.7 63.7 62.7 61.8	317.7 286.9 279.5 275.9 271.4 268.0 256.0 223.8	VEL 001 238.6 238.5 205.8 170.1 158.4 146.0 143.1 141.9 138.2 155.2	114.2 118.6 116.0 115.7 115.2 115.6 115.4	00T 112.8 118.5 107.3 103.0 96.3 92.7 89.4 89.9	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1	122.7 118.2 119.5 129.6 132.4 133.7 134.9 135.6 134.3	1N 334.4 326.4 294.7 262.3	
G - 254 5 5 6 8 9 9 9 1 1	. 525 . 538 . 355 . 346 . 545 . 545 . 544 . 544 . 544	H NO 017 1.467 1.455 1.466 1.463 1.463 1.463 1.463 1.463 1.463 1.463 1.463 1.463	REL M 1.038 1.023 0.946 0.855 0.833 0.822 0.808 0.798 0.763 1.667 0.634	OUT	0.525 0.358 0.353 0.346 0.345 0.345 0.344 0.344	0.01 0.516 0.555 0.504 0.265 0.274 0.264 0.255 0.256 0.264 0.264 0.340 0.365			E. 4	443 442 442 456 395 36 375 36 375 36
RP 23456789	PERCENT SPAN 5.00 10.00 30.00 50.00 55.00 57.50 62.50 70.00 93.00	INC III MEAN 8.9 8.9 10.3 12.4 12.9 13.1 13.3 13.4 13.6 14.5 15.6	DENCE 55 6.1 5.8 6.2 7.4 7.5 7.5 7.6 7.2 8.2	3.0 2.0 3.4 3.6 5.6 7.6 6.7 7.6 6.8	D-FACT 0.454 0.456 0.478 0.542 0.571 0.586 0.602 0.606 0.584 0.518	0.778 0.793 0.793 0.790 0.790 0.791 0.764 0.799 0.909 0.929	2.355 C ToT 0.178 0.166 0.184 0.201 0.226 0.237 0.236 0.237 0.243 0.114 0.103	DEFF PROF 0.154 0.169 0.212 0.223 0.223 0.235 0.242 0.114 0.103	2055 2015 2015 2015 2015 2015 2015 2015	DROF 0.029 0.029 0.035 0.035 0.040 0.040 0.040

## (i) 90 Percent of design speed; reading 2820

RP 1 234567.89.011		ABS BETAN IN 001 -0.1 28. -0.1 26. -0.1 33. -0.0 34. -0.1 34. -0.0 35. -0.0 35. -0.0 38. -0.0 38.	IN OUT 5 65.0 59.5 7 63.9 60.4 8 60.9 57.2 9 58.0 50.4 8 60.9 1 56.4 51.0 4 56.0 50.2 4 54.7 45.2 9 50.9 31.2	TOTAL TEMP IN RATIO 289.6 1.126 289.5 1.112 288.5 1.104 287.7 1.111 287.6 1.106 287.7 1.104 287.4 1.103 287.4 1.108 287.4 1.108 287.4 1.108	
P - CH 45-01 8-0	ABS VEL IN OUT 177-2 191.9 181.2 182.3 185.9 181.4 185.7 192.0 185.6 183.8 185.2 181.6 184.4 178.1 184.1 179.1 182.9 192.5 175.4 212.5 167.9 226.1	REL VEL (N OUT 418.7 332.6 412.0 329.4 382.1 295.4 350.0 250.6 342.6 243.1 337.8 257.6 338.6 232.3 329.2 227.3 316.4 223.2 278.4 191.5 265.1 165.4	181.2 162.8 185.9 163.0 185.7 159.3 185.6 152.4 185.0 149.9 184.4 146.2 184.1 145.9 182.9 157.2 175.4 163.8	-0.2 102.8 -0.1 103.9 -0.2 107.6 -0.1 132.3	
F1 28.45.07.89.01	ABS MACH NO IN 0.17 0.534 0.546 0.547 0.521 0.563 0.521 0.563 0.528 0.561 0.522 0.559 0.514 0.558 0.515 0.554 0.550 0.530 0.610 0.537 0.655	REL MACH NO IN OUT 1.262 0.944 1.244 0.941 1.158 0.846 1.062 0.715 1.039 0.696 1.012 0.66 0.999 0.655 0.959 0.645 0.842 0.555 0.800 0.53	IN OUT  4 0.554 0.480  1 0.547 0.465  8 0.563 0.459  9 0.563 0.458  9 0.563 0.438  4 0.561 0.431  7 0.559 0.420  5 0.558 0.420  5 0.554 0.454  5 0.530 0.474		MERIC PEAK SS VEL R MACH NO 0.952 : 374 0.899 : 362 0.861 : 363 0.858 : 376 0.810 : 390 0.792 : 398 0.792 : 403 0.860 : 375 0.860 : 375 0.934 : 261 1.012 : 1.254
RP 1 234 567 89011	PERCENT INCOMES PAN MEAN 5.00 2.0 10.00 2.0 30.00 3.1 50.00 4.2 55.00 4.5 57.50 4.6 60.00 4.8 62.50 4.9 70.00 5.3 90.00 6.4 95.00 7.6	SS -0.7 0.3 -1.0 2.2 -1.0 2.1 -1.0 1.3 -0.9 4.2 -0.9 6.4 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5 -0.9 6.5	0.289 0.763 0.274 0.814 0.502 0.870 0.377 0.842 0.378 0.810 0.383 0.812 0.391 0.793 0.396 0.804 0.384 0.887 0.419 0.885	LOSS COEFF TOT PROF 0.143 0.105 0.105 0.070 0.075 0.050 0.107 0.089 0.127 0.110 0.127 0.111 0.140 0.124 0.134 0.119 0.082 0.073 0.108 0.108 0.139 0.139	LOSS PARAM TOT PROF 0.027 0.020 0.019 0.013 0.014 0.009 0.020 0.017 0.023 0.020 0.025 0.020 0.025 0.022 0.024 0.021 0.015 0.013 0.020 0.020 0.026 0.026

#### (j) 90 Percent of design speed; reading 2821

RP 1 2 3 4 5 6 7 8 9 10 11	17.818 18.209 16.850 17.374 14.130 15.146	-0.0 43.2	IN 00T 65.8 58.4 64.7 59.6 61.7 57.4 59.0 51.0 58.3 51.1 57.9 50.1 57.6 50.0 57.2 49.1 56.0 44.9 52.5 30.8	TOTAL TEMP IN RATIO 289.7 1.155 289.3 1.136 288.4 1.119 287.7 1.122 287.5 1.119 287.6 1.119 287.4 1.118 287.4 1.116 287.4 1.115 287.4 1.117 287.4 1.117	1N RATIO 10.05 1.484 10.12 1.450 10.15 1.424 10.14 1.424 10.14 1.398 10.14 1.399 10.14 1.390
RP 1 23 4 5 6 1 8 9	ABS VEL :N OUT 169.9 197.4 174.4 185.9 178.9 179.4 177.7 188.5 176.5 183.7 176.5 183.7 176.3 181.9 175.1 181.5 175.1 181.5 175.2 224.1			-0.1 141.6	
RP 1 25 4 5 6 7 8 9 10 11	ABS MACH NO 1N OUT 0.5:1 0.555 0.526 0.526 0.541 0.511 0.538 0.539 0.536 0.521 0.534 0.525 0.534 0.520 0.529 0.519 0.524 0.541 0.500 0.596 0.479 0.647	REL MACH NO IN OUT 1.246 0.869 1.229 0.877 1.142 0.792 1.045 0.670 1.020 0.650 1.006 0.634 0.995 0.613 0.977 0.604 0.937 0.589 0.822 0.506 0.781 0.486	MERID MACH NO IN OUT 0.511 0.455 0.526 0.444 0.541 0.427 0.538 0.422 0.536 0.408 0.534 0.406 0.534 0.394 0.529 0.395 0.524 0.417 0.500 0.435 0.479 0.452		MERIC PELF SS FEL R MACH NG 0.953 1.388 0.900 1.376 0.838 1.377 0.831 1.414 0.806 1.416 0.806 1.424 0.782 1.429 0.789 1.414 0.839 1.386 0.909 1.273 0.984 1.242
RP 1 23 4 5 6 7 8 9 10 11	PERCENT INCOMES SPAN MEAN 5.00 2.9 10.00 2.8 30.00 3.9 50.00 5.3 55.00 5.6 57.50 5.8 60.00 6.0 62.50 6.1 70.00 6.6 90.00 8.0 95.00 9.0	DENCE DEV  SS  0.1 -0.4  -0.2 1.4  -0.2 2.2  0.1 1.8  0.2 4.2  0.2 4.3  0.2 5.4  0.3 5.8  0.4 6.2  0.7 9.9  1.5 7.1	0.356 0.772 0.329 0.626 0.351 0.895 0.423 0.874 0.423 0.844 0.433 0.849 0.450 0.836 0.441 0.897 0.473 0.894 0.484 0.886	LOSS COEFF 101 PROF 0.167 0.128 0.117 0.082 0.070 0.044 0.095 0.076 0.119 0.00 0.117 0.099 0.130 0.112 0.130 0.115 0.085 0.075 0.112 0.111 0.139 0.139	LOSS PARAM TOT PROF 0.033 0.025 0.022 0.015 0.012 0.008 0.018 0.014 0.021 0.018 0.021 0.018 0.023 0.020 0.023 0.021 0.016 0.014 0.021 0.021 0.021 0.021 0.027 0.027

## (k) 90 Percent of design speed; reading 2822

RP: 23456789111	RADII IN 24.724 24 24.155 24 21.811 21 19.385 19 18.766 19 18.451 18 18.136 18 17.818 18 16.850 17 14.130 15 13.409 14	007 .615 .829 .601 .045 .766 .766 .209	-0.1 -0.1 -0.1 -0.1 -0.0 -0.1 -0.1	37.4 37.5 42.3 42.9 44.6 46.4	1N 67.1 66.0 63.0 60.4 59.8 59.5 59.1 58.8 57.7 54.4	BETAM OUT 58.8 59.3 57.2 51.3 51.2 50.4 50.0 49.1 45.8 30.5 20.9	1N 290.5 289.8 288.2 267.5 267.4 287.3 287.2 287.2 287.3 287.3	1.153 1.133 1.131 1.130 1.131	10.15 10.15 10.15 10.15 10.15 10.15 10.15 10.15	. 425 1.425 1.425 1.425
P: 25456 6::	159.9 1 164.3 1 170.2 1 168.5 1 167.4 1 166.5 1 164.8 1 164.8 1 164.4 2	00T 97.3 88.7 81.4 87.6 83.1 83.5 82.6 85.1	1N 410.1 404.3 374.6 341.1 332.4 327.8 322.9 318.0 304.9 265.6	213.8 205.0 195.9 195.2 188.1	170.2 168.5 167.4 166.5 165.6 164.8 163.1 154.4	0UT 150.8 150.0 143.9 138.8 134.0 130.7 125.9 127.8	-0.2 -0.1 -0.1 -0.1 -0.1 -0.2	00T 127.2 114.5 110.4 126.1 124.7 129.0 132.2 130.3	1N 377.5 369.2 533.6 296.4 287.0 282.2 277.0 271.8 257.5 215.9	291.3 287.1 282.4 277.8 265.5
P. 254561 69011	0.495 0.515 0.508 0.505 0.502 0.499 0.497 0.491 0.464	0.1 .550 .529 .514 .534 .520 .522 .519 .519	1.228 1.213 1.129 1.029 1.003 0.989 0.974 0.959 0.919	0.810 0.825 0.753 0.632 0.608 0.583 0.557	0.508 0.505 0.502	0.420 0.421 0.428 0.395 0.381 0.371 0.358 0.364 0.374				PE17 SS M46H N; .416 .418 .425 .445 .459 .459 .459 .439 .439 .439 .439
R - 25456-895	PERCENT SPAN 5.00 10.00 30.00 50.00 55.00 57.50 60.00 62.50 70.00 90.00	INCII MEAN 4.1 4.2 5.2 6.7 7.1 7.3 7.5 7.7 8.3 9.9	DENCE 55 1.4 1.1 1.5 1.6 1.7 1.8 1.9 2.0 2.7	DEV -0.0 1.2 2.1 2.2 4.6 5.7 7.1 9.7 6.3	D-FACT 0.408 0.376 0.389 0.459 0.466 0.487 0.509 0.500 0.496 0.518	0.768 0.830 0.891 0.885 0.851 0.859 0.858 0.858 0.898 0.898	LOSS C TOT 0.188 0.128 0.080 0.125 0.139 0.147 0.147 0.124 0.118	CEFF PROF 0.147 0.091 0.051 0.051 0.105 0.105 0.118 0.142 0.131 0.114	LOSS P 101 0.037 0.024 0.014 0.023 0.025 0.025 0.026 0.023	PROF 0.029 0.019 0.019 0.019 0.021 0.026 0.024 0.021

#### (1) 90 Percent of design speed; reading 2824

RP: 254501 89011	RADII IN 007 24.724 24.615 24.155 24.056 21.811 21.829 19.385 19.601 18.766 19.045 18.451 18.766 18.136 18.486 17.818 18.209 16.850 17.374 14.130 15.146 13.409 14.587	-0.1 44. -0.1 41. -0.1 48. -0.1 51. -0.1 52. -0.1 53. -0.1 53. -0.1 51.	1N 001 5 69.0 59.2 8 68.0 58.7 5 65.1 57.8 3 62.9 53.0 2 62.4 52.6 8 62.1 52.3 5 61.8 51.8 9 61.5 50.0 1 60.4 45.6 1 56.6 30.7	IN RATIO 291.4 1.179 290.9 1.164 288.1 1.141 287.1 1.142 287.0 1.143 287.0 1.143 286.9 1.143 286.9 1.142 286.9 1.136 286.8 1.128	10.15 1.446 10.15 1.497
P - 254501 80	ABS VEL (N OUT) 145.1 198.0 149.0 193.8 154.4 179.5 151.6 183.6 150.3 182.0 149.3 181.2 148.4 181.8 148.0 184.2 146.1 186.8 142.1 202.4 136.3 219.9	REL VEL 1N 00T 403.9 275.3 397.4 278.0 366.7 252.4 332.9 203.3 324.0 187.8 318.8 179.2 314.4 171.7 309.6 168.7 296.0 167.8 258.3 157.3 245.6 152.8	MERID VEL IN OUT 145.1 141.1 149.0 144.5 154.4 134.3 151.6 122.2 150.3 114.1 149.3 109.5 148.4 106.2 148.0 108.5 146.1 117.4 142.0 135.2 136.3 142.6	-0.1 144.4 -0.1 147.5 -0.1 148.9 -0.1 145.3 -0.1 150.7	WHEEL SPEED 1N 001 376.9 375.2 368.2 366.7 332.5 332.8 296.3 299.6 286.9 291.1 281.5 286.3 277.1 282.4 272.1 278.1 257.3 265.2 215.6 231.1 204.2 222.1
RF: 254561.89111	485 MACH NO IN OUT 3.432 3.549 0.444 0.541 0.463 0.506 0.455 0.519 0.448 0.512 0.446 0.514 0.444 0.521 0.446 0.531 0.426 0.580 0.408 0.632	REL MACH NO 1N OUT 1.202 0.763 1.185 0.775 1.101 0.712 1.000 0.575 0.973 0.531 0.957 0.506 0.944 0.485 0.930 0.477 0.74 0.451 0.735 0.439	MERID MACH NO IN OUT 0.432 0.391 0.444 0.405 0.309 0.446 0.309 0.444 0.307 0.439 0.334 0.426 0.307 0.408 0.410		MERIC PELF SS JEL R MACH NO 0.973 1.459 0.970 1.452 0.806 1.523 0.759 1.509 0.755 1.497 0.716 1.492 0.753 1.461 0.804 1.446 0.952 1.309 1.047 1.274
RP 1 2 3 4 5 6 1 8 9 5 1 1	PERCENT INC SPAN MEAN 5.00 6.0 10.00 6.1 30.00 7.3 50.00 9.2 55.00 9.7 57.50 9.9 60.00 10.2 62.50 10.4 70.00 11.0 90.00 12.1 95.00 13.1	3.5 0.4 3.1 0.5 3.2 2.7 4.0 3.9 4.2 5.6 4.3 6.5 4.5 7.2 4.5 6.6	0.448 0.773 0.420 0.829 0.420 0.861 0.512 0.820 0.547 0.795 0.567 0.779 0.589 0.781 0.563 0.818 0.523 0.902 0.525 0.909	LOSS COEFF TOT PROF 0.195 0.151 0.140 0.099 0.111 0.078 0.163 0.132 0.193 0.167 0.213 0.190 0.223 0.292 0.216 0.200 0.188 0.177 0.122 0.122 0.129 0.129	LOSS PARAM TOT PROF 0.030 0.029 0.027 0.019 0.020 0.014 0.029 0.024 0.034 0.029 0.037 0.035 0.030 0.035 0.039 0.035 0.034 0.032 0.035 0.035

## (m) 90 Percent of design speed; reading 2839

RP 1 2 3 4 5 6 7 8 9 10 11	RAD1 IN 24.724 2 24.155 2 21.811 2 19.385 1 18.766 1 18.451 1 18.136 1 17.818 1 16.850 1 14.130 1	0UT 24.615 24.056 21.829 19.601 19.045 18.766 18.486 18.209 17.374	-0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0	BETAM 0UT 46.6 44.1 45.9 52.9 55.1 56.7 56.5 52.5 48.6 49.9	1N 70.2 69.3 66.6 64.6 64.1 63.8 63.5 63.5 63.2 61.9	BETAM OUT 60.2 58.9 58.7 53.3 53.1 52.9 52.2 50.8 45.7 30.7 20.9	1N 292.3 291.3 287.9 287.0 286.8 286.7 286.8 286.9 286.6	RAT:0 1.179 1.168 1.148 1.150 1.148 1.146 1.145 1.144 1.138 1.128 1.135	10.05 10.09 10.15 10.15 10.15 10.15	.488 1.475 1.457 1.450 1.445 1.445 1.446
Q - 254561 89	138.2 143.5 139.5 138.2 137.3 136.9 136.6 135.1	VEL 0UT 194.1 193.6 178.0 185.1 182.7 181.5 182.9 186.3 201.3 219.8	IN 398.8 391.9 361.1 325.7 316.5 312.1 307.5 303.3 290.2 253.6	VEL 0UT 268.0 269.0 238.5 186.8 174.1 162.9 160.0 162.3 154.9 151.4	143.5 139.5 138.2 137.7 137.3 136.9 136.6	VEL CUT 133.3 139.0 124.0 111.6 104.7 101.4 99.7 101.0 113.4 133.2 141.5	-0.0 -0.0 -0.0 -0.0 -0.0	0 VEL 0UT 141.1 134.8 127.8 147.7 149.8 150.8 151.7 152.4 147.9 151.0 168.1	WHEEL IN 375.2 366.7 331.3 294.3 284.7 280.1 275.1 270.6 256.0 214.7 204.1	297.5 288.9 284.6 283.4
RP: 234567.89011	0.411 0.430 0.418 0.414 0.413 0.411	0.536 0.536 0.539 0.501 0.522 0.516 0.513 0.513 0.517 0.529 0.577	IN 1.182 1.165 1.081 0.976 0.948 0.935 0.921	0.740 0.740 0.748 0.671 0.527 0.491 0.475 0.460 0.452 0.460 0.444 0.435	MERID M 1N 0.400 0.411 0.430 0.418 0.414 0.413 0.411 0.410 0.409 0.404 0.387	0.1 0.368 0.387 0.349 0.315 0.295			MER: D 0.986 0.055 0.864 0.800 0.757 0.737 0.738 0.830 0.830 0.986 1.092	PE44 SS M46H No . 486 . 512 . 513 1.526 . 518 . 516 1.49 1.459 1.285
RP 1 2 3	PERCENT SPAN 5.00 10.00	INC II MEAN 7.3 7.5	DENCE SS 4.5 4.5	DEV 1.4 0.7	0.461 0.440	EFF 0.766 0.810	LOSS C TOT 0.205 0.162	OEFF PROF 0.158 0.118	LOSS P TOT 0.030 0.031	PROF 0.030 0.025

## (n) 100 Percent of design speed, reading 2817

P - 254561-899	24.724 24.615	-0.1 44.7 -0.1 44.5 -0.1 48.4 -0.1 50.2 -0.1 52.3 -0.1 53.2 -0.1 52.3 -0.1 50.4 -0.0 51.0	66.1 59.6 67.2 56.9 61.4 51.6 60.9 51.7 60.5 51.6 60.1 50.6 59.6 48.7 58.7 45.2 55.5 30.9	269.9 .244 269.5 1.226 269.5 1.226 269.5 1.26 261.5 1.6 261.6 1.7 261.2 1.74 291.4 1.65 281.2 1.63 261.3 1.69	PRESS 91 15 15 15 15 15 15 15 15 15 15 15 15 15
P. 25450 89	ABS VEL :N OUT 16 . 3 218.8 :1 . 3 217.4 :1 . 5 204.7 :1 . 6 . 4 213.2 :1 . 6 . 4 213.2 :1 . 6 . 213.5 :1 . 9 216.3 :2 . 5 217.2 :6 . 6 243.3	REL VEL 1N 0UT 448.5 291.3 441.5 295.8 438.0 267.5 371.7 222.7 362.2 210.0 357.1 198.9 352.4 191.8 347.4 190.9 332.3 187.4 268.6 162.2 274.9 161.1	177.5 146.0 177.7 157.8 176.4 150.1 175.9 125.6 175.7 121.7 174.9 125.9 172.5 152.0	-0.2 155.0 -0.2 156.1 -0.2 160.1 -0.2 163.0 -0.2 163.0 -0.2 159.7 -0.1 171.6	N-EEL SPEED :N 0.7 416.0 414.2 406.0 405.7 367.2 367.5 326.3 329.9 310.6 315.9 310.6 315.9 300.0 306.6 283.9 292.7 257.0 254.9 225.0 245.7
P 23456189011	ABS MACH NO IN OUT 0.502 0.595 0.515 0.596 0.536 0.570 0.537 0.581 0.533 0.569 0.532 0.566 0.531 0.569 0.529 0.578 0.521 0.584 0.492 0.627 0.471 0.694	REL MACH NO 1N 0UT 1.347 0.791 1.328 0.811 1.233 0.745 1.124 0.624 1.096 0.588 1.090 0.557 1.066 0.537 1.051 0.536 1.004 0.528 0.870 0.460 0.827 0.459	0.492 0.395		XER: DPEAR SS 10. 4 X104 NO 10.875 1.56 1.902 1.552 1.823 1.53 1.776 1.535 1.738 1.542 1.703 1.544 1.693 1.546 1.720 1.551 1.852 1.437 1.967 1.404
RP: 25456189	PERCENT INC. SPAN MEAN 5.00 5.2 10.00 5.3 30.00 6.4 50.00 7.7 55.00 8.2 57.50 8.3 60.00 8.5 62.50 8.7 70.00 9.3 90.00 11.0	SS 2.4 1.0 2.3 0.3 2.5 2.6 2.7 4.7 2.6 5.7 2.8 6.0 2.9 5.4 3.1 6.5 3.8 10.0 4.7 5.4	D-FACT EFF  0.488 0.725 0.458 0.773 0.462 0.855 0.526 0.863 0.545 0.829 0.571 0.811 0.586 0.805 0.581 0.823 0.563 0.857 0.573 0.888 0.564 0.906	LOSS COEFF TOT PROF 0.267 0.181 0.211 0.131 0.128 0.065 0.130 0.082 0.166 0.120 0.197 0.144 0.197 0.155 0.180 0.139 0.150 0.111 0.143 0.134 0.136 0.131	LOSS PARAM TOT PROF 0.051 0.034 0.041 0.025 0.023 0.012 0.024 0.015 0.030 0.022 0.035 0.025 0.035 0.027 0.035 0.027 0.035 0.027 0.035 0.025 0.027 0.020 0.027 0.025

#### (o) 100 Percent of design speed; reading 2818

RP : 254 567 89111	RAD: 1N 24.724 2 24.155 2 21.811 2 19.385 1 18.766 1 18.451 1 18.136 1 17.818 1 16.850 1 14.130 1 13.409 1	0UT 2.615 4.056 1.829 9.601 9.045 8.766 8.486 8.209 7.374 5.146	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	BETAM OUT 37.8 33.7 35.2 41.3 41.4 42.1 43.1 42.7 40.5 43.4 46.6	1N 65.2 64.2 61.2 58.3 57.6 57.4 56.9 56.4 55.1	59.1 59.6 57.1 51.3 53.1 53.4 53.2 51.6 45.6 35.3 22.9	289 4 289 4 288 4 287 8 287 6 287 6 287 5 287 5	TEMP .199 1.173 1.155 1.146 1.143 1.142 1.141 1.159 1.157	10.12 10.12 10.12 10.13 10.13 10.13	1.495
P - 254561 80	197.5 202.8 202.5 201.8 199.6 199.6	001 214.6 205.7 200.2 207.1 193.5 189.8 188.0 191.2 205.6 219.3	420.6 365.0 375.2 369.9 365.5 380.6 346.9	0UT 330.4 338.2 301.4 248.9 242.0 256.1 229.1 226.0 223.4 190.7	202.3 200.8 199.6 199.8 199.5 198.7 189.8	0 VEL 169.6 171.1 163.5 155.6 145.2 140.9 137.3 140.5 156.4 159.4	-0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2	0 VEL 0UT 131.5 114.3 115.5 136.7 127.9 127.1 128.4 129.7 133.5 150.6 175.6	1N 416.8 407.4 368.3 327.4 316.7 311.3 305.9 300.1 284.2 238.2	351.0 321.4 316.6 311.6 306.7 295.0 255.3
SP 234561.89111	0.585 0.599 0.617 0.613 0.608 0.609 0.608 0.606 0.577	CH NO 0.595 0.575 0.564 0.586 0.547 0.537 0.532 0.542 0.629 0.694	IN 1.393 1.375 1.282 1.174 1.144 1.128 1.115 1.099 1.058		MERID M 1N 0.585 0.599 0.617 0.613 0.608 0.609 0.608 0.577 0.551	0.478 0.478 0.461 0.440 0.411 0.399				PELK 55 MACH NO 1.516 1.495 1.466 1.466 1.467 1.468 1.467 1.465 1.467
RP 1 2 3 4 5 6 7 8 9 11 11	PERCENT SPAN 5.00 10.00 30.00 50.00 55.00 57.50 60.00 62.50 70.00 90.00 95.00	INCI MEAN 2.3 3.4 4.6 5.0 5.2 5.3 5.7 7.0	DENCE SS -0.5 -0.7 -0.6 -0.5 -0.4 -0.5 -0.6 -0.6	DEV 0.3 1.4 2.0 2.2 6.1 7.5 8.6 8.2 6.8 12.4 8.3	D-FACT 0.389 0.346 0.375 0.460 0.454 0.460 0.472 0.473 0.458 0.466 0.509	0.727 0.806 0.863 0.863 0.803 0.803 0.800 0.789 0.805 0.805 0.887 0.872	LOSS C TOT 0.218 0.143 0.100 0.129 0.156 0.158 0.168 0.158 0.102 0.115	OEFF PROF 0.137 0.067 0.042 0.087 0.117 0.121 0.133 0.124 0.074 0.105 0.150	LOSS P TOT 0.042 0.027 0.018 0.024 0.027 0.027 0.028 0.027 0.019 0.021	PROF 0.027 0.012 0.008 0.016 0.020 0.020 0.022 0.021 0.013 0.019 0.029

# (p) 100 Percent of design speed; reading 2819

RP 1 25 4 5 6 7 8 9 10 11		ABS BETAM IN OUT -0.1 30.1 -0.0 28.1 -0.1 36.1 -0.1 36.1 -0.1 36.1 -0.1 36.1 -0.1 36.1 -0.1 36.1 -0.1 36.1 -0.1 34.1	IN OUT 64.8 60.9 63.9 60.4 60.9 57.9 57.8 51.1 57.0 54.5 7 56.6 54.9 55.7 53.0 54.4 46.1 50.6 31.8	287.5 1.129	IN R4110 10.07 1.429 10.12 1.432 10.14 1.415 10.14 1.420 10.15 1.345 10.14 1.332 10.15 1.331 10.14 1.339 10.14 1.408 10.14 1.458
254561 8911	ABS VEL (N OUT 196.1 202.0 199.9 200.4 204.8 196.0 205.6 186.8 204.9 181.9 204.8 181.0 204.4 184.5 205.6 185.9 205.6 185.9 205.6 185.9 205.6 185.9 205.6 185.9 205.6	REL VEL IN OUT 461.3 359.8 453.8 357.4 421.0 321.5 386.2 265.8 377.7 259.4 572.5 256.7 367.9 250.7 363.0 245.5 349.4 244.4 508.4 212.9 293.4 202.7	MERID VEL IN OUT 196.1 174.9 199.9 176.5 204.8 171.0 205.6 150.8 204.9 147.7 204.8 145.8 204.4 147.6 205.5 169.4 195.9 180.9 187.1 183.9	-0.2 110.2 -0.2 106.2 -0.2 107.3 -0.2 110.3 -0.2 116.5 -0.2 142.9	NHEEL SPEED IN OUT 417.3 415.5 415.5 407.2 405.5 367.7 368.1 326.6 530.2 516.7 321.4 510.9 316.2 515.4 311.3 205.8 316.4 283.9 292.7 258.1 255.2 225.8 245.6
P : 25.4 5 6 . 8 9 11 11	485 MACH NO (N OUT 0.595 0.570 0.608 0.568 0.625 0.559 0.629 0.592 0.628 0.516 0.624 0.526 0.624 0.526 0.622 0.591 0.597 0.666 0.568 0.705	REL MACH NO IN OUT 1.400 1.015 1.379 1.013 1.284 0.917 1.180 0.759 1.154 0.740 1.138 0.733 1.124 0.716 1.109 0.701 1.067 0.703 0.940 0.615 0.891 0.585	MERID MACH NO IN OUT 0.595 0.495 0.608 0.500 0.625 0.488 0.629 0.476 0.628 0.450 0.626 0.416 0.624 0.422 0.624 0.422 0.622 0.487 0.597 0.523 0.568 0.531		MEA:U PELV 13 
RP.	PERCENT INCI	DENCE DEV	D-FACT EFF	LOSS COEFF	LOSS PARAM

## (q) 100 Percent of design speed; reading 2914

8P 1 2 3 4 5 6 7 8 9 11	24, 724, 24, 615 24, 155, 24, 056 21, 811, 21, 829 19, 385, 19, 601 18, 766, 19, 045 18, 451, 18, 766 18, 136, 18, 486 17, 818, 18, 209 16, 850, 17, 374	-0.0 42.4 -0.0 46.3 -0.0 46.6 -0.0 48.3 -0.0 49.6	1N OUT 66.7 59.4 65.7 58.9 62.7 57.0 60.0 51.5 59.4 51.6 59.0 51.1 58.6 50.9 58.2 49.3 57.0 44.5 53.7 33.0	TOTAL TEMP IN RATIO 289.5 1.256 289.1 1.211 288.2 1.180 287.7 1.168 287.7 1.168 287.7 1.167 287.6 1.165 287.7 1.159 287.5 1.155 287.5 1.165	TOTAL PRESS IN RATIO 10.08 1.752 10.11 1.720 10.14 1.656 10.14 1.569 10.14 1.569 10.14 1.569 10.14 1.569 10.14 1.566 10.14 1.566 10.14 1.566
P-25456 85	185 VEL 179.6 218.2 183.7 213.2 189.5 203.1 188.8 207.9 187.4 201.8 187.5 201.5 186.4 202.5 186.4 202.5 186.4 202.5 186.6 242.9	REL VEL IN OUT 453.6 302.2 446.8 307.5 413.7 275.4 370.0 231.0 367.9 222.2 363.5 213.8 358.3 205.5 354.0 203.7 339.3 198.9 297.0 167.8 282.5 163.7	186.4 152.8	-0.1 157.0 -0.1 150.2 -0.1 147.2 -0.1 150.3 -0.1 152.4 -0.1 152.9	W-EEL SPEED 1N 00T 416.4 414.6 407.2 405.5 367.7 368.1 327.4 331.1 316.6 321.3 511.5 316.8 305.9 311.8 300.9 307.5 284.6 293.4 239.2 256.3 226.7 246.6
25.45.61.89	485 MACH NO 2N 007 0.542 0.596 0.555 0.588 0.575 0.567 0.573 0.564 0.569 0.567 0.568 0.566 0.566 0.562 0.566 0.570 0.560 0.592 0.532 0.616 0.509 0.693	REL MACH NO IN OUT 1.368 3.825 1.351 0.848 1.255 0.769 1.148 0.649 1.117 0.624 1.103 0.600 1.087 0.577 1.074 0.573 1.029 0.562 0.898 0.477 0.852 0.467	MERIO MACH NG (N OUT 0.542 0.421 0.555 0.438 0.575 0.418 0.573 0.404 0.569 0.388 0.566 0.377 0.566 0.364 0.566 0.372 0.560 0.401 0.532 0.400 0.509 0.437		MEA: PELV 05 16. 4 M20-17 1656 553 1.865 524 1.757 516 1.767 517 1.767 517 1.767 517 1.768 521 1.799 1.427 1.999 1.392
RP 1 2 3 4 5 6 7 8 9	PERCENT INCO SPAN MEAN 5.00 3.8 10.00 3.9 30.00 4.9 50.00 6.3 55.00 6.7 57.50 6.8 60.00 7.0	DENCE DEV SS 1.0 0.6 6.8 0.7 0.8 1.9 1.1 2.4 1.2 4.6 1.3 5.3 1.3 6.3	D-FACT EFF 0.462 0.722 0.429 0.796 0.445 0.864 0.508 0.872 0.512 0.844 0.530 0.836 0.546 0.821	LOSS COEFF TOT PROF 0.25T 0.174 0.178 0.101 0.115 0.054 0.116 0.070 0.143 0.101 0.152 0.112 0.169 0.131	LOSS PARAM TOT PROF 0.049 0.055 0.054 0.019 0.021 0.015 0.021 0.015 0.026 - 0.018 0.027 0.025

TABLE VII. - Concluded,
(r) 100 Percent of design speed; reading 2918

RP 1 2 3 4 5 6 6 7 8 9 10 11	RADII IN OUT 24.724 24.615 24.155 24.056 21.611 21.829 19.335 19.601 18.766 19.045 18.451 18.766 18.136 18.486 17.818 15.239 16.850 17.374 14.130 15.146 13.409 14.587	ABS BETAM IN OUT -0.0 43.1 -0.0 38.9 -0.0 40.6 -0.0 45.4 -0.0 45.6 -0.0 47.2 -0.0 45.6 -0.0 49.6	1N 007 65.9 59.0 65.0 58.9 62.0 57.2 7 59.3 51.5 4 58.6 51.8 5 58.3 51.2 7 57.9 51.3 2 57.6 50.0 56.4 44.8 5 52.9 32.3	TOTAL TEMP IN RATIO 289.3 1.227 239.2 1.198 228.3 1.173 227.8 1.166 287.6 1.162 287.2 1.161 287.6 1.161 287.3 1.158 267.5 1.154 287.6 1.149 287.6 1.162	IN RATIO 10.09 1.707 10.12 1.692 10.14 1.629 10.14 1.601 10.14 1.562 10.14 1.554 10.14 1.541 10.14 1.540 10.14 1.558
RP 1 254 567 891011	ABS VEL 1N OUT 166.5 218.8 189.8 211.5 195.9 201.7 194.6 207.1 193.3 200.4 191.7 199.6 191.6 197.6 190.7 198.9 180.8 207.6 179.8 218.6 172.1 243.3	REL VEL IN OUT 457.3 310.2 449.3 318.7 417.6 282.7 581.0 236.9 571.4 227.7 365.0 219.4 361.0 212.3 355.8 210.1 540.8 204.5 298.1 172.9 264.1 168.9	193.3 140.7 191.7 137.4 191.6 132.9 190.7 135.0 188.8 145.1 179.8 146.2	-0.1 142.7 -0.1 144.7 -0.1 146.2 -0.1 146.0 -0.1 148.4 -0.1 162.5	HHEEL SPEED IN OUT 417.4 415.6 407.2 405.5 568.7 369.0 327.5 331.1 317.1 321.8 510.5 315.8 300.3 306.9 263.7 292.5 237.8 254.9 226.0 245.9
RP 1 2 3 4 5 6 7 8 9 10 11	ABS MACH NJ IN OUT 0.564 0.600 0.575 0.586 0.596 0.564 0.592 0.583 0.588 0.564 0.583 0.562 0.582 0.556 0.580 0.561 0.573 0.588 0.544 0.623 0.520 0.695	REL MACH NO IN OUT 1.383 0.850 1.361 0.883 1.270 0.791 1.159 0.667 1.130 0.641 1.110 0.618 1.097 0.597 1.082 0.592 1.035 0.579 0.903 0.493 0.858 0.483	IN 0UT 0.564 0.438 0.575 0.456 0.596 0.428 0.592 0.414 0.588 0.396 0.583 0.387 0.582 0.374 0.580 0.381		MERID PEAK SS VEL R MACH NO 0.856 1.523 0.868 1.510 0.782 1.495 0.757 1.488 0.728 1.490 0.717 1.489 0.694 1.492 0.708 1.494 0.769 1.501 0.813 1.412 0.916 1.385
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT INCOME SPAN MEAN 5.00 3.0 10.00 3.2 30.00 4.2 50.00 5.5 55.00 6.0 57.50 6.2 60.00 6.3 62.50 70.00 7.0 90.00 8.4 95.00 9.6	SS 0.2 0.3 0.1 0.7 0.1 2.1 0.4 2.4 0.5 4.9 0.6 5.4 0.6 6.7 0.7 0.7 0.1 1.1 11.4 2.1 6.4	D-FACT EFF  0.445 0.728 0.399 0.807 0.428 0.864 0.493 0.866 0.498 0.838 0.512 0.833 0.512 0.833 0.526 0.818 0.523 0.851 0.515 0.880 0.543 0.889 0.547 0.899	LOSS COEFF TOT PROF 0.241 0.159 3.159 0.063 0.110 0.049 0.116 0.072 0.143 0.102 0.149 0.110 0.164 0.127 0.154 0.118 0.115 0.083 0.126 0.117 0.134 0.129	LOSS PARAM TOT PROF 0.047 0.031 0.030 0.016 0.020 0.009 0.022 0.013 0.025 0.018 0.026 0.020 0.029 0.022 0.027 0.021 0.021 0.015 0.023 0.022 0.026 0.025

## TABLE VIII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 17

## (a) 50 Percent of design speed; reading 2837

RP 1 2 5 4 5 6 7 8 9 11 11	RADII IN OU 24.587 24.6 24.056 24.1 21.961 22.1 19.883 20.1 19.365 19.6 19.106 19.4 18.847 19.1 18.588 18.9 17.813 18.2 15.751 16.2 15.237 15.8	T IN 00 46.8 10 41.5 34 40.7 60 45.4 70 47.8 26 49.5 82 50.9 38 51.4 14 48.6 97 44.0	7.8 4.7 0.8 1.9 1.6 1.0 0.9	1N 46.8 41.5 40.7 45.4 47.8 49.5 50.9 51.4 48.6 44.0	0.8 1.9 1.6 1.3 1.0 0.9 1.2 2.8	1N 304.9 303.5 300.8 300.4 300.4 300.1 300.2 300.1 299.8	1.000 1.000 1.000 1.000 0.999 0.999	11.51 11.53 11.45 11.43 11.41	0.996 0.993 0.994 0.994 0.995 0.994 0.999
RP 1 23 4 5 6 6 8 9	ABS VEL 1N OU 102.5 84 104.6 84 100.9 61 103.5 75 103.2 76 104.9 75 14.9 75 14.9 82	T IN 102.3 104.6 100.9 103.5 103.5 101.7 101.5 113.6 113.6	VEL 0UT 84.5 84.7 81.0 77.3 76.0 74.0 73.6 75.1 88.3 82.5	MERIO 1N 70.0 78.3 76.4 72.7 69.4 66.2 64.2 63.3 69.4 81.7 84.8	00T 83.7 84.4 81.0 77.3 76.0 74.0 73.6 75.1 88.2	78.7	0UT 11.4 7.0 1.1 2.6 2.2 1.7 1.3	:N 0. 0. 0. 0. 0.	SPEED OUT 2. 2. 2. 2. 2. 2. 2. 2.
40	ABS MACH IN 00 0.295 0.2	1 (N 43 0.295	0.243 0.244	MERID MI IN 0.202	0.241			EL 9	PEAR SS MACH NO 0.491 0.455
254561-8951	0.302 0.2 0.293 0.2 0.301 0.2 0.300 0.2 0.296 0.2 0.295 0.2 0.305 0.2 0.352 0.2	34 0.293 24 0.301 20 0.300 17 0.296 14 0.295 13 0.295 18 0.305 56 0.332	0.234 0.224 0.220 0.217 0.214 0.213 0.218 0.256 0.239	0.226 0.222 0.211 0.201 0.192 0.166 0.184 0.202 0.238	0.245 0.234 0.224 0.220 0.217 0.214 0.213 0.217 0.256 0.239			1.064 1.064 1.096 1.132 1.153 1.162 1.083 1.079	0.435 0.499 0.508

#### (b) 60 Percent of design speed; reading 2835

RP 1 2 3 4 5 6 7 8 9 111	RAD IN 24.587 24.056 21.961 19.883 19.365 19.106 18.847 18.588 17.813 15.751 15.237	0UT 24.600 24.110 22.134 20.160 19.670 19.426 19.182 18.938 18.214	IN 47.2 41.7 40.7 45.6 48.3 49.7 51.1 51.5 48.3	1.5 1.1 0.9 0.6 1.0	1N 47.2 41.7 40.7 45.6 48.3 49.7 51.1 51.5 48.3 44.3	1.1 0.9 0.6 1.0 2.8	1N 312.0 310.1 306.2 305.7 305.6 305.5 305.5 305.4 305.0 303.5	1.000 0.999 0.999 0.999	1014L 1N 12.15 12.20 12.05 12.01 11.99 11.96 11.93 11.98 12.06 12.15	3.989 5.994 3.995 5.989 5.995 3.995 5.995
RP 1 23 4 5 6 1 8 9	185 18 125.1 125.7 121.0 125.4 125.4 122.7 122.6 127.6 139.4	VEL 0UT 101.0 101.4 96.5 91.2 89.2 88.0 87.2 86.5 96.2 96.2	REL (N 125.1 125.7 121.0 123.4 123.4 122.4 122.7 122.6 139.4 147.4	00T 101.0 101.4 96.5 91.2 89.2 88.0 87.2 86.5 88.2	91.8 86.3 82.1 79.2 77.0 76.3 84.9 99.8	00T 100.1 101.1 96.5 91.2 89.2 88.0 87.2	TAN (N 90.5 85.7 78.8 88.2 92.1 93.4 95.5 96.0 97.4	13.6 6.2 1.4 2.9 2.4 1.7 1.3	:N 0. 0. 0. 0. 0. 0. 0.	SPEED OUT
R+ 254561 89911	ABS M IN 0.352 0.361 0.357 0.357 0.354 0.355 0.369 0.406 0.429	ACH NO 0.298 0.290 0.277 0.262 0.256 0.251 0.249 0.254 0.299 0.277	REL M IN 0.352 0.361 0.357 0.357 0.354 0.355 0.369 0.406 0.429	0.288 0.290 0.277 0.262 0.253 0.253 0.251 0.249 0.254 0.299	MERID M 1N 0.239 0.269 0.265 0.249 0.237 0.229 0.221 0.246 0.790 0.301	ACH NO 007 0.285 0.289 0.277 0.262 0.256 0.253 0.250 0.249 0.254 0.299 0.277				2.625 2.625

# (c) 70 Percent of design speed; reading 2829

P - 254561 8951	24.587 24.608 24.056 24.118 21.961 22.134 19.883 20.163 19.365 19.678 19.106 19.426 18.847 19.182 18.588 18.938 17.613 18.214 15.751 16.297	44.4 5. 43.0 1. 47.9 1. 50.0 1. 51.3 1. 52.4 1. 53.0 1. 49.1 1. 44.9 3.	1N 001 6 48.8 7.6 0 44.4 5.0 5 43.0 1.5 9 47.9 1.9 6 50.0 1.6 3 51.3 1.3 1 52.4 1.1 2 53.0 1.2 8 49.1 1.8	322.1 0.997 319.5 0.999 313.9 0.999 313.1 0.998 312.8 0.998 312.7 0.998 312.5 0.998 312.4 0.997 311.4 0.999 308.9 1.2.5	13.02 0.987 13.07 0.983 12.91 0.987 12.86 0.980 12.80 0.981 12.76 0.983 12.72 0.985 12.71 0.985 12.75 0.983
g. 254561 85	14.6 117.1 144.1 111.4 147.5 123.8 146.2 101.2	147.6 117.1 144.1 111.4 147.3 103.8 146.2 101.2 145.0 99.9 144.0 99.3 144.7 98.7 149.7 101.5	98.7 103.7 94.0 101.1 90.6 99.9 87.9 99.3	1N 00T 109.0 15.4 103.3 10.1 98.2 2.9 109.4 3.4 111.9 2.8 113.2 2.3 114.0 2.0 115.5 2.1	
g · 254561.8951	ABS MACH NO 1N 0.7 0.410 0.328 0.419 0.331 0.412 0.317 0.423 0.295 0.423 0.288 0.416 0.284 0.413 0.283 0.415 0.281 0.431 0.290 0.463 0.336 0.494 0.308	REL MACH NO IN OUT 0.410 0.328 0.419 0.331 0.412 0.317 0.423 0.295 0.420 0.284 0.416 0.284 0.415 0.281 0.431 0.290 0.463 0.336 0.494 0.308	MERID MACH NO 1N 0UT 0.270 0.325 0.350 0.350 0.350 0.268 0.260 0.264 0.252 0.265 0.262 0.262 0.269 0.328 0.341 0.307		MER: PELY 55 EL F MICH 15 218
RP 1 234561 8951	PERCENT (NC SPAN MEAN 5.00 12.9 10.00 10.3 30.00 10.6 50.00 14.7 55.00 16.3 57.50 17.4 60.00 18.3 62.50 18.7 70.00 90.00 6.5 95.00 6.6	SS 6.7 19.9 4.2 16.1 4.4 10.9 8.5 10.8 10.1 10.4 11.3 10.1 12.1 9.9 12.5 9.9 7.9 10.5 0.5 11.9 6.0 11.7	D-FACT EFF  0.445 0. 0.424 0. 0.519 0. 0.534 0. 0.539 0. 0.539 0. 0.545 0. 0.525 0. 0.427 0. 0.530 0.	LOSS COEFF TOT PROF 0.124 0.124 0.147 0.147 0.114 0.110 0.163 0.163 0.153 0.153 0.158 0.158 0.138 0.138 0.138 0.138 0.139 0.139 0.064 0.064 0.210 0.210	LOSS PARAM TOT PROF 0.047 0.047 0.055 0.055 0.039 0.039 0.053 0.050 0.046 0.046 0.041 0.041 0.040 0.040 0.039 0.039 0.016 0.016 0.051 0.051

TABLE VIII. - Continued.

(d) 70 Percent of design speed; reading 2830

B . 25.45.01.83.31	RAD1: 24.687 24.683 24.356 24.110 21.961 22.134 19.885 22.163 19.365 19.673 19.136 19.426 18.647 19.182 16.588 16.938 17.615 18.214 15.751 16.297 15.257 15.814	38 007 35.7 5.6 35.1 4.6 37.1 2.1 40.6 2.5 43.1 2.5 44.7 2.2 46.0 -0.0 45.9 -0.4 45.1 -0.6 42.5 1.9	55.1 4.6 57.1 3.1 43.6 3.5 43.1 3.5 44.7 3.1 46.3 -3.3 45.9 3.4 45.1 -3.8 42.5 1.9	7074 TEMP 18. 82.10 519.9 1.001 510.9 0.999 510.6 0.997 510.6 0.9	2.65 .66 2.60 .689 2.60 .689 2.60 .689 2.61 .69 2.65 .69 2.65 .684 2.75 .689
B - 25 4 5 61 8 9	485 VEL (N 007 127.0 119.3 129.1 126.2 121.5 117.5 125.4 115.4 126.3 114.3 125.7 112.6 124.6 111.2 125.8 113.8 151.5 113.8 151.5 113.8 151.5 113.8 151.5 113.8	REL VEL IN 00T 147.0 119.3 149.1 126.2 141.3 117.5 145.4 115.4 146.3 114.3 145.7 112.6 144.6 111.4 145.8 110.8 151.5 111.5 163.9 127.1 174.1 122.0	100.5 111.4	TANG VEL (N OUT 65.9 12.1 65.2 0.2 64.5 1.0 122.5 0.5 124.0 -0.1 124.8 -0.1 124.8 -1.5 110.7 4.2 121.3 7.9	1. 1.
P: 25.4 5 61: 8 9 51	ABS MACH NO IN OUT 0.420 0.339 0.427 0.360 0.406 0.327 0.420 0.327 0.420 0.323 0.416 0.319 0.420 0.317 0.438 0.320 0.476 0.365 0.506 0.350	REL MACH NO IN OUT 0.420 0.339 0.427 0.360 0.406 0.336 0.419 0.330 0.421 0.327 0.420 0.323 0.416 0.319 0.420 0.317 0.438 0.320 0.476 0.365 0.506 0.350	MERID MACH NO IN OUT 0.341 0.337 0.350 0.358 0.318 0.330 0.327 0.298 0.323 0.299 0.319 0.292 0.317 0.320 0.351 0.365 0.363 0.349		MERIO PEAK SS MEL R MACH NO 0.995 0.538 1.031 0.548 1.043 0.553 1.044 0.601 1.071 0.635 1.088 0.652 1.108 0.661 1.093 0.663 1.007 0.637 1.050 0.632 0.974 0.778
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT INC SPAN MEAN 5.00 -0.2 10.00 1.0 30.00 4.7 50.00 7.3 55.00 9.5 57.50 10.8 60.00 11.9 62.50 11.6 70.00 8.0 90.00 4.1	-6.3 18.1 -5.2 15.7 -1.5 9.5	D-FACT EFF  0.381 0. 0.345 0. 0.375 0. 0.406 0. 0.423 0. 0.436 0. 0.442 0. 0.450 0. 0.456 0. 0.383 0.	LOSS COEFF TOT PROF 0.114 0.114 0.083 0.083 0.046 0.046 0.081 0.081 0.094 0.094 0.093 0.093 0.081 0.081 0.082 0.082 0.132 0.132 0.073 0.073	LOSS PARAM TOT PROF 0.044 0.044 0.031 0.031 0.016 0.016 0.025 0.025 0.029 0.029 0.028 0.028 0.024 0.024 0.037 0.037 0.018 0.018

# (e) 70 Percent of design speed; reading 2831

RP 1 2 3 4 5 6 7 8 9 10 11	RAD IN 24.587 24.056 21.961 19.885 19.365 19.106 18.847 18.588 17.813 15.751 15.237	0UT 24.600 24.110 22.134 20.160 19.670 19.426 19.182 18.938 18.214 16.297	ABS IN 30.3 28.5 30.3 34.2 35.7 57.4 59.3 39.1 37.1 39.3 41.2	BETAM OUT 5.2 3.5 -1.0 -0.9 -0.3 -0.5 -0.6 -1.3 0.5 3.3	IN 30.5 28.5 30.3 34.2 35.7 37.4 39.3 39.1 37.1	BETAM OUT 5.2 3.5 -1.0 -0.9 -0.3 -0.3 -0.5 -1.3 0.5 3.3	1N 312.9 310.2 307.7 307.5 308.1 308.4 308.7 308.4	TEMP RATIO 0.999 1.002 0.999 0.999 0.997 0.996 0.997 0.998 1.000 2.999	1014L 1N 12.58 12.54 12.40 12.38 12.44 12.34 12.35 12.35 12.59 12.74	PRESS RATIO 0.983 0.995 0.996 0.992 0.994 0.998 0.996 0.991 0.992 0.969
RP 1 2 5 4 5 6 7 8 9	ABS (N 150.5 147.0 140.4 144.8 146.9 145.3 147.1 152.5 167.3	VEL 0117 122.4 130.7 126.1 127.2 126.8 126.6 126.5 128.3 142.8 137.8	1N .150.3 147.0 140.4 144.8 148.3 146.9 145.3 147.1 152.5	VEL 001 122.4 130.7 126.1 126.1 127.2 126.8 126.6 126.5 128.3 142.8 137.8	129.2 121.2 119.8 120.5 116.8 112.5 114.2 121.7 129.4	VEL 0017 121.9 130.5 126.1 126.0 127.2 126.8 126.5 128.2 142.8 137.6	TAN IN 75.8 70.1 70.9 81.3 86.5 89.1 92.0 92.7 92.0 106.1	8.0 -2.2 -1.9 -0.7 -0.6 -1.0 -1.4 -2.9	0. 0. 0.	SPEED OUT
RP 23456789111	ABS M 1N 0.432 0.424 0.426 0.419 0.425 0.425 0.425 0.427 0.516	ACH NO OUT 0.350 0.375 0.363 0.363 0.365 0.365 0.365 0.365 0.370 0.413 0.397	REL M IN 0.432 0.424 0.406 0.419 0.425 0.425 0.425 0.442 0.487 0.516	0.350 0.375 0.363 0.363 0.363 0.365 0.365 0.365 0.365 0.370 0.413 0.397	MERID M IN 0.375 0.375 0.350 0.347 0.349 0.338 0.325 0.350 0.353 0.376 0.388	ACH NO 0UT 0.348 0.374 0.363 0.363 0.365 0.365 0.365 0.370 0.413 0.397			MER 15 VEL R 0.939 1.010 1.052 1.056 1.086 1.126 1.108 1.054 1.104	PEAR SS MACH NO 0.443 0.424 0.504 0.504 0.551 0.571 0.571 0.548 0.590 0.742

## (f) 70 Percent of design speed; reading 2832

RP 1 23 4 5 6 7 8 9 11 11		24.110 22.134 20.160 19.670 19.426 19.182 16.938 18.214 16.297	23.6	BETAM 0UT 4.6 2.2 -1.8 -2.4 -1.9 -1.7 -1.5 -1.4 -2.2 -0.3 2.5	IN 23.6 22.2 23.2 27.3 28.4 29.8 31.9 31.3 30.3	BETAM 0UT 4.6 2.2 -1.8 -2.4 -1.9 -1.7 -1.5 -1.4 -2.2 -0.3 2.5	308.1 306.0 304.1 304.6 304.9 305.4 306.0 305.7 305.3 306.5	RATIO 1.000 1.000 1.000 0.998 0.998 0.998 0.998 0.998 1.000 0.999		0.994 0.994 0.995 0.995 0.995 0.998
R - 254561 80	ABS 1N 153.5 147.8 144.9 148.5 152.1 152.1 152.4 159.5 143.9	VEL 0UT 126.9 139.2 139.1 140.9 145.5 144.8 145.5 145.9 149.8 166.5 158.1	REL :N 153.5 147.8 144.9 148.5 151.7 152.1 151.3 152.4 159.5 174.3 183.9	VEL 0UT 126.9 139.2 139.1 140.9 143.5 144.6 145.3 145.9 149.8 166.5 158.0	MERI 1N 140.6 136.9 133.2 132.0 135.5 131.9 128.2 137.8 143.6 147.5	126.5 139.1 139.0 140.8 143.4 144.8 145.3 145.9 149.7 166.5	51.55.55.55.55.55.55.55.68.2221.75.80.85.98.8	0UT 10.3 5.4 -4.3 -6.0 -4.7 -4.2 -3.7 -5.6 -0.8	:N 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	:
RP - 25 4 5 6 1 8 9 0 1 1	ABS M IN 0.445 0.429 0.422 0.443 0.443 0.443 0.465 0.509 0.537	ACH NO OUT 0.365 0.403 0.404 0.410 0.417 0.421 0.423 0.424 0.436 0.486 0.459	0.422 0.432 0.442 0.443 0.439	0UT 0.365 0.403 0.404 0.410 0.417 0.421 0.423 0.424 0.436 0.459	0.407 0.397 0.388 0.384 0.389	ACH NO OUT 0.364 0.403 0.404 0.409 0.417 0.421 0.422 0.424 0.436 0.486 0.458				PEAR SS MACH NO 0.445 0.429 0.422 0.432 0.443 0.443 0.465 0.509 0.686
RP 1 2 3 4 5 6 7 8 9	PERCENT SPAN 5.00 10.00 30.00 50.00 57.50 60.00 62.50	1NC1 MEAN -12.3 -11.9 -9.2 -5.9 -5.3 -4.0 -2.2 -3.0	SS -18.4 -18.1 -15.4 -12.1 -11.4 -10.2 -8.4 -9.2	DEV 16.9 13.3 7.6 6.4 6.9 7.1 7.3	D-FACT 0.302 0.187 0.186 0.207 0.208 0.205 0.200	0. 0. 0. 0.	LOSS CO TOT 0.221 0.053 0.020 0.042 0.047 0.038 0.013	DEFF PROF 0.221 0.053 0.020 0.042 0.047 0.038 0.013	LCSS P TOT 0.085 0.020 0.007 0.013 0.014 0.011	ARAM PROF 0.085 0.020 0.007 0.013 0.014 0.011 0.024

TABLE VIII, - Continued,

# (g) 70 Percent of design speed, reading 2917

RP: 25456789011	24,567 24, 24,365 24, 21,961 22, 19,883 20, 19,365 19, 19,106 19, 18,847 19, 18,588 18, 17,613 18,	UT (N 600 15.1 110 15.2 134 16.2 160 20.5 670 21.5 426 22.9 182 25.0 936 24.8 214 24.0 297 29.1	5.0 2.7 -1.6 -3.0	15.1 15.2 16.2 20.5 21.5 22.9 25.0 24.8 24.0	5.6 2.7	1% 502.4 501.1 503.0 501.1 501.5 502.4 502.4 504.5	1.005 1.005 1.005 0.903 0.903 0.996 0.998	11.42 11.45 11.47 11.58 11.61 11.63	RATIO 0.945 0.979 0.986 0.985 0.989 0.591 0.994 0.988
RP 1 25 4 5 6 7 6 9 5 5 1	155.1 13 151.6 15 151.0 15 157.6 16 159.5 16 160.1 16 160.2 17 160.2 17 168.3 17	UT 1N 0.3 155.1 2.3 151.6 6.7 151.0 4.0 157.6 7.5 159.5 9.9 160.1 2.8 160.2 4.9 160.2 9.7 160.0 2.8 186.8	00T 130.3 152.3 156.7 164.0 167.5 169.9 172.8 174.9 179.7 202.8	145.2 145.5 153.5 163.2	007 129.6 152.2 156.6 163.7 167.1 169.6 172.7 174.8 179.5 202.8	1N 40.4 39.6 42.0 55.3 58.4 62.4 67.7	13.: 7.1 -4.4 -8.5 -12.1 -10.6 -6.0 -8.1 -8.3	:N c. c. c. c. c. c.	0. 0. 0.
RP 1 2 3 4 5 6 7 8 9 10 11	0.454 0.444 0.463 0.463 0.468 0.470 0.469 0.470 0.555 0.555 0.555	UT IN 378 0.454 446 0.444 461 0.445 483 0.465 493 0.468 501 0.470 509 0.469 516 0.470 530 0.494	0.578 0.446 0.461 0.483 0.493 0.501 0.509 0.516 0.530	IN 0.458 0.429 0.435 0.435 0.436 0.455 0.425 0.426	007 0.576 0.445 0.461 0.402 0.402 0.500 0.509 0.515			VEL R 0.866 1.040	0.445 0.445 0.468 0.468 0.470 0.469
RP 1 2 3 4 5 6 7	5.00 - 10.00 - 30.00 - 50.00 - 55.00 -	INCIDENCE MEAN SS 20.8 -26.9 18.9 -25.0 16.2 -22.4 12.7 -18.9 12.2 -18.3 11.0 -17.1	DEV 18.1 13.8 7.8 5.9 4.7 5.2	D-F4CT 0.076 0.076 0.000 0.000 0.004 0.004	0. 0. 0. 0.	LOSS C 107 0.413 0.166 0.116 0.118 0.118 0.118	OEFF PROF 0.416 0.166 0.106 0.106 0.081	LOSS P TOT 0.160 0.003 0.003 0.003 0.025 0.025	ARAM PROF 0.160 0.665 0.037 0.034 0.025

TABLE VIII. - Continued.

(h) 80 Percent of design speed; reading 2814

\$P 1 25 4 5 6 7 8 0	24.587 24.587 24.056 21.961 19.865 19.365 19.166 18.847 18.568	007 24.600 24.110 22.134 20.160 19.670 19.426 19.162 18.938	46.1 43.4 46.1 49.3 51.7 53.0 54.2	BET4M 0(17 8.0 5.8 1.9 1.8 1.1 0.6	1% 45.4 46.3 49.3 51.7 53.0 54.2 54.1	BET4M 0UT 8.0 5.6 1.6 1.6 1.7	551.4 528.7 522.5 521.0 522.5 520.5 520.5 519.9	1.999 1.998 1.998 1.996 1.997	14.25 14.26 15.66 15.66 15.66 15.62	985 985 984 984 984 984 984
18	17.815		51.8 45.4	1.6	50.8		318.1 315.5	1.005	15.64	1.986 1.992
11	15.257		46.6				517.5	1.002	14.:"	:.954
ap.		VEL	REL		MERI		120	5 iE,	WEE.	SPEED
	170.5	142 4	173.5	140.4	118.3	159.0		19.5	: %	OUT.
3	1.2.2	150.0	172.2	159.9	1,35.3	159.2	118.2	14.1	õ.	
3	64.9	26.9	164.9	126.9	114.6	126.8	118.6	4.2	3.	2.
5	68.8	118.	168.8	116.5	110.2	118.6	127.9	3.6	2.	
6	64.4	115.3	164.4	115.0	99.3	115.3	150	2.5		
		114.2	165.2	114.2	65.5	116.2	152.5	4	2.	
a	65.9	114.3	165.9	114.5	96.3	114.0	152.8	1.5	* *	9
9	69.		169.0	116.9	106.9	116.8	150.9	5.2	S .	
	6	152.9	180.6	152.9	136.0	132.6	128.6	8.3	0 x	
\$0. 254561 89511	485 M 3.478 3.468 3.468 3.468 3.465 3.465 3.465 3.467 0.465	0.7 0.7 0.391 0.391 0.357 0.324 0.324 0.322 0.322 0.322 0.327 0.349	REL N 1N 0.478 0.485 0.468 0.465 0.465 0.467 0.467 0.571	MACH NO 0UT 0.591 0.591 0.357 0.354 0.328 0.524 0.522 0.522 0.530 0.577	MERID M (N 0.351 0.352 0.325 0.325 0.293 0.292 0.272 0.306 0.366 0.366	ACH NO OUT 0.587 0.587 0.354 0.328 0.322 0.322 0.322 0.322			6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 6 9 9 9 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	85. 85. 85. 86. 86. 82. 92.
254561 89011	0.478 0.485 0.468 0.468 0.465 0.467 0.467 0.571	007 0.391 0.391 0.357 0.354 0.328 0.322 0.322 0.322 0.349	0.478 0.485 0.468 0.461 0.473 0.466 0.465 0.467 0.521 0.571	0.07 0.591 0.591 0.557 0.554 0.526 0.524 0.522 0.522 0.530 0.577	0.351 0.352 0.325 0.314 0.295 0.282 0.272 0.274 0.366	0.7 0.587 0.589 0.557 0.554 0.528 0.522 0.522 0.522 0.522	LOSS C			
25456 89011 RP	0.478 0.485 0.468 0.465 0.465 0.467 0.463 0.521 0.571 PERCENT	007 0.391 0.391 0.357 0.354 0.328 0.322 0.322 0.322 0.330 0.377 0.349	0.478 0.485 0.468 0.461 0.473 0.468 0.465 0.467 0.521 0.571	0.07 0.591 0.591 0.557 0.534 0.529 0.524 0.522 0.522 0.530 0.577 0.349	0.351 0.352 0.325 0.325 0.314 0.293 0.282 0.272 0.274 0.306 0.366 0.395	0.7 0.387 0.389 0.357 0.354 0.322 0.322 0.322 0.322 0.322	101	PROF		
23.45.61 89111 RP1	3.478 3.468 3.468 3.468 3.468 3.465 3.467 3.467 3.521 3.521 3.571 PERCENT SPAN 5.00	007 0.391 0.391 0.357 0.354 0.328 0.322 0.322 0.322 0.330 0.377 0.349	0.478 0.485 0.468 0.468 0.467 0.467 0.467 0.571 0.571	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.522 0.530 0.577 0.549	0.351 0.352 0.325 0.314 0.295 0.282 0.272 0.274 0.306 0.366 0.395	0.7 0.587 0.589 0.557 0.534 0.528 0.522 0.522 0.522 0.522	101	PROF 0.118		
23.45.61 89111 RP1	2.478 2.485 3.468 3.468 3.465 3.465 3.467 3.521 3.521 3.571 PERCENT SPAN 5.00 10.00 30.00	007 0.391 0.391 0.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.3 13.6	0.478 0.485 0.468 0.468 0.465 0.465 0.467 0.467 0.521 0.571 DENCE SS 4.1	0.07 0.391 0.391 0.357 0.354 0.329 0.524 0.322 0.322 0.350 0.377 0.349	0.331 0.352 0.325 0.314 0.293 0.282 0.272 0.274 0.306 0.366 0.393	0.7 0.587 0.589 0.557 0.534 0.528 0.522 0.522 0.522 0.549	0.118 0.118 0.135 0.115	0.118 0.155 0.115		
23.45.61 89111 RP1	2.478 3.478 3.468 3.468 3.468 3.465 3.467 0.465 3.521 0.571 PERCENT SPAN 5.00 10.00 30.00 50.00	007 0.391 0.391 0.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.3 13.6 16.0	0.478 0.485 0.468 0.469 0.465 0.467 0.467 0.521 0.571 DENCE SS 4.1 7.4 9.8	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.522 0.530 0.577 0.549	0.331 0.352 0.325 0.314 0.293 0.282 0.272 0.274 0.306 0.366 0.393	0.7 0.587 0.589 0.554 0.528 0.522 0.522 0.522 0.549	101 0.118 0.135 0.115	PROF 0.118 0.135 0.115 0.161	5 2 5 6 93 93 93 93 93 93 93 93 93 93	
23.45.61 89111 RP1	2.478 3.478 3.468 3.468 3.465 3.465 3.467 0.465 3.521 0.571 PERCENT SPAN 5.00 10.00 50.00 55.00	007 0.391 0.391 0.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.3 13.6 16.0 18.0	0.478 0.485 0.468 0.468 0.465 0.465 0.467 0.467 0.521 0.571 DENCE SS 4.1 7.4 9.8 11.8	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.530 0.577 0.549 0EV 20.5 16.9 11.5 10.7	0.331 0.352 0.325 0.314 0.295 0.282 0.272 0.274 0.306 0.366 0.393 0-Fact 0.410 0.415 0.469 0.525 0.532	0.7 0.587 0.589 0.554 0.528 0.522 0.522 0.522 0.549	101 0.118 0.135 0.115 0.161 0.157	PROF 0.118 0.155 0.115 0.161 0.137		
23.45.61 89111 RP1	2.478 3.478 3.468 3.468 3.465 3.465 3.467 0.465 3.521 0.571 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50	007 3.391 3.391 3.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.3 13.6 16.0 18.0 19.1	0.478 0.485 0.468 0.468 0.465 0.467 0.465 0.521 0.571 0.571 0.571	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.530 0.577 0.549 0EV 20.5 16.9 11.5 10.7 9.9 9.6	0.331 0.352 0.325 0.314 0.295 0.282 0.272 0.306 0.366 0.393 0-FACT 0.410 0.415 0.469 0.525 0.536	0.7 0.587 0.589 0.554 0.528 0.522 0.522 0.522 0.549 0.549	TOT 0.118 0.135 0.115 0.161 0.157 0.117	PROF 0.118 0.135 0.115 0.161 0.157 0.117		
23.45.61 89111 RP1	2.478 3.478 3.468 3.468 3.465 3.465 3.467 0.465 3.521 0.571 PERCENT SPAN 5.00 10.00 50.00 55.00	007 3.391 3.391 3.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.5 13.6 16.0 18.0 19.1 20.1 19.8	0.478 0.485 0.468 0.468 0.465 0.467 0.467 0.571 0.571 0.571 0.571	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.530 0.577 0.549 0EV 20.5 16.9 11.5 10.7 9.6 9.5	0.331 0.352 0.325 0.314 0.295 0.282 0.272 0.306 0.366 0.393 0-FACT 0.410 0.415 0.469 0.525 0.536 0.536	0.7 0.587 0.589 0.554 0.528 0.522 0.522 0.522 0.549	101 0.118 0.135 0.115 0.161 0.157	PROF 0.118 0.135 0.161 0.161 0.137 0.117		
- 254561 8951 P1254561 89	2.478 3.478 3.468 3.468 3.468 3.465 3.467 3.521 3.521 3.571 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50 70.00	0.7 0.391 0.391 0.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INC! MEAN 10.2 9.3 13.6 16.0 18.0 19.1 19.8 15.7	0.478 0.468 0.468 0.468 0.465 0.467 0.467 0.571 0.571 0.571 0.571	007 0.591 0.591 0.557 0.554 0.529 0.524 0.522 0.530 0.577 0.549 0EV 20.5 16.9 11.5 10.7 9.6 9.5 9.4 10.2	0.331 0.352 0.325 0.314 0.293 0.282 0.272 0.274 0.306 0.366 0.393 0-FACT 0.410 0.415 0.469 0.525 0.536 0.537 0.516	0.7 0.587 0.589 0.557 0.534 0.522 0.522 0.522 0.522 0.549 0.549	0.118 0.135 0.115 0.161 0.157 0.117 0.096 0.092	PROF 0.118 0.135 0.151 0.151 0.151 0.151 0.092 0.092		
23.45.61 891011 RP1	2.478 3.478 3.468 3.468 3.465 3.465 3.467 0.465 3.521 0.571 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50	007 3.391 3.391 3.357 0.354 0.322 0.322 0.322 0.330 0.377 0.349 INCI MEAN 10.2 9.5 13.6 16.0 18.0 19.1 20.1 19.8	0.478 0.485 0.468 0.468 0.465 0.467 0.467 0.571 0.571 0.571 0.571	007 0.591 0.591 0.557 0.554 0.524 0.522 0.522 0.550 0.577 0.549 0EV 20.5 16.9 11.5 10.7 9.6 9.6 9.5 9.4	0.331 0.352 0.325 0.314 0.295 0.282 0.272 0.274 0.306 0.366 0.395 0-FACT 0.410 0.415 0.469 0.525 0.536 0.536 0.537	0.7 0.587 0.589 0.554 0.522 0.522 0.522 0.522 0.549 0.549	0.118 0.135 0.135 0.115 0.161 0.157 0.117 0.096	PROF 0.118 0.135 0.151 0.161 0.157 0.117 0.096 0.092		

# (i) 90 Percent of design speed; reading 2820

RP 1 2 3 4 5 6 7 8 9 10 11	RADII 1N 007 24.587 24.600 24.056 24.110 21.961 22.134 19.883 20.160 19.365 19.670 19.106 19.426 18.847 19.182 16.586 18.938 17.813 18.214 15.751 16.297 15.257 15.814	3N 007 56.3 6.3 32.0 3.5 33.0 -0.1 58.7 1.8 38.8 -1.3 59.4 -2.6 40.4 -2.3 40.0 -1.5 57.4 -0.4 40.0 1.5	36.5 6.3 32.0 3.5 33.0 -0.1 38.7 1.8 38.8 -1.3 39.4 -2.6 40.4 -2.3 40.0 -1.5 57.4 -0.4 40.0 1.5	TOTAL TEMP (N RATIO 347.0 0.995 339.4 1.003 333.1 0.998 332.1 0.996 329.6 0.999 328.8 0.998 328.5 0.998 328.0 0.999 327.4 0.999 326.8 1.008 351.5 1.001	TOTAL PRESS 1N RATIO 16.17 0.965 16.00 0.988 15.75 0.992 15.52 0.986 14.93 1.000 14.76 1.002 14.70 1.006 14.76 1.006 15.19 0.994 15.15 1.000 15.68 0.936
	485 VEL (N 001 222.4 181.8 215.1 189.9 210.7 184.6 215.4 178.5 210.8 165.9 166.5 161.6 194.2 161.7 197.6 164.6 214.1 75.2 225.2 184.7 246.2	REL VEL  IN CUT  222.4 181.8 215.1 189.9 210.7 184.6 215.4 178.5 220.8 185.9 196.5 161.6 194.2 161.7 197.6 184.6 214.1 175.2 225.2 184.7 246.2 171.7	MERID VEL 1N 00T 179.2 160.T 162.4 169.5 176.T 164.6 168.1 178.5 156.5 165.9 151.6 161.4 147.8 161.5 151.5 164.6 178.0 175.2 172.4 164.6 179.9 171.4	TANG VEL (N 0017 131.6 20.1 114.0 11.4 114.8 -0.4 134.8 5.5 125.8 -5.9 124.9 -7.3 126.0 -6.4 127.1 -4.3 130.2 -1.2 144.8 4.1	1. 1. 1. 1. 2. 1.
ない のは 日のの 日の あいまり		REL MACH NO (N OUT 0.618 0.500 0.603 0.508 0.596 0.519 0.611 0.502 0.569 0.466 0.551 0.454 0.551 0.455 0.612 0.463 0.612 0.463 0.647 0.521 0.708 0.481	MERID MACH NO IN OUT 0.498 0.497 0.512 0.527 0.512 0.519 0.477 0.532 0.444 0.466 0.450 0.454 0.450 0.454 0.450 0.465 0.495 0.521 0.517 0.480		MERIC PEAK SS EL 9 MACH NO 1.018 .814 1.059 .721 1.062 .858 1.064 .765 1.064 .765 1.064 .765 1.064 .765 1.064 .765 1.064 .765

# (j) 90 Percent of design speed, reading 2821

	RAS	110	489	BETAM	REL	BETAM	1014	L TEMP	1014	PRESS
RP.	: `	0U7	!N	OUT	IN	DUT	;N	RAT:0	18	RATIO
*	24.587	24.600	28.7	5.1	28.7	5.1	555.1	1.002	14.59	
2	24.056	24,110	26.	2.6	26.	2.6	529.	1.005	14.49	0.980
3	21.961	22.134	27.2	-1.6	27.2	-1.6		1.000	14.55	1.99
4	19.885	20.160	55.9	0.6	55.9	0.6	326.8	0.995	14.40	0.982
5	19.365		35.6	-2.1	55.6	-2.1	325.5	0.999	15.65	1.005
5 6 7 8	19.106		55.2	-3.5	55.2	-3.5	321.8	1.001	15.51	1.006
•	18.847	19.182	35.8	-3.4	33.8	-3.4		0.999		1.008
8	18.588		34.1	-2.4	34.1	-2.4	522.1	1.000	13.58	1.313
9	17.815	18.214	51.5	-1.5		-1.5	322.0	1.001	14.28	1.995
10	15.751	16.29	34.8	2.4	34.8	2.4		1.007	14.78	
11	15.257	15.614	57.4	6.1	57.4	6.1	327.9	1.002	15.00	0.904
	489	VEL	REL		MERI		TAN		₩€D	SPEED
<b>qp</b>	: N	DUT	IN	OUT	IN	OUT	IN	OUT	IN	OU
1	210.9	181.0	210.9	181.0		180.3	101.2	16.0	٥.	٤.
2	211.3	195.9	211.0	195.9	188.5	195.7	94.8	8.8	٥.	
5	238.4	199.2	200.4	199.2		199.1	95.1	-5.6	٥.	٥.
4	217.9	1/8.5	217.9	198.5	181.0		121.4	2.0		٥.
5	195.	184.8	195.7	184.8	162.9		108.4	-6.9		2.
1254561.69	. 65.6	63.9	190.6	180.9		180.6	104.5	-11.1		٥.
-	189.5	182.1	189.5	182.1	157.4		105.2	-10.8	0.	
8	92.6	186.5		186.5	159.4	186.4	108.1	-7.7	٥.	
. 9	2	205.5		205.5	185.2	205.4	115.6	-4.5	٥.	
::	246	222.5	240.6		197.5	222.1	137.4	9.4	٥.	:.
* *	252.9	211.2	252.9	200.2	200.9	199.0	153.6	21.2	٥.	:.
	ABS M	ACH NO		ACH NO	MERID M	ACH NO				PELF SS
ep.	: N	OUT	IN	OUT	IN	OUT			.E. 9	MACH NO
-	3.597	0.507	IN 0.597	0.507	IN 0.524	0.505			1.974	MACH NO 1.597
-	2.597 2.600	0.507 0.557	0.597 0.600	0.507 0.554	IN 0.524 0.536	0.505 0.553			.E. R 0.974	MACH NO :.597 :.6::
-	2.597 2.600 0.597	0.507 0.554 0.569	0.597 0.600 0.597	0.507 0.554 0.569	0.524 0.536 0.531	0.505 0.555 0.553 0.568			.C. 4 3.974 3.038	MACH NO 1.597 1.611
-	2.597 2.600 0.597 0.624	0.77 0.507 0.554 0.569 0.567	0.597 0.600 0.597 0.624	0.507 0.554 0.569 0.567	0.524 0.536 0.531 0.518	0.505 0.553 0.568 0.567			.038	MACH NO 1.597 1.611 1.597
-	0.597 0.600 0.597 0.624 0.560	0.17 0.507 0.554 0.569 0.567 0.527	IN 0.597 0.600 0.597 0.624 0.560	0.7 0.507 0.554 0.569 0.567 0.527	(N 0.524 0.536 0.531 0.518 0.466	0.505 0.555 0.553 0.568 0.567			.038 1.074 1.074 1.074	MACH NO 597 611 597 3.745 651
-	0.597 0.600 0.597 0.624 0.560 0.546	0.17 0.507 0.554 0.569 0.567 0.527	IN 0.597 0.600 0.597 0.624 0.560 9.546	0.07 0.507 0.554 0.569 0.567 0.527 0.516	IN 0.524 0.536 0.531 0.518 0.466 0.457	0.505 0.555 0.568 0.567 0.527 0.515			.058 1.074 1.097 1.097 1.134	MACH NO 597 651 597 3.745 651
-	0.597 0.600 0.597 0.624 0.560 0.546 0.546	0.507 0.507 0.554 0.569 0.567 0.527 0.526	IN 0.597 0.600 0.597 0.624 0.560 0.546	0.507 0.507 0.554 0.569 0.567 0.527 0.516	0.524 0.536 0.531 0.518 0.466 0.457	0.505 0.505 0.553 0.568 0.567 0.527 0.515			.058 1.074 1.074 1.097 1.34 1.32	MACH NO 1.597 1.601 1.597 1.745 1.651 1.621
- 25456-8	0.597 0.600 0.597 0.624 0.560 0.546 0.542	0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533	IN 0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551	0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533	(N 0.524 0.536 0.531 0.518 0.466 0.457 0.450	0.505 0.505 0.553 0.568 0.567 0.527 0.515 0.519			0.974 1.038 1.074 1.097 1.134 1.132 1.155	M4CH NC 0.597 0.597 0.745 0.650 0.651 0.635
254561.89	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627	0.07 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590	IN 0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627	0.507 0.554 0.569 0.567 0.527 0.527 0.520 0.533 0.590	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456	0.505 0.553 0.568 0.567 0.527 0.515 0.519 0.533 0.590			10.974 1.038 1.074 1.097 1.34 1.32 1.55 1.69	M4(- N) 597 651 597 45 651 621 635
5 6 9 9 10	3.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698	0.07 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.542 0.551 0.627 0.698	0.01 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638	(N 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535	0.505 0.553 0.567 0.567 0.515 0.519 0.533 0.590 0.637			10.974 1.038 1.074 1.097 1.34 1.32 1.55 1.69	M4(
254561.89	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627	0.07 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590	IN 0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627	0.507 0.554 0.569 0.567 0.527 0.527 0.520 0.533 0.590	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456	0.505 0.553 0.568 0.567 0.527 0.515 0.519 0.533 0.590			10.974 1.038 1.074 1.097 1.34 1.32 1.55 1.69	M4(- N) 597 651 597 45 651 621 635
5 6 9 9 10	3.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698	0.07 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.542 0.551 0.627 0.698	0.01 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638	(N 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535	0.07 0.505 0.553 0.566 0.567 0.527 0.515 0.519 0.533 0.590 0.637	LOSS C	CEFF	10.974 1.038 1.074 1.097 1.34 1.32 1.55 1.69	M4(
5 6 9 9 10	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735	0.07 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568	(N 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733	0.07 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.568	(N 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.535	0.07 0.505 0.553 0.566 0.567 0.527 0.515 0.519 0.533 0.590 0.637	LOSS C	OEFF PROF	10.974 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991	MACH NO 1.597 1.611 1.597 1.651 1.651 1.621 1.627 1.627 1.628 1.956
25 4 5 6 7 8 9 10 11	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735	007 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733	0.07 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.568	(N 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.535	0.07 0.505 0.553 0.566 0.567 0.527 0.515 0.519 0.533 0.590 0.637			10.974 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991	MACH NO 1.597 1.611 1.597 1.651 1.651 1.621 1.627 1.627 1.628 1.956
2334 556 9 10 11	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT	0.07 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733	0.07 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.573 0.583	0.07 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	TOT	PROF	1.097 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991 LOSS F	MACH NO 1.597 1.611 1.597 1.651 1.651 1.621 1.627 1.628 1.628 1.628
2334 556 9 10 11	0.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733	0.01 0.507 0.554 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.573 0.583	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	0.200	PROF 0.200	1.097 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991 LOSS P	MACH NO 1.597 1.611 1.621 1.621 1.627 1.627 1.628 1.627 1.628 1.627 1.628 1.627 1.628
23.45.67.89.111 RP 1.23.4	2.597 2.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2 0.6	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6	0.01 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.456 0.535 0.573 0.583 D-FACT 0.297 0.225 0.210 0.259	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	TOT 0.200 0.091 0.016 0.078	PROF 0.200 0.091 0.016 0.078	1.097 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991 LOSS P	MACH NO. 597 0.651 0.651 0.651 0.621 0.635 0.627 0.698 0.956
23.45.67.89.111 RP 1.23.4	2.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00 10.00 50.00 55.00	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2 0.6	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6 -6.2	0.01 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.573 0.583 0-FACT 0.297 0.225 0.210 0.259 0.234	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	101 0.200 0.091 0.016 0.078 -0.025	PROF 0.200 0.091 0.016 0.078 -0.025	1.097 1.038 1.074 1.097 1.134 1.132 1.155 1.169 1.109 1.125 0.991 LOSS F	MACH NO. 597 0.651 0.651 0.651 0.621 0.635 0.627 0.698 0.956 MARAM PROF 0.034 0.005 0.024 -0.018
23.45.67.89.111 RP 1.23.4	2.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2 0.6 -0.0	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6 -6.2 -6.8	0.01 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.456 0.535 0.573 0.583 0-FACT 0.297 0.225 0.210 0.259 0.234 0.232	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	TOT 0.200 0.091 0.016 0.078 -0.025 -0.032	PROF 0.200 0.091 0.016 0.078 -0.025 -0.032	1.097 1.038 1.074 1.097 1.34 1.32 1.095 1.109 1.125 0.991 LOSS F TOT 0.077 0.034 0.005 0.024 -0.008	MACH NO. 597 0.651 0.651 0.651 0.655 0.627 0.698 0.956 MRAM PROF 0.034 0.005 0.024 -0.018 -0.010
23.45.67.89.111 RP 1.23.4	2.597 2.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00 10.00 50.00 50.00 57.50 60.00	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2 0.6 -0.0 -0.7	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -5.6 -11.4 -5.6 -6.2 -6.8 -6.5	0.01 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.456 0.535 0.573 0.583 0-FACT 0.297 0.225 0.210 0.259 0.234 0.232	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	TOT 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046	PROF 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046	1.097 1.038 1.074 1.097 1.34 1.32 1.095 1.109 1.125 0.991 LOSS F TOT 0.077 0.034 0.005 0.024 -0.008 -0.010	MACH NO. 597 0.651 0.651 0.651 0.651 0.621 0.635 0.698 0.956 MRAM PROF 0.051 0.054 0.005 0.024 -0.018 -0.018
123456189011 RP12345618	2.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCI MEAN -7.2 -7.4 -5.2 0.6 -0.0 -0.7 -0.3	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6 -6.2 -6.8 -6.5 -6.5	007 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.535 0.573 0.583 0-FACT 0.297 0.225 0.210 0.259 0.234 0.232 0.219	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053	PROF 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053	LOSS F 1077 1081 1074 1097 1097 1099 1109 1125 0099 1005 1007 1007 1007 1007 1007 1007 1007	MACH NO. 597 0.651 0.651 0.651 0.651 0.655 0.627 0.698 0.956 MRAM PROF 0.057 0.034 0.005 0.024 -0.018 -0.014 -0.016
123456189011 R123456189	2.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.733 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50 70.00	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCL MEAN -7.2 -7.4 -5.2 0.6 -0.0 -0.7 -0.3 -0.2 -3.6	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6 -6.2 -6.8 -6.5 -6.3	007 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569 0.569	0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.456 0.535 0.573 0.583 D-FACT 0.297 0.225 0.210 0.259 0.234 0.232 0.219 0.206 0.205	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	101 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053 0.020	PROF 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053 0.020	LOSS F 1.077 1.097 1.097 1.097 1.099 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.109 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009 1.009	MACH NO. 597 0.651 0.651 0.651 0.651 0.655 0.627 0.698 0.956 MRAM PROF 0.034 0.005 0.024 -0.018 -0.016 0.006
123456189011 RP12345618	2.597 0.600 0.597 0.624 0.560 0.546 0.542 0.551 0.627 0.698 0.735 PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50	007 0.507 0.569 0.567 0.527 0.516 0.520 0.533 0.590 0.638 0.568 INCI MEAN -7.2 -7.4 -5.2 0.6 -0.0 -0.7 -0.3	IN 0.597 0.600 0.597 0.624 0.560 0.542 0.551 0.627 0.698 0.733 DENCE SS -13.4 -13.6 -11.4 -5.6 -6.2 -6.8 -6.5 -6.5	007 0.507 0.569 0.567 0.527 0.516 0.520 0.535 0.590 0.638 0.569 0.569	IN 0.524 0.536 0.531 0.518 0.466 0.457 0.450 0.535 0.573 0.583 0-FACT 0.297 0.225 0.210 0.259 0.234 0.232 0.219	0.01 0.505 0.553 0.566 0.567 0.515 0.519 0.533 0.590 0.637 0.565	0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053	PROF 0.200 0.091 0.016 0.078 -0.025 -0.032 -0.046 -0.053	LOSS F 1077 1081 1074 1097 1097 1099 1109 1125 0099 1005 1007 1007 1007 1007 1007 1007 1007	MACH NO. 597 0.651 0.651 0.651 0.651 0.655 0.627 0.698 0.956 MRAM PROF 0.057 0.034 0.005 0.024 -0.018 -0.014 -0.016

## (k) 90 Percent of design speed; reading 2822

RP 1 2 5 4 5 6 7 8 9 9 1 1 1	R40 3N 24.567 24.056 21.961 19.885 19.365 19.106 18.847 18.588 17.815 15.751 15.257	00T 24.600 24.110 22.134 20.160 19.670 19.426 19.182 18.938 18.214 16.297	27.2 25.3 26.2 31.5 31.5 31.9 32.6 32.6 31.5	BETAM 0UT 5.1 2.6 -1.4 -0.1 -3.9 -1.7 -1.6 -1.4 -1.8 1.1 4.6	27.2 25.5 26.2 31.5 31.9 32.6 32.8 31.5	DETAM OUT 5.1 2.8 -1.4 -0.1 -0.9 -1.7 -1.6 -1.4 -1.8 1.1 4.6	3N 325.9 321.7 318.3 319.6 318.1 317.6 317.1 316.6 316.6 318.6	0.999 1.001 1.001	13.88 13.75 13.75 13.66 13.54 15.46 15.37	PRESS 847:0 0.956 0.991 0.995 0.988 1.004 1.004 1.011 1.012 1.000 0.995 0.929
P-254501 89	485 IN 200.5 191.8 192.7 202.4 193.3 191.8 197.6 200.9 218.7 253.7	101.1 167.1 167.1 182.0 182.0 182.0 182.0 182.0 182.0 182.0 182.0 182.0 182.0 182.0	197.8	00T 167.1 180.9 182.0 187.4 184.8 182.9 182.8 183.8 191.9 207.3	164.8 162.1 157.9 157.6	0 VEL 0UT 166.5 180.7 181.9 187.4 184.7 182.8 182.7 183.8 191.8 207.3	95.1 105.7 101.0 100.7 100.8 101.8 104.9	VEL 0UT 14.8 8.9 -4.4 -0.3 -5.3 -5.2 -4.5 -4.5 15.5	0. 0. 0. 0.	0UT 0. 0. 0. 0.
RP: 254567-89111	485 M N 0.572 0.549 0.555 0.554 0.554 0.541 0.582 0.635 0.679	ACH NO OUT 0.473 0.516 0.523 0.539 0.531 0.526 0.526 0.526 0.529 0.554	REL M 1N 0.572 0.549 0.555 0.557 0.557 0.550 0.541 0.582 0.635 0.679	ACH NO OUT 0.473 0.516 0.523 0.539 0.531 0.526 0.526 0.529 0.554 0.598	MERID M 1N 0.509 0.498 0.498 0.475 0.467 0.455 0.455 0.455 0.517	0.471 0.471 0.515 0.522 0.539 0.536 0.526 0.526 0.529 0.554 0.547			10.934 1.042 1.052 1.086 1.121 1.128 1.157 1.166 1.120	PEAK SS MACH NO 0.572 0.555 0.555 0.585 0.585 0.586 0.582 0.641 0.891
RP 1 23 4 5 6 7 8 9 10 11	PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50 70.00 95.00	INCI MEAN -8.7 -8.8 -6.2 -1.9 -2.0 -1.5 -1.5 -2.6 -2.8 -2.0	DENCE SS -14.8 -14.9 -12.4 -8.0 -8.3 -8.2 -7.7 -7.6 -9.8 -8.9 -2.6	DEV 17.4 13.9 8.0 8.8 7.9 7.1 7.1 7.5 6.8 9.9	D-FACT 0.314 0.200 0.215 0.237 0.207 0.207 0.191 0.184 0.199 0.189	0. 0. 0. 0. 0. 0. 0.	0.220 0.048 0.036 0.058 -0.021 - -0.061 - -0.065 - 0.001 0.027	PROF 0.220 0.046 0.036 0.059 0.021 0.021	-0.006	PROF 0.084 0.018 0.012 0.018 -0.006 -0.006

# (1) 90 Percent of design speed; reading 2824

5 6 7 8 9 10 11	RADII IN 24.587 24 24.056 24 21.961 22 19.885 20 19.365 19 19.106 19 18.847 19 18.588 18 17.813 18 15.751 16 15.237 15	0UT .600 .110 .134 .160 .670 .426 .182 .938 .214	33.4 30.8 31.3 35.9 36.0 36.7 38.1 37.8 36.6 39.9	BETAM OUT 6.4 4.2 -0.2 0.4 -0.3 -0.5 -0.1 -0.0 -0.9 0.8 3.6	1N 53.4 30.8 31.3 35.9 36.0 36.7 38.1 37.8 36.6 39.9	BETAM OUT 6.4 4.2 -0.2 0.4 -0.3 -0.5 -0.1 -0.0 -0.9 0.8 3.6	522.6 522.6 521.7 521.7 521.4 520.8 319.7 521.0	RATIO 0.994 1.002 1.000 0.997 0.999 0.999 1.000 1.000 1.000	14,92 14,67 14,45 14,44 14,17 14,19 14,10 14,04 14,21 14,36	0.995 0.991 1.004 1.006 1.006 1.010 0.998 0.995
RP 1 254 561 89	204.9 14 194.5 1 188.8 14 196.9 14 190.5 14 188.6 14 188.5 14 196.5 14 212.4 1	0UT 65.9 74.6 67.5 69.0 66.0 66.0 66.0 66.1	168.8 196.9 190.3 191.2 188.6 188.3 196.5 212.4	VEL 0UT 165.9 174.6 167.5 166.5 166.2 166.2 166.1 168.6 179.1	159.5 153.9 153.4 :48.5 148.9 157.7 163.0	0UT 164.8 174.2 167.5 169.0 166.5 166.0 166.2 166.1 168.6 179.1	116.4	0UT 18.5 12.8 -0.6 1.2 -0.8 -1.4 -0.3	0. 0. 0. 0. 0. 0.	
F: 254561 89111	0.577 0 0.551 0 0.542 0 0.545 0 0.547 0 0.540 0 0.540 0 0.565 0	007 .463 .492 .476 .481 .474 .472 .473 .473 .481	0.564 0.545 0.547 0.540 0.540 0.565		0.457 0.441 0.439 0.425 0.427 0.454	0.461 0.490 0.476 0.476 0.474 0.472 0.473			1.064 1.064 1.062 1.082 1.082 1.082 1.088 1.088	588 588 588 695 695
RP 123456189111	PERCENT SPAN 5.00 10.00 50.00 55.00 57.50 60.00 62.50 70.00 90.00 95.00	INCID MEAN -2.5 -3.3 -1.1 2.6 2.3 2.6 4.0 3.4 1.5 1.5 2.5	ENCE 95 -8.6 -9.4 -7.3 -3.5 -3.6 -3.4 -2.2 -2.6 -4.6 -1.9	DEV 18.7 15.5 9.2 9.5 8.5 8.6 8.7 9.6	0-FACT 0.368 0.269 0.292 0.322 0.304 0.312 0.301 0.296 0.311	5 F F S S S S S S S S S S S S S S S S S	-0.004	0EFF PROF 0.186 0.032 0.047 -0.021 -0.034 -0.055 0.055 0.055 0.055		PR-5

TABLE VIII. - Continued.

(m) 90 Percent of design speed; reading 2839

25456	24.587 24. 24.056 24. 21.961 22. 19.685 20. 19.365 19. 19.106 19. 18.647 19. 18.588 18. 17.615 18.	UT IN 600 38. 110 35. 134 35. 160 39. 670 40. 426 42. 182 43. 938 42. 214 42.	7 5.2 4 0.4 8 1.3 4 0.7 1 0.6 8 0.6 9 0.3 0 -1.0	1N 38.7 35.7 35.4 39.8 40.4 42.1 43.8 42.9 42.0	00T 7.1 5.2 0.4 1.3 0.6 0.6 0.6	1N 340.1 334.1 326.4 325.1 324.7 324.9 325.0 323.9 322.7	RAT:0 0.994 1.001 0.999 0.998 0.999 0.997	18,51 15,51 15,34 15,00 14,88 14,64 14,61 14,52 14,46 14,66	RATIO 0.986 0.989 0.993 0.993 0.994 0.994 0.996 0.997
P-254561 89	205.6 16 196.1 16 199.7 15 194.4 15 189.3 15 189.2 15 187.5 14 197.5 14 207.6 15	5.1 205. 9.8 196. 9.8 189. 7.2 194. 5.0 189. 1.0 189. 0.1 187. 8.1 187. 5.9 190.	00T 6 165.1 1 169.8 1 159.8 1 157.2 3 153.0 2 151.0 3 150.1 5 148.1 5 145.9	158.9 159.2 154.7 149.5 144.2 143.5 135.2 137.3 141.7	007 161.8 169.1 159.8 157.2 153.0 151.0 150.1 148.1 145.8 157.0	1N 127.4 114.5 129.6 124.3 126.7 126.7 127.4 143.6	15.5 1.1 3.5 2.0 1.6 1.7 2.6 4.6		
	ABS MACH	1 NO BC	MACH NO	-	1.04 %				
F. 25.45.61 8 9	5566 0.5551 0.5554 0.5554 0.5554 0.5554 0.5554 0.5555 0.5555 0.5555 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.5557 0.55	(T (N 451 0.5) 451 0.5) 473 0.5) 480 0.5) 444 0.5) 432 0.5) 424 0.5) 424 0.5) 438 0.5)	0.47 88 0.451 51 0.473 59 0.450 54 0.444 59 0.432 59 0.426 53 0.424 54 0.418 55 0.412 57 0.444	MERID M 0.445 0.445 0.456 0.411 0.400 0.504 0.501 0.405 0.405	0.448 0.472 0.450 0.444 0.452 0.432 0.435 0.425			63 55 55 67 67 67 68 69 69	661

## (n) 100 Percent of design speed; reading 2817

	810::	120	BETAM	25	BETAM	* . * .	T.Ab		PRESS
00	4-0	-0;	DEING	"ALL	317	: ``	R4*::		41
30	:N 00"	: 5	0.1		66		***		74
*	24.58 24.60	45.1	7.5	45.	7.5	545.		15.83	1.981
2	24.156 24.11	22.2	5.5	40.2	5.5	558.5		15. 77	1.981
3	21.46" 22.15	4 39.4	1.1		1.1	528.6		15.15	1.986
	19.665 20.16	9 25 5		45.0	2.3	527.9		:4.93	/
2	19,000 20,10	45.9	6.6	43.5	2.0		* . 77		
5	19.565 19.6	46.6	1.5		1.5	528.0	1.996	14.78	1.976
ê	19,106 19,43	50.4	1.4	50.4	1.4	328.0	0.995	14.68	0.982
0	16.847 19.18.				1.3	327.9	0.995	14.64	1.985
8	10 500 10 37	51.5	1.2	51.5	:.2	X3	1.995	14.66	1.479
a	18.588 18.93	31.2	1.5	21.2	1.00	327.7			*
9	:7.8:5 18.21 :5.751 16.29	48.5	1.5	48.3		525.8	0.998	14.68	2.27
13	15. 51 16.29	44.9	2.9	44.9	2.4	323.4	1.004	14.85	1.983
	15.237 15.814	46.2	5.0		3.0	325.3	1.000	15.17	0.944
	15.257 15.81	-0.2							
	-BS .EL	REL	VE.	MERIC	151	148	5 151	WILL	SPEED
QP.		N.	001		CUT	:N	2.7	: X	0.7
							00.		W
9	203.3 165.5		165.9	148.4		159.0	21.		
2	200.5 168.0	200.3	160.0	153.1	168.0	129.2	16.		:.
3	166.5 149.	186.5	149.7	144.1	149.6	118.3	2.8	* .	2.
4	88.3 135.	188.5	135.0	131.1	134.9	: 35.1	4.6	2.	:.
	00.3 133.						•.0		
2	185.5 131.	185.5	131.3	122.2	131.3	139.5	3.5		
£ .01 B	'84.: '29.1	8 184.0	129.8	117.2	129.8		3.1		
	185.5 178.1	185.9	128.5	113.5	128.3	144.7	3.0	5.	2.
2	186.4 27. 189.9 29.	186.4	127.7	116.1	127.7	145.9		3	
	00.	100.4	120.1		122.0				
9	189.9 129.	189.9	129.0	126.4	128.9		3.3		
* *	2:5.3 :48		148.2	145.3	148.0		7.4	Q.	
	22' . 5 . 5 . 1	9 22'.9	157.8	153.6	137.6	160.2	7.3	0.	
	ABS MACH N	O REL !	MACH NO	MERID MA	ACH NO			MERIC	PEAK SS
20	ABS MACH N	O REL I	MACH NO	MERIO MA	ACH NO			MEAIL R	PEAC SS
\$P	IN OUT	IN	OUT	IN	007			IEL R	MACH NO
	3.564 3.45	IN 0.564	0.457	IN 0,412	0.453			EL R	MACH N: 1.668
•	3.564 3.45 3.563 3.46	IN 0.564 0.560	0.457 0.468	0.412 0.428	0.453 0.466			EL R	Ma(+ \) 668 878
2	3,564 3,45 3,563 3,46 3,527 3,419	IN 7 0.564 8 0.560 9 0.527	0.457 0.468 0.419	0.412 0.428 0.408	0.453 0.466 0.419			.EL R 1.18 1.69 1.638	Maica N. 1.668 1.818 1.759
2	3,564 0.45 0.563 0.46 0.527 0.41 0.533 0.37	IN 7 0.564 8 0.560 9 0.527	0.457 0.468 0.419	0.412 0.428 0.408	0.453 0.466			.EL R 1.18 1.69 1.638	Maica N. 1.668 1.818 1.759
2 3 4	3,564 0.45 0.563 0.46 0.527 0.41 0.533 0.37	IN 7 0.564 8 0.560 9 0.527 8 0.533	0.457 0.468 0.419 0.378	0.412 0.428 0.408 0.371	0.453 0.466 0.419 0.378			/EL R 1.108 1.097 1.038 1.029	MiCH N. 1.668 1.818 1.759
2 5 4 5	:N 001 0.564 0.45 0.560 0.46 0.527 0.41 0.533 0.37 0.525 0.36	7 0.564 8 0.560 9 0.527 8 0.533 7 0.525	0.457 0.468 0.419 0.378 0.367	IN 0.412 0.428 0.408 0.371 0.346	0.453 0.466 0.419 0.378 0.367			.EL R 1.08 1.097 1.038 1.029 1.075	MACH NO 668 659 661 692
25456	:N 001 0.564 0.45 0.560 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36	7 0.564 8 0.560 9 0.527 8 0.533 7 0.525 3 0.520	0.457 0.468 0.419 0.378 0.367 0.363	1N 0.412 0.428 0.408 0.371 0.346 0.331	0.453 0.466 0.419 0.378 0.367 0.363			.EL R 1.196 1.097 1.038 1.029 1.075	X104 \: 668 818 759 861 832
25456	:N 001 0.564 0.45 0.560 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 3 0.520 9 0.520	0.457 0.458 0.419 0.367 0.367 0.363 0.359	1N 0.412 0.428 0.408 0.371 0.346 0.331 0.321	0.1 0.453 0.466 0.419 0.378 0.367 0.363			.EL R 1.08 1.097 1.038 1.029 1.075 1.108	MACH N. 0.666 0.818 0.759 0.661 0.692
25456	:N 001 0.564 0.45 0.560 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 3 0.520 9 0.520	0.457 0.458 0.419 0.367 0.367 0.363 0.359	1N 0.412 0.428 0.408 0.371 0.346 0.331 0.321	0.1 0.453 0.466 0.419 0.378 0.367 0.363			EL R . 58 . 536 . 529 1.575 1.108	MACH N. 0.666 0.818 0.759 0.661 0.692
254561.8	:N 001 0.564 0.45 0.560 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.528 0.35	1N 0.564 0.560 9 0.527 9 0.535 7 0.525 3 0.520 9 0.528	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357	IN 0,412 0,428 0,408 0,371 0,346 0,331 0,321 0,329	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359			EL R . 58 . 536 . 529 1.575 1.108	MACH N; 0.868 0.8759 0.861 0.892 0.993 0.935
254561.89	:N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.535 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.528 0.35 0.540 0.36	1N 0.564 0.560 9.527 9.533 7.525 3.520 9.520 9.528 1.540	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.357	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.359	0.1 0.453 0.466 0.419 0.578 0.567 0.363 0.359 0.357			.EL R 56 59 536 55 1.108 55	MACH N. 0.868 0.8759 0.861 0.892 0.933 0.935
254501.890	:N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.528 0.35 0.540 0.36	7N 0.564 0.563 0.527 0.525 0.525 0.526 0.520 0.528 0.540 0.589	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 2.361 0.418	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417			. 58 . 59 . 539 . 529 . 575 . 158 . 135 . 525	M4(→ \) 0.666 0.6759 0.661 0.692 0.931 0.933 0.660 0.633
254561.89	:N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.528 0.35 0.540 0.36	7N 0.564 0.563 0.527 0.525 0.525 0.526 0.520 0.528 0.540 0.589	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.359	0.1 0.453 0.466 0.419 0.578 0.567 0.363 0.359 0.357			.EL R 56 59 536 55 1.108 55	MACH N. 0.868 0.8759 0.861 0.892 0.933 0.935
254501.890	:N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.528 0.35 0.540 0.36	7N 0.564 0.563 0.527 0.525 0.525 0.526 0.520 0.528 0.540 0.589	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 2.361 0.418	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417			. 58 . 59 . 539 . 529 . 575 . 158 . 135 . 525	M4(→ \) 0.666 0.6759 0.661 0.692 0.931 0.933 0.660 0.633
254501.890	:N 00° 3.564 3.45' 3.563 3.46' 3.527 3.41' 3.525 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36' 3.520 3.36'	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 9 0.520 9 0.528 1 0.540 8 0.589 7 0.638	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417 0.386	1,000	APPP	. 56 . 597 . 538 . 529 1.575 1.108 . 135 . 135 . 135 . 135 . 135	M4(→ \) 0.666 0.818 0.851 0.692 0.935 0.935 0.935 1.026
254501.890	:N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 3 0.520 9 0.528 1 0.540 8 0.589 7 0.638	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 2.361 0.418	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417	LOSS C		.EL R 56 57 58 55 155 156 55 156 55 156 55 156	MACH NO. 6686 0.818 0.859 0.861 0.892 0.931 0.933 0.880 0.833
254501.890	N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 3 0.520 9 0.528 1 0.540 8 0.589 7 0.638	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417 0.386	TOT	PROF		MACH NO. 6686
254561.8901.	N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36	7 0.564 8 0.560 9 0.527 8 0.535 7 0.525 3 0.520 9 0.528 1 0.540 8 0.589 7 0.638	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417 0.386	TOT	PROF		MACH NO. 6686
25.4561.8955.	N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT 11 SPAN MED 5.00 7	7 0.564 8 0.560 9 0.527 9 0.525 3 0.520 9 0.528 1 0.540 8 0.589 7 0.638 NCIDENCE AN SS	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.417 0.386	TOT 0.143	PROF 0.143		MACH NO. 6686   0.818   0.828   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938
25.4561.8955.	N 001 0.564 0.45 0.563 0.46 0.527 0.415 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.410 0.638 0.36 PERCENT 19 SPAN MED 5.00 7.	7 0.564 8 0.560 9 0.527 8 0.535 7 0.526 9 0.520 9 0.528 1 0.540 8 0.589 7 0.638 NCIDENCE AN SS	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.366	TOT 0.143 0.104	PROF 0.143 0.104		MACH NO. 6686   0.818   0.828   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938   0.938
25.4561.8955.	N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT 11 SPAN MED 5.00 7.	1N 0.564 0.560 0.527 0.525 0.525 0.520 0.528 0.540 0.589 0.638 NCIDENCE AN SS 1.1 -0.1	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.366	TOT 0.143 0.104 0.080	PROF 0.143 0.104 0.080	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.030 1.030 1.035 1.035 1.039 1.039 1.039	MACH NO. 0.666 0.6759 0.667 0.692 0.935 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.685 0.
- 25.4561.89511 P1254	IN 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT II SPAN MED 5.00 7. 10.00 6. 30.00 7.	1N 0.564 0.560 0.527 0.525 0.525 0.520 0.528 0.540 0.589 0.638 NCIDENCE AN SS 1.1 -0.1 0.8 6.4	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387 0.51	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.366	TOT 0.143 0.104 0.080 0.146	PROF 0.143 0.104 0.080 0.146		MACH NO. 1668 1.0818 1.082 1.083 1.026 ARAM PROF 1.025 1.026 1.026
- 25.4561.89511 P1254	N 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT 11 SPAN MED 5.00 7.	1N 0.564 0.560 0.527 0.525 0.525 0.520 0.528 0.540 0.589 0.638 NCIDENCE AN SS 1.1 -0.1 0.8 6.4	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.321 0.329 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.386 EFF	TOT 0.143 0.104 0.080 0.146 0.128	PROF 0.143 0.104 0.080	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.030 1.039 1.039 1.039 1.039	MACH NO. 10.666   1.666   1.759   1.661   1.692   1.933   1.626   1.626   ARAM PROF   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626
- 25.4561.89511 P1254	IN 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT II SPAN MED 5.00 7. 10.00 6. 30.00 7. 50.00 12.	1N 0.564 0.560 0.527 0.525 0.525 0.520 0.528 0.540 0.589 0.638 NCIDENCE AN SS 1.1 -0.1 0.8 6.4 1.9	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.361 0.418 0.387	0.412 0.428 0.408 0.371 0.346 0.331 0.329 0.359 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.386 EFF	TOT 0.143 0.104 0.080 0.146 0.128	PROF 0.143 0.104 0.080 0.146 0.128	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.030 1.039 1.039 1.039 1.039	MACH NO. 10.666   1.666   1.759   1.661   1.692   1.933   1.626   1.626   ARAM PROF   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626
- 25.4561.89511 P1254	IN 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT II SPAN MED 5.00 7. 10.00 6. 30.00 7. 50.00 12. 55.00 15.	7 0.564 8 0.563 9 0.527 8 0.525 3 0.525 3 0.520 9 0.528 1 0.540 8 0.589 7 0.638 NCIDENCE AN SS 1 1 1 0.8 6 6.4 9 0.6	0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387 0.51 10.6	0.412 0.428 0.408 0.371 0.346 0.331 0.329 0.359 0.417 0.442	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.386 EFF	TOT 0.143 0.104 0.080 0.146 0.128 0.104	PROF 0.143 0.104 0.080 0.146 0.128 0.104	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.030 1.039 0.039 0.039 0.033	MACH NO. 10.666   1.666   1.759   1.661   1.692   1.933   1.626   1.626   ARAM PROF   1.626   1.626   1.626   1.627   1.627   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628   1.628
- 25.4561.89511 P1254	IN 001 0.564 0.45 0.563 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.540 0.36 0.589 0.41 0.638 0.36 PERCENT II SPAN MED 5.00 7. 10.00 6. 30.00 7. 50.00 12. 55.00 15. 60.00 17.	7 0.564 8 0.563 9 0.527 8 0.525 7 0.528 1 0.520 7 0.528 1 0.540 8 0.589 7 0.638 NCIDENCE AN SS 1 1.1 1 0.8 1 0.8	0.01 0.457 0.468 0.419 0.378 0.367 0.363 0.359 0.357 0.418 0.387 0.51 10.6 10.5 10.8 10.3	0.412 0.428 0.408 0.371 0.346 0.331 0.329 0.359 0.417 0.442 0-FACT 0.406 0.370 0.410 0.498 0.514 0.519 0.529	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.366 EFF	TOT 0.143 0.104 0.080 0.146 0.128 0.104	PROF 0.143 0.104 0.080 0.146 0.128 0.104 0.103	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.030 1.039 0.039 0.031	MACH NO. 10.666
- 25.4561.89511 P1254	IN 001 0.564 0.45 0.565 0.46 0.527 0.41 0.533 0.37 0.525 0.36 0.520 0.36 0.520 0.35 0.520 0.35 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.520 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.3630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 0.5630 0.36 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1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   1.626   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0.370 0.410 0.410 0.514 0.519 0.529 0.538 0.523	0.1 0.453 0.466 0.419 0.578 0.567 0.563 0.359 0.357 0.361 0.417 0.366 EFF	TOT 0.143 0.104 0.080 0.146 0.128 0.104 0.103 0.124	PROF 0.143 0.104 0.080 0.146 0.128 0.104 0.103 0.124 0.130	LCSS P 1.039 1.039 1.039 1.039 1.030 1.030 1.039 0.039 0.031 0.036 0.037	MACH NO. 0.666 0.6759 0.667 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 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## (o) 100 Percent of design speed; reading 2818

RP 1 2 3 4 5 6 7 8 9 11 11	1N 24.587 24.056 21.961 19.883 19.365 19.106 18.847 18.588 17.813 15.751	24.110 22.134 20.160 19.670 19.426 19.182 18.938 18.214	1N 45.3 42.5 43.7 50.6 52.8 53.8 54.4 54.1 49.8 45.4	1.6	1N 45.3 42.5 43.7 50.6 52.8 53.8 54.4 54.1	0UT 7.7 5.7 1.8 1.6 1.2 1.0 0.9 1.5 3.4	330.4 330.0 329.2 328.6 328.5 328.3 326.3 323.2	RAT10 0.994 0.997 0.999 0.995 0.996 0.997	15.77 15.78 15.10 14.97 14.79 14.72 14.67	0.977 0.966 0.971 0.974 0.976 0.975 0.975
	485	VEL	REL	VEL	MERI		TAN	G VEL	WHEEL	SPEED
QP.	:N	OUT	IN	DUT	IN	OUT	IN	OUT	:N	DUT
1	198.9	163.9	198.9	163.9	140.0	162.4	:4:.3	22.0	٥.	٥.
2	199.5	163.4	199.5	163.4	147.1	162.5	134.8	16.3	٥.	٥.
254561 00	165.7	141.0	183.7	141.0	132.7	140.9	127.0	4.5	٥.	2. 2.
-	188.3	128.6	188.3	128.6	119.4	128.6	145.6	3.7	٥.	
3	83.5	123.9		124.9	108.4	124.8	147.3	2.7		÷.
	165.0	123.0	185.0	123.0	106.6	123.0	148.6	2.2	ž.	:: ::
9	84.3	122.7		122.7	108.0	122.7	149.3	2.0	÷.	::
ä	188.8	25.4		125.4		125.4	144.2	3 4	ă.	::
•:	2:3.9	144.3		144.3	143.1	144.5	145.2	3.4 8.7	ž.	::
	22' .6	133.1		133.1		132.9		6.2	3.	::
6 - 25 4 5 to 1 8 9 19 -	ABS M 1N 0.556 0.558 0.532 0.532 0.517 0.521 0.536 0.637	ACH NO 0.450 0.451 0.359 0.359 0.346 0.345 0.345 0.342 0.351 0.406 0.573	IN 0.550 0.556 0.518 0.532 0.522	ACH NO 0UT 0.450 0.451 0.393 0.359 0.346 0.346 0.342 0.351 0.406 0.373	MERIO M IN 0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.411 0.438				MER:0 	* 5/5
- 25.45.61 89.5	IN 0.550 0.556 0.518 0.532 0.517 0.521 0.536 0.537 PERCENT	0.450 0.451 0.451 0.393 0.359 0.346 0.345 0.342 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.517 0.521 0.536 0.585 0.637	0.450 0.451 0.393 0.359 0.348 0.346 0.343 0.342 0.351	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411	0.446 0.449 0.393 0.359 0.348 0.345 0.343 0.343	LOSS C	CEFF		MACH NO 687 657 657 659 959 966 971 969 969 973
25.45.61 83.51	IN 0.550 0.556 0.518 0.532 0.517 0.521 0.536 0.637 PERCENT	0.450 0.451 0.393 0.359 0.348 0.346 0.343 0.342 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.517 0.521 0.536 0.585 0.637	0.450 0.451 0.451 0.393 0.348 0.346 0.343 0.342 0.351 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.345 0.373	101	PROF		MACH NO 687 687 682 945 959 966 970 969 937 933
25.45.61 @ 9.55 P.	IN 0.556 0.556 0.552 0.532 0.517 0.521 0.536 0.537 PERCENT SPAN 5.00	0.450 0.451 0.393 0.359 0.348 0.346 0.343 0.342 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.518 0.517 0.521 0.536 0.637 DENCE SS 3.2	0.450 0.451 0.451 0.393 0.348 0.346 0.343 0.342 0.351 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.345 0.351	101	PROF 0.149		MACH NO 687 687 682 945 959 966 970 969 937 933
P-2	IN 0.550 0.556 0.518 0.532 0.517 0.521 0.536 0.537 PERCENT SPAN 5.00	0.450 0.451 0.393 0.359 0.346 0.345 0.345 0.406 0.373 INCL MEAN 9.4	IN 0.550 0.556 0.518 0.532 0.522 0.518 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.2 2.2	00T 0.450 0.451 0.393 0.348 0.346 0.343 0.342 0.351 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438	0.446 0.449 0.393 0.359 0.348 0.345 0.345 0.351 0.405 0.373	0.149 0.153	PROF 0.149 0.155		MACH NO 687 687 682 945 959 966 970 937 933
P-2	IN 0.550 0.556 0.552 0.522 0.518 0.517 0.525 0.637 PERCENT SPAN 5.00 50.00	0.450 0.451 0.451 0.359 0.348 0.346 0.345 0.345 0.351 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.518 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.2 2.2 5.2	00T 0.450 0.451 0.393 0.348 0.346 0.343 0.342 0.351 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.351 0.405 0.373	101 0.149 0.153 2.135	0.149 0.153 0.155		MACH NO. 687 687 687 682 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683 683
P-2	IN 0.556 0.556 0.552 0.522 0.518 0.521 0.525 0.537 PERCENT SPAN 5.00 50.00 50.00	0.450 0.451 0.393 0.359 0.346 0.345 0.345 0.406 0.373 INCI MEAN 9.4 9.4	IN 0.550 0.556 0.518 0.532 0.522 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.2 2.2 5.2	0.450 0.451 0.451 0.393 0.348 0.346 0.345 0.406 0.373 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438 0.437 0.407 0.407	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.351 0.373 EFF	101 0.149 0.153 0.155 0.195	PROF 0.149 0.153 0.155 0.195		MACH NO. 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687
P-2	IN 0.556 0.556 0.552 0.552 0.552 0.5536 0.557 PERCENT 5.00 50.00 50.00 50.00 50.00	0.450 0.451 0.393 0.359 0.346 0.345 0.345 0.345 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.2 2.2 5.2 11.2	0.450 0.451 0.451 0.393 0.348 0.346 0.345 0.406 0.373 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438 0.407 0.407 0.407 0.407 0.407	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.373 EFF	101 0.149 0.153 0.135 0.195 0.169	PROF 0.149 0.153 0.155 0.155 0.169		MACH NO. 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687 687
- 254561 @ 9151 P - 254561	IN 0.556 0.556 0.556 0.552 0.552 0.552 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536	0.450 0.451 0.451 0.393 0.359 0.346 0.345 0.345 0.345 0.351 0.406 0.373	IN 0.550 0.556 0.518 0.532 0.522 0.521 0.536 0.536 0.585 0.637 DENCE SS 3.22 5.2 11.2 12.9	0.450 0.450 0.451 0.393 0.348 0.346 0.345 0.345 0.351 0.351 0.351 0.351 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438 0.407 0.407 0.407 0.407 0.407 0.407	0.446 0.449 0.393 0.359 0.345 0.345 0.345 0.351 0.351 0.373	101 0.149 0.153 0.135 0.195 0.169 0.153	PROF 0.149 0.155 0.155 0.195 0.169 0.155		MACH NO. 1687 1.687 1.687 1.682 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.959 1.95
- 254561 @ 9151 P - 254561	IN 0.556 0.556 0.556 0.552 0.552 0.552 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536 0.5536	0.450 0.451 0.393 0.359 0.346 0.343 0.342 0.351 0.406 0.373 INCI MEAN 9.4 11.4 11.4 11.9 12.9 20.3	IN 0.550 0.556 0.518 0.532 0.522 0.521 0.536 0.536 0.585 0.637 DENCE SS 3.22 5.2 11.2 12.9	0.450 0.450 0.451 0.393 0.348 0.346 0.345 0.345 0.351 0.351 0.351 0.351 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438 0.407 0.407 0.407 0.407 0.407	0.446 0.449 0.393 0.348 0.345 0.345 0.351 0.351 0.373 EFF	101 0.149 0.153 0.155 0.169 0.153 0.142	PROF 0.149 0.153 0.155 0.195 0.169 0.153 0.142 0.145	EL 4 60 62 56 54 56 56 56 57 57 58 58 58 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 56 	MACH NO. 687 657 657 659 959 966 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 
- 254561 8955- P- 254561 89	2.556 2.556 2.556 2.552 2.518 2.522 2.518 2.526 2.526 2.526 2.536 2.537 PERCENT 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.0000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.000 50.00	0.450 0.451 0.393 0.359 0.348 0.346 0.343 0.342 0.351 0.406 0.373 1NCI MEAN 9.4 11.4 11.4 11.4 11.4 11.4 11.4 11.4	IN 0.550 0.556 0.518 0.532 0.522 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.22 5.22 11.2 12.9 13.8 14.1	0.450 0.451 0.451 0.393 0.348 0.346 0.345 0.345 0.373 0.373 0.50 10.60 11.25 10.1 9.8 9.7	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.346 0.411 0.438 0.407 0.407 0.407 0.407 0.407 0.407 0.407	0.446 0.449 0.393 0.345 0.345 0.345 0.351 0.351 0.373 EFF	101 0.149 0.153 0.155 0.169 0.153 0.142 0.145	PROF 0.149 0.153 0.155 0.195 0.169 0.153 0.142 0.145 0.140	EL 6: 552 1: 552 1: 553 1:	MACH NO 687 687 687 682 966 966 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969 969
- 254561 @ 9151 P - 254561	IN 0.556 0.556 0.552 0.552 0.552 0.5536 0.557 PERCENT 5.00 50.00 50.00 50.00 50.00	0.450 0.451 0.451 0.355 0.359 0.346 0.345 0.345 0.345 0.351 0.406 0.373 1NCI MEAN 9.4 11.4 19.9 20.3 19.8	IN 0.550 0.556 0.518 0.532 0.522 0.518 0.517 0.521 0.536 0.585 0.637 DENCE SS 3.2 2.2 11.2 12.9	0.450 0.451 0.451 0.393 0.348 0.346 0.345 0.345 0.406 0.373 0.406 0.373	0.387 0.410 0.374 0.337 0.316 0.306 0.301 0.305 0.411 0.438 D-FACT 0.407 0.407 0.407 0.407 0.407 0.407 0.407 0.407 0.561 0.562 0.564 0.566	0.446 0.449 0.393 0.348 0.345 0.345 0.351 0.351 0.373 EFF	101 0.149 0.153 0.155 0.169 0.153 0.142	PROF 0.149 0.153 0.155 0.195 0.169 0.153 0.142 0.145		MACH NO. 1687 1.687 1.687 1.682 1.945 1.959 1.966 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.969 1.96

TABLE VIII, - Continued,

## (p) 100 Percent of design speed; reading 2819

254561.89	24.587 24.056 21.961 19.883 19.365 19.106 18.847 18.588 17.815	001 24,600 24,110 22,134 20,160 19,670 19,426 19,426 19,182 18,938 18,214	1N 46.6 43.0 42.2 45.9 47.7 49.9 50.8 49.8	1.8 2.3 1.1 1.0 1.2	1N 46.6 43.0 42.2 45.9 47.7 49.9 50.8 49.8 47.6	1.8 2.3 1.1 1.0 1.2 1.3	1N 360.7 354.8 342.1 338.3 338.0 338.1 338.4 337.1	0.097 0.997 0.996 0.994 0.995 0.995	13.74 17.74 16.64 16.35 16.21 16.17 16.21	0.974 0.977 0.977 0.972
10	15.751 15.237	15.814	48.3	5.8 3.5		3.8 3.5			16.15	0.971 0.922
P - 254501 89	4BS	VEL 00T 185.7 186.2 169.6 154.8 147.4 144.9 143.9 142.3 159.8	REL (N 224.1 224.2 212.0 212.9 207.5 205.6 206.3 209.1 210.9	VEL 001 185.7 185.2 169.6 154.8 147.4 144.9 143.9 142.3 139.8	MERII IN 154.0 164.0 156.9 148.2 139.7 132.5 130.4 134.9 142.5	184.1 185.5 169.5 154.6 147.4 144.8 143.9 142.3	TAN (N 162.8 152.9 142.5 153.6 153.5 157.3 159.9 159.7	6 VEL 007 25.9 16.0 5.3 6.2 2.8 2.9 3.1	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	SPEED
	10C W									
RP: 254567 89111	0.610 0.616 0.591 0.598 0.582 0.576 0.578	0.388	IN 0.610 0.616 0.591 0.598 0.582 0.576	0.502 0.502 0.507 0.466 0.428 0.407 0.400 0.398 0.394 0.388 0.416 0.385	0.579 0.401 0.424	0.498 0.505 0.468 0.428 0.427 0.403 0.398 0.394 0.387			VEL 9 1.196 1.31 1.044 1.055 1.094	PE4K SS MACH NO 0.959 0.966 0.967 0.996 1.005 0.957 1.169

TABLE VIII. - Continued.

(q)	100	Percent	oî	design	speed;	reading	2914

2 5 4 5 6 7 8	24.587 2 24.056 2 21.961 2 19.885 2 19.365 1 19.106 1 18.847 1	007 24.600 24.110 22.134 20.160 19.670 19.426 19.182	1N 43.6 40.1 40.2 43.7 44.3 45.7 47.0 46.4	007 6.8 4.5 0.7 1.4 -0.1 -0.2	43.6 40.1 40.2 43.7 44.3 45.7 47.0	00T 6.8 4.5 0.7 1.4 -0.1 -0.2	1N 357.7 350.0 339.9 336.8 335.9 335.8 335.8	0.990 0.997 0.997 0.997 0.996 0.996 0.996	1N 17.46 17.39 16.80 16.47 16.12 16.05 15.92 15.96 16.09	0.972 0.984 0.977 0.986 0.986 0.993 0.991 0.982
<b>QP</b>	:N	OUT	IN	OUT	MER II	007	TAN	G VEL	WHEEL IN	SPEED
2	224.2	178.2		178.2	162.3	176.9 182.4	154.8	21.0	0. 0.	:: ::
3	211.1	151.1	211.1	171.1	161.3	171.1	136.2	2.1	٥.	٥.
5	214.2	155.3	214.2	161.7	154.7	155.3	146.1	-0.3	3. 3.	å. 8.
254561 80	206.3	153.6	206.3	153.6	144.1	153.6	147.7	-0.5	0.	2.
8	2:6.8	153.5	204.2 206.8	153.5 153.7	142.5	153.7	149.4	0.4	ð. 0.	::
	214.7	155.1	214.7	155.1	153.4	155.1	150.3	1.9	٥.	2.
.:	244.4	4:.0	219.1	140.6	151.2	140.4	158.6	8.4	ð. ð.	÷:
F-254561-89011	0.563 0.560 0.574 0.582 0.608 0.623	0.483 0.500 0.474 0.449	0.613 0.610 0.591 0.603 0.583 0.580 0.574 0.582 0.608 0.623	0.500 0.474 0.449 0.431 0.427 0.427	0.418 0.405 0.391 0.401 0.434 0.430	0.474 0.469 0.474 0.474 0.431 0.427 0.427 0.427 0.432			1.090 1.081 1.045 1.046 1.066 1.078	921

#### TABLE VIII, - Concluded,

## (r) 100 Percent of design speed; reading 2918

	RAD	11	ABS	BETAM	REL	BETAM	TOTA	L TEMP	TOTAL	PRESS
RP	IN	OUT	IN	OUT	IN	OUT	:N	RAT:0	IN	RATIO
1	24.587		41.7	6.7	41.7	6.7	354.9	0.991	17.22	u.958
2	24.056		57.1	4.2	37.1	4.2	346.6	1.331		0.978
3	21.961		33.4 42.1	1.3	38.4 42.1	1.3		0.998		0.983
	19.565		42.8	-0.5	42.8	-2.5		0.997	15.65	
6	19.106		43.9	-0.7		-0.7		0.997		0.992
5 6 7	18.847		45.1			-0.4	555.9			0.998
8	18.538		44.6	-0.3		-0.3	532.7	0.999	15.62	0.999
9	17.613	18.214	42.7	0.3		0.3		0.997	15.80	0.990
10	15.751		44.6	1.6				1.004		0.979
11	15.237	15.814	46.2	5.4	46.2	3.4	334.1	0.998	16.28	0.922
		VEL		VEL		D VEL		G VEL	WHEEL	
RP	IN.	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT
1	225.3 219.8	178.2	225.3	163.2	168.3	177.0 182.7	149.3	20.7	o.	٥.
3	210.5	174.5	210.3	174.5	164.9	174.5	130.5	1.9	0. 0.	0.
ž	214.0	166.1	214.0	166.1		166.1	143.6	3.7	õ.	õ.
	206.4	158.6	206.4	158.6		158.6	140.4	-1.3		ō.
ô	205.0	156.9	205.0	156.9	147.8	156.9	142.2	-1.9		0.
567.09	202.5	156.9	202.3	156.9	142.7	156.9	143.4	-1.0		0.
Ş	203.7	157.6	203.7	157.6	145.1	157.6	143.0	-0.6		0.
	213.6	161.3	213.6	161.3	157.1	161.3	144.8	0.8	٥.	0.
10	221.8 245.6	157.7 148.0	221.8 245.6	148.0		157.6 147.8				٥.
	2-3.0	1-0.0	2-3.6	140.V	163.9	147.0	177.	8.7	0.	٥.
	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO			MERID	PEAK SS
RP	ABS M	ACH NO	REL M	ACH NO	MERID M	ACH NO				PEAK SS MACH NO
1	IN 0.619	0.485	IN 0.619	0UT 0.485	IN 0.462	0.482			VEL R	MACH NO 0.922
1	0.619 0.610	0.485 0.503	IN 0.619 0.610	0.485 0.503	IN 0.462 0.467	0.482 0.502			VEL R 1.052 1.043	0.922 0.828
2 3	0.619 0.610 0.590	0.485 0.503 0.485	0.619 0.610 0.590	0.485 0.503 0.485	0.462 0.467 0.463	0.482 0.502 0.485			VEL R 1.052 1.043 1.058	MACH NO 0.922 0.628 0.628
2 3 4	0.619 0.610 0.590 0.604	0.485 0.503 0.485 0.465	IN 0.619 0.610 0.590 0.604	0.485 0.503 0.485 0.485	0.462 0.467 0.463 0.448	0.482 0.502 0.485 0.463			VEL R 1.052 1.043 1.058 1.046	MACH NO 0.922 0.828 0.828 0.899
2 3 4	IN 0.619 0.610 0.590 0.604 0.582	0.485 0.503 0.485 0.463	IN 0.619 0.610 0.590 0.604 0.582	0.485 0.503 0.485 0.463 0.442	IN 0.462 0.467 0.463 0.448 0.427	0.482 0.502 0.485 0.463 0.442			VEL R 1.052 1.043 1.058 1.046 1.048	MACH NO 0.922 0.628 0.628 0.699 0.872
2 3 4	IN 0.619 0.610 0.590 0.604 0.582 0.579	0.485 0.503 0.485 0.463 0.442 0.437	IN 0.619 0.610 0.590 0.604 0.582 0.579	0.485 0.503 0.485 0.463 0.442 0.442	IN 0.462 0.487 0.463 0.448 0.427 0.417	0.482 0.502 0.485 0.463 0.442 0.437			VEL R 1.052 1.043 1.058 1.046 1.048 1.062	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683
1 2 3 4 5 6 7	0.619 0.610 0.590 0.604 0.582 0.579	0.485 0.503 0.485 0.463 0.442 0.437	IN 0.619 0.610 0.590 0.604 0.582	0.485 0.503 0.485 0.463 0.442 0.437	0.462 0.467 0.463 0.448 0.427 0.417	0UT 0.482 0.502 0.465 0.463 0.442 0.437			VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689
2 3 4	0.619 0.610 0.590 0.604 0.582 0.579	0.485 0.503 0.485 0.463 0.442 0.437	IN 0.619 0.610 0.590 0.604 0.582 0.579	0.485 0.503 0.485 0.463 0.442 0.442	0.462 0.467 0.463 0.448 0.427 0.417 0.402	0UT 0.482 0.502 0.465 0.463 0.442 0.437			VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683
1 2 3 4 5 6 7 8 9	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.570 0.575 0.666 0.633	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446	0.482 0.502 0.405 0.465 0.463 0.442 0.437 0.437 0.440 0.452			VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873
1 2 3 4 5 6 7 8 9	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.570 0.575	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452	0.462 0.467 0.463 0.448 0.427 0.417 0.402 0.410	0.482 0.502 0.405 0.465 0.463 0.442 0.437 0.437 0.440 0.452			VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873
1 2 3 4 5 6 7 8 9	0.619 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449	0.482 0.502 0.485 0.465 0.463 0.442 0.437 0.437 0.440 0.452 0.410	1000	AFFF	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892
1 2 3 4 5 6 7 8 9 10	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446	0.482 0.502 0.485 0.465 0.463 0.442 0.437 0.437 0.440 0.452 0.410	LOSS C		VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130
1 2 3 4 5 6 7 8 9 10 11	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449	0.482 0.502 0.405 0.465 0.463 0.442 0.437 0.437 0.440 0.452 0.410	TOT	PROF	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130
1 2 3 4 5 6 7 8 9 10 11	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.467 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486	0.482 0.502 0.485 0.465 0.463 0.442 0.457 0.457 0.440 0.410 EFF	TOT 0.136	PROF 0.186	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130
1 2 3 4 5 6 7 8 9 10 11	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 33.00	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411 INCL MEAN 5.8 3.0	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449	0.482 0.502 0.405 0.465 0.463 0.442 0.437 0.437 0.440 0.452 0.410	TOT	PROF	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 33.00 50.00	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8 3.0 6.0 8.9	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.371 0.301 0.427	0.482 0.502 0.485 0.465 0.442 0.457 0.457 0.440 0.410 EFF	TOT 0.135 0.093 0.042 0.080	PROF 0.186 0.098 0.042 0.083	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870 LOSS P TOT 0.071 0.037 0.015 0.025	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 33.00 55.00	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8 3.0 6.0 8.9 9.2	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7 3.0	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.450 0.371 0.301 0.427 0.439	0.482 0.502 0.485 0.465 0.442 0.457 0.457 0.440 0.410 EFF	TOT 0.136 0.093 0.042 0.080 0.045	PROF 0.186 0.098 0.042 0.083 0.045	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870  LOSS F TOT 0.071 0.037 0.015 0.025 0.014	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025 0.014
1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 33.00 55.00 57.50	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.411 INCL MEAN 5.8 3.0 6.0 8.9 9.2	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7 3.0 3.9	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.452 0.440 0.411	0.462 0.487 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.450 0.371 0.301 0.427 0.439 0.445	0.482 0.502 0.405 0.465 0.442 0.437 0.437 0.440 0.410 EFF	TOT 0.136 0.093 0.042 0.060 0.045 0.040	PROF 0.196 0.098 0.042 0.083 0.045 0.045	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870  LOSS F TOT 0.071 0.037 0.015 0.025 0.014	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025 0.014
1 23 4 5 6 7 8 9 10 11 RP 1 23 4 5 6 7	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 55.00 57.50 60.00	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8 3.0 6.0 8.9 9.2 10.0	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7 3.0 3.9 4.9	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 0EV 19.0 15.5 10.0 13.2 6.4 6.1 8.4	0.462 0.467 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.450 0.371 0.301 0.427 0.439 0.439	0.482 0.482 0.502 0.485 0.463 0.442 0.437 0.437 0.440 0.410 EFF	TOT 0.136 0.093 0.042 0.080 0.045 0.045 0.009	PROF 0.196 0.098 0.042 0.083 0.045 0.040 0.049	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870  LOSS F TOT 0.071 0.037 0.015 0.025 0.014 0.012	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025 0.014 0.012
1 23 4 5 6 7 8 9 10 11 RP 1 23 4 5 6 7 8	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 55.00 57.50 62.50	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8 3.0 6.0 8.9 9.2 10.0	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7 3.0 3.9 4.9	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.437 0.440 0.411 0EV 19.0 15.3 10.0 10.2 8.4 8.4	0.462 0.467 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.450 0.371 0.301 0.427 0.439 0.434 0.434	0.482 0.502 0.405 0.465 0.442 0.437 0.437 0.440 0.410 EFF	707 0.136 0.093 0.042 0.080 0.045 0.040 0.009	PROF 0.186 0.098 0.042 0.083 0.045 0.040 0.049	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870  LOSS F TOT 0.071 0.037 0.015 0.025 0.014 0.012 0.003	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025 0.014 0.012 0.003
1 23 4 5 6 7 8 9 10 11 RP 1 23 4 5 6 7	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.606 0.633 0.703 PERCENT SPAN 5.30 10.00 55.00 57.50 60.00	0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 INCL MEAN 5.8 3.0 6.0 8.9 9.2 10.0	IN 0.619 0.610 0.590 0.604 0.582 0.579 0.575 0.666 0.633 0.703 DENCE SS -0.4 -3.1 -0.2 2.7 3.0 3.9 4.9	0UT 0.485 0.503 0.485 0.463 0.442 0.437 0.437 0.440 0.411 0EV 19.0 15.5 10.0 13.2 6.4 6.1 8.4	0.462 0.467 0.463 0.448 0.427 0.417 0.402 0.410 0.446 0.449 0.486 D-FACT 0.450 0.371 0.301 0.427 0.439 0.439	0.482 0.482 0.502 0.485 0.463 0.442 0.437 0.437 0.440 0.410 EFF	TOT 0.136 0.093 0.042 0.080 0.045 0.045 0.009	PROF 0.196 0.098 0.042 0.083 0.045 0.040 0.049	VEL R 1.052 1.043 1.058 1.046 1.048 1.062 1.099 1.086 1.027 1.002 0.870  LOSS F TOT 0.071 0.037 0.015 0.025 0.014 0.012	MACH NO 0.922 0.628 0.628 0.699 0.872 0.683 0.689 0.882 0.873 0.892 1.130 PARAM PROF 0.071 0.037 0.015 0.025 0.014 0.012

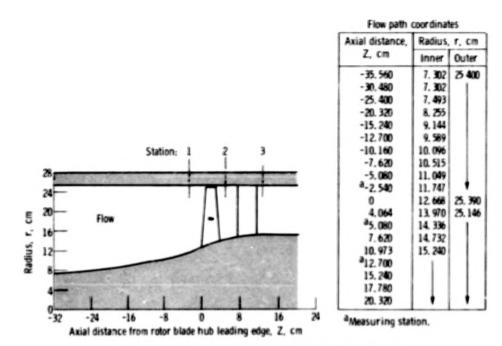


Figure 1. - Flow path for stage 20-17 showing instrumentation location.

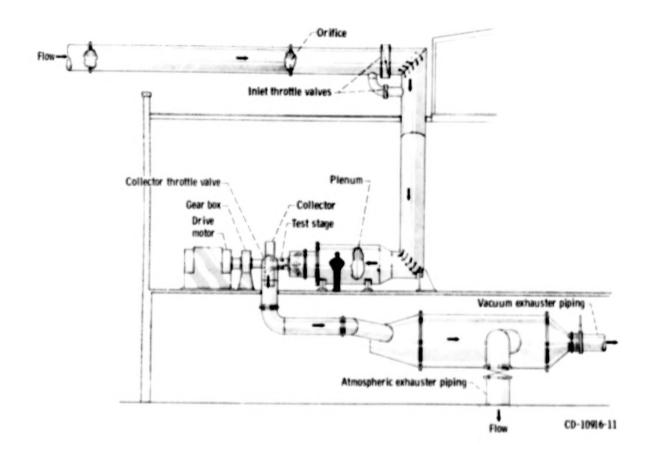


Figure 2. - Single-stage compressor facility,

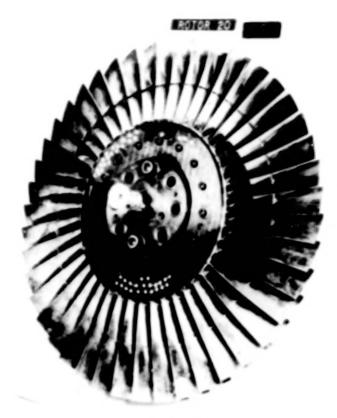
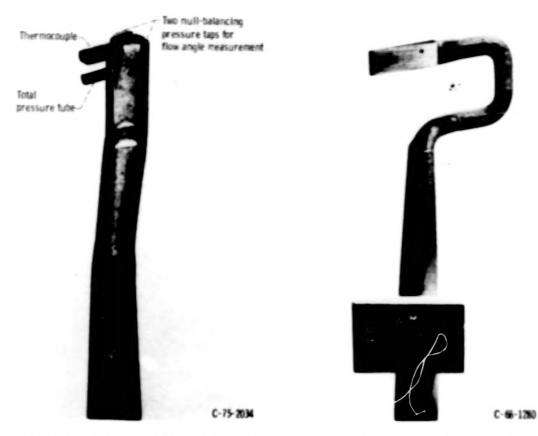


Figure 3. - Rotor 20.



Figure 4. - Stater 17.



 (a) Combination total pressure, total temperature, and flow angle probe. (b) Static pressure probe, 8° C-shaped wedge.

Figure 5. - Survey probes.

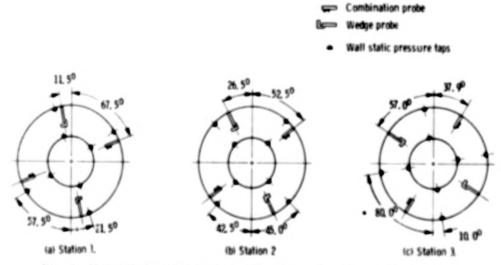


Figure 6. · Circumferential location of instrumentation at measuring stations (koking downstream),

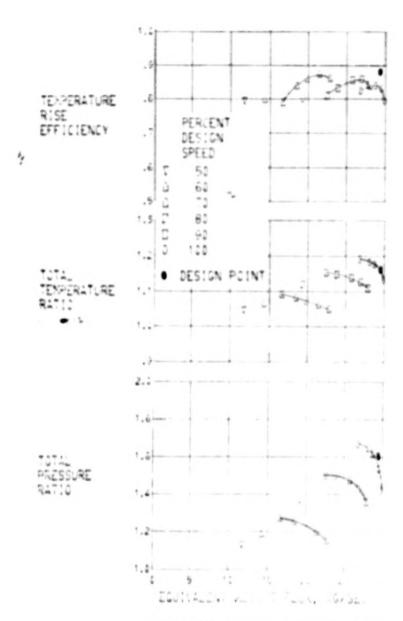


FIGURE 7. - OVERALL PERFORMANCE FOR ROTOR 20.

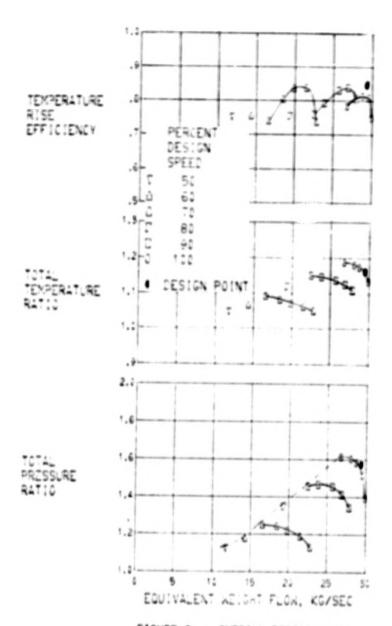


FIGURE 8. - OVERALL PERFORMANCE FOR STAGE 20-17.

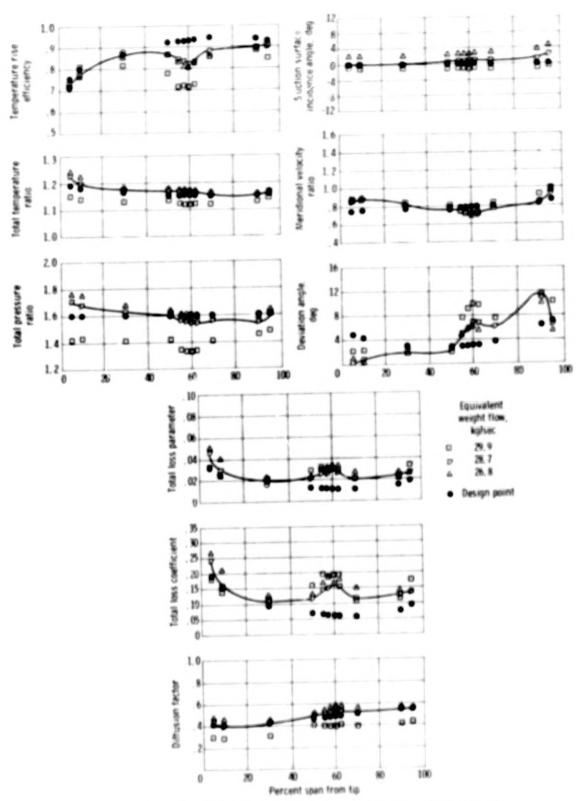


Figure 9. - Radial distribution of performance for rotor 30 at 100 percent of design speed.

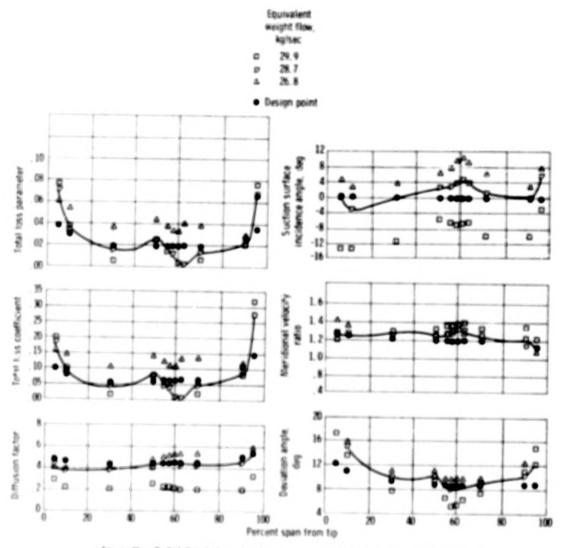
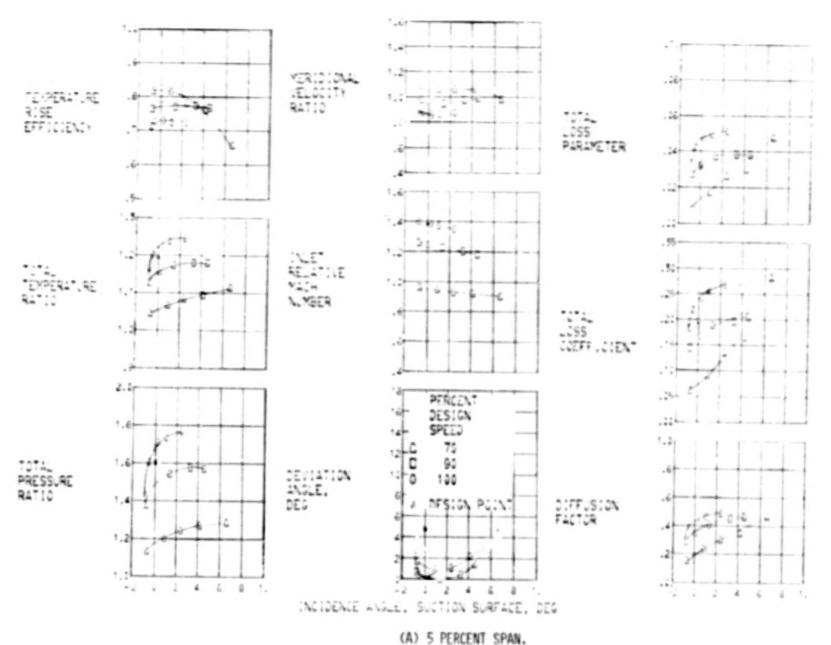


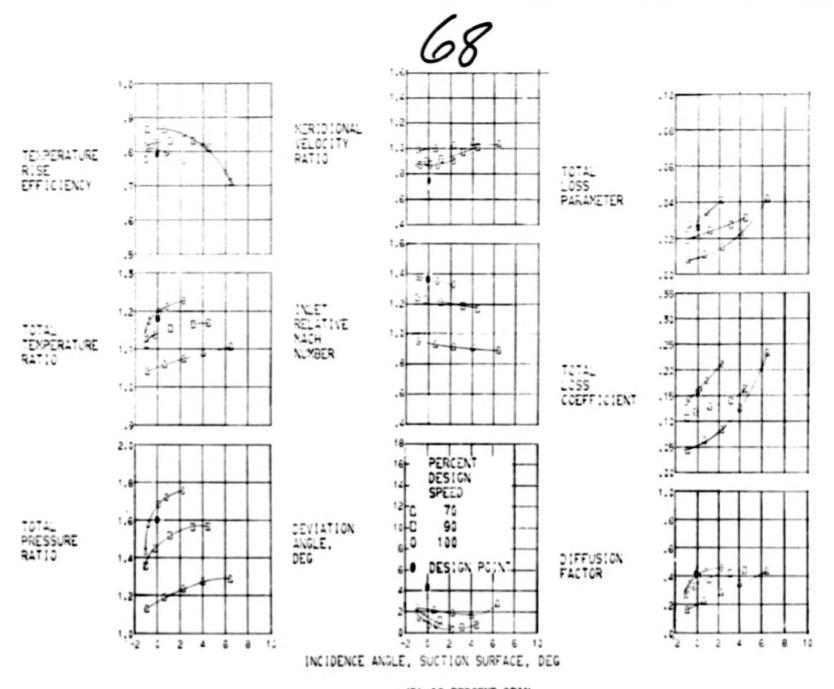
Figure 10. - Radial distribution of performance for stator 17 at 100 percent of design speed.



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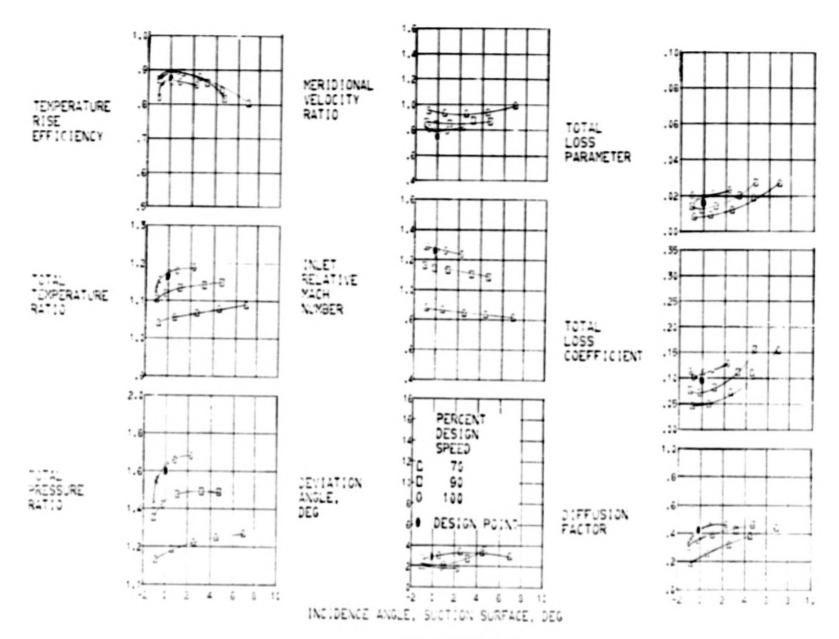
FIGURE 11. - BLADE ELEMENT PERFORMANCE FOR ROTOR 20.





(B) 10 PERCENT SPAN.

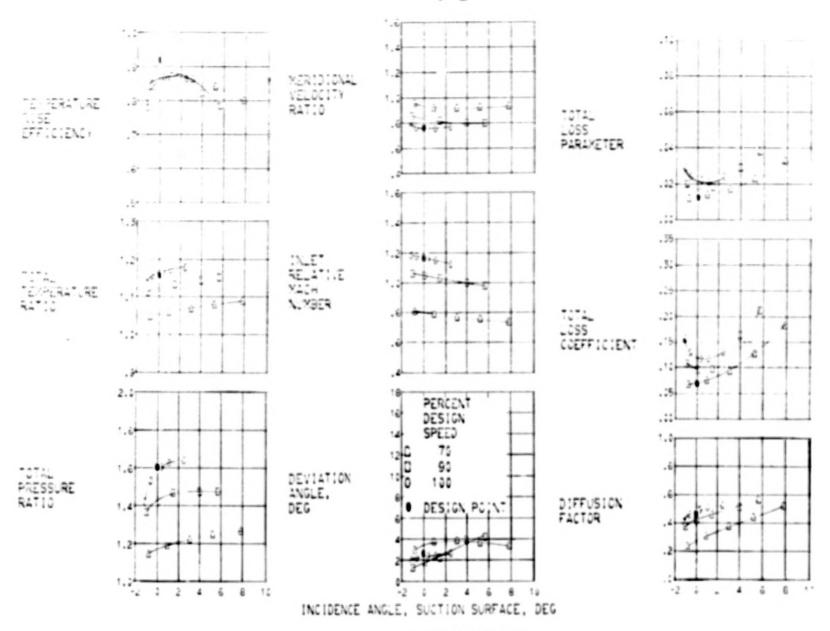
FIGURE 11. - CONTINUED.



(C) 30 PERCENT SPAN.

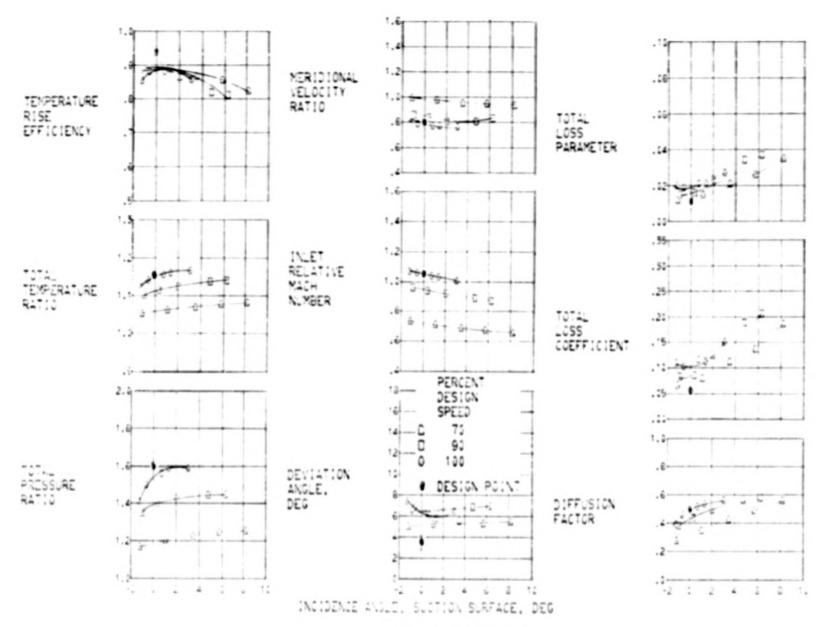
FIGURE 11. - CONTINUED.





(D) 50 PERCENT SPAN.

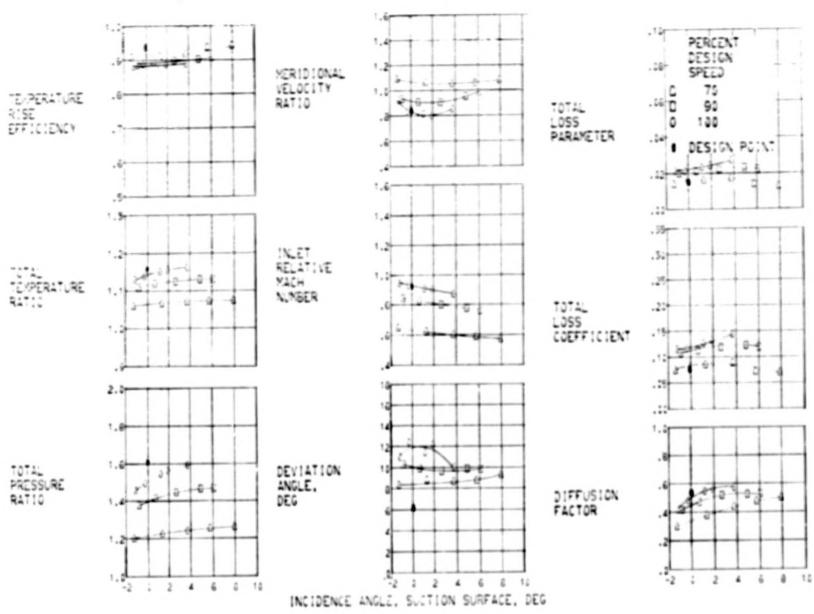
FIGURE 11. - CONTINUED.



(E) 70 PERCENT SPAN.

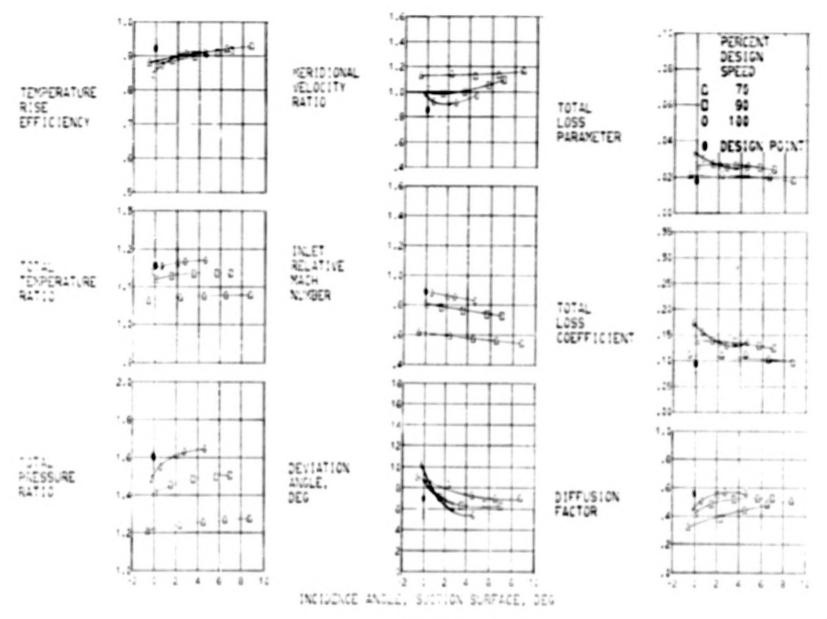
FIGURE 11. - CONTINUED.

7/



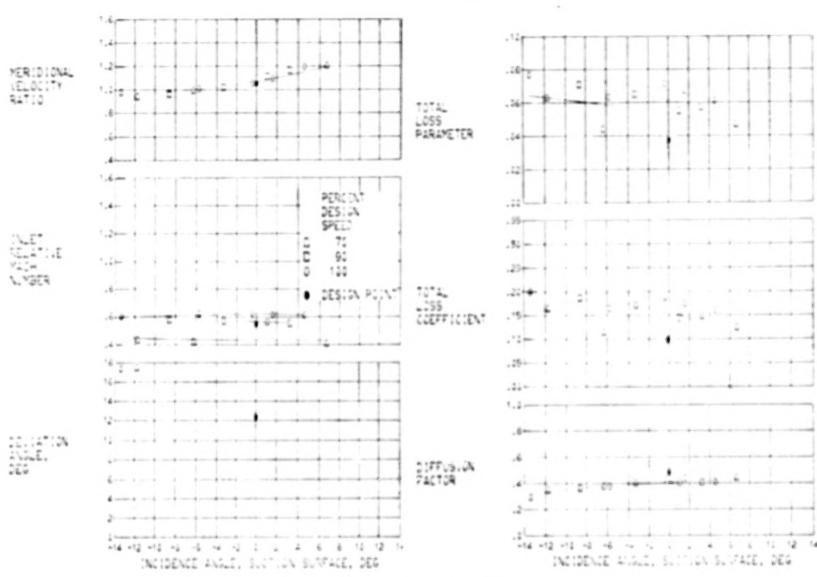
(F) 90 PERCENT SPAN.

FIGURE 11. - CONTINUED.



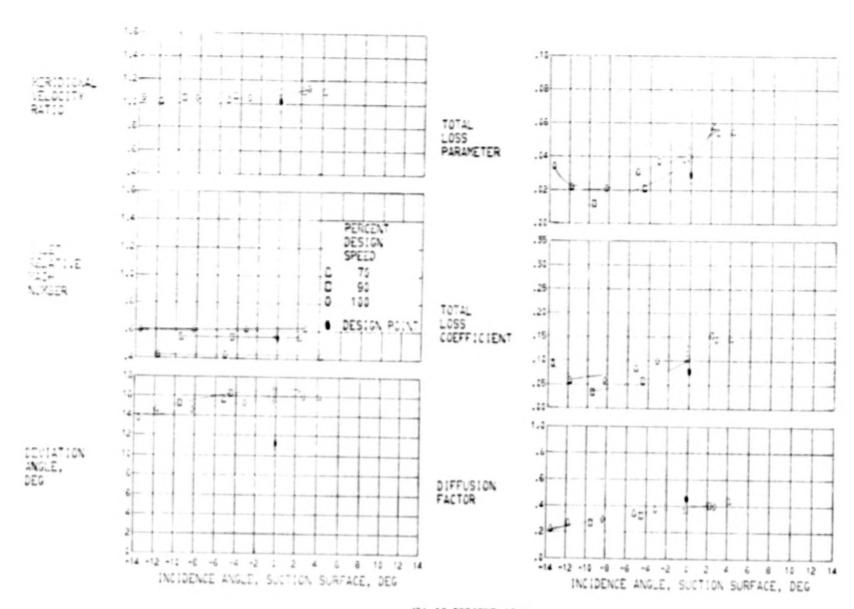
(G) 95 PERCENT SPAN.

FIGURE 11. - CONCLUDED.

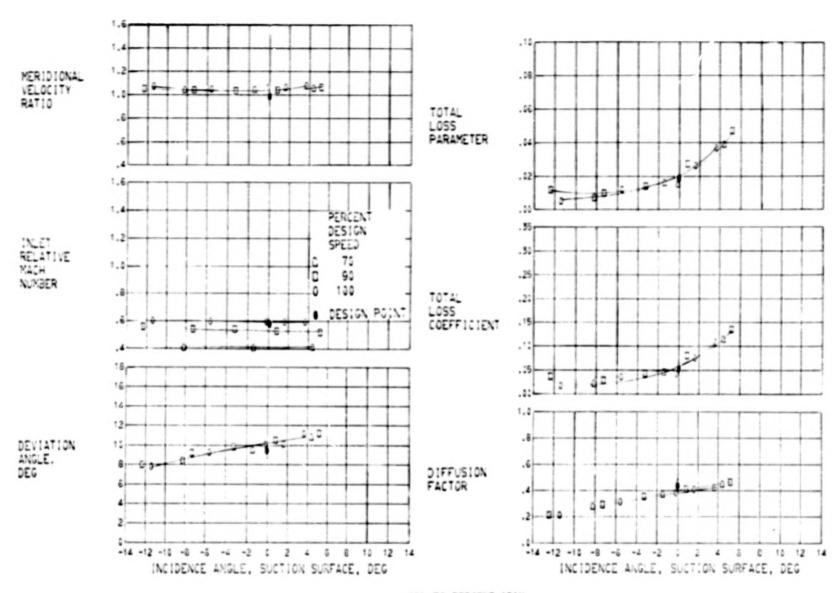


(A) 5 PERCENT SPAN.

FIGURE 12. - BLADE-ELEMENT PERFORMANCE FOR STATOR 17.

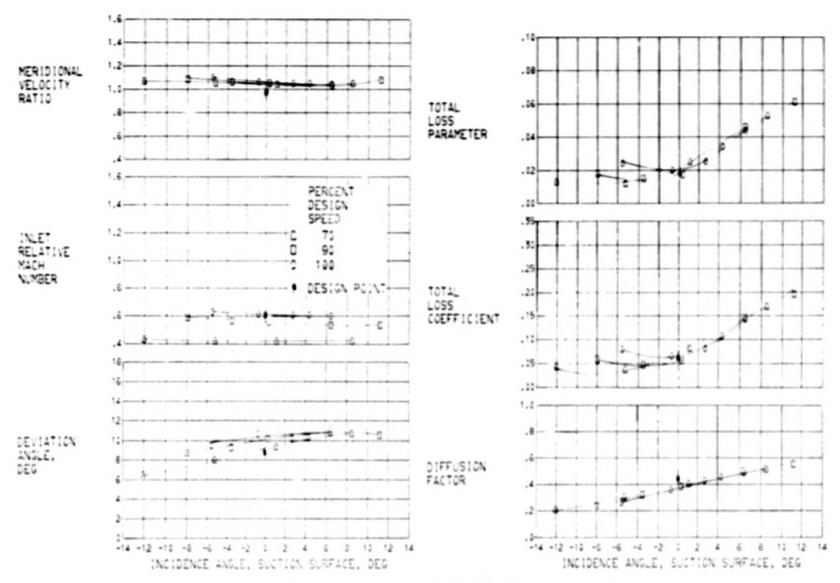


(B) 10 PERCENT SPAN.
FIGURE 12. - CONTINUED.



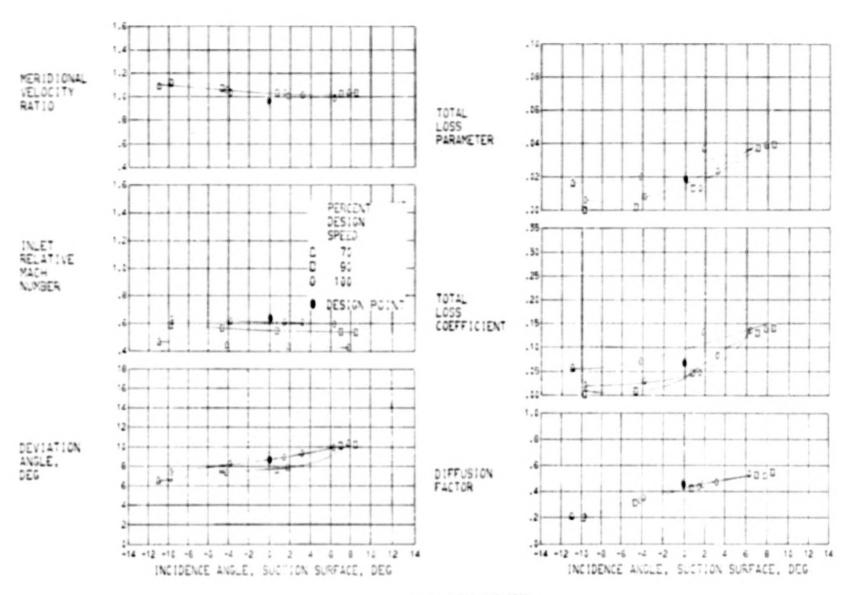
(C) 30 PERCENT SPAN.

FIGURE 12. - CONTINUED.



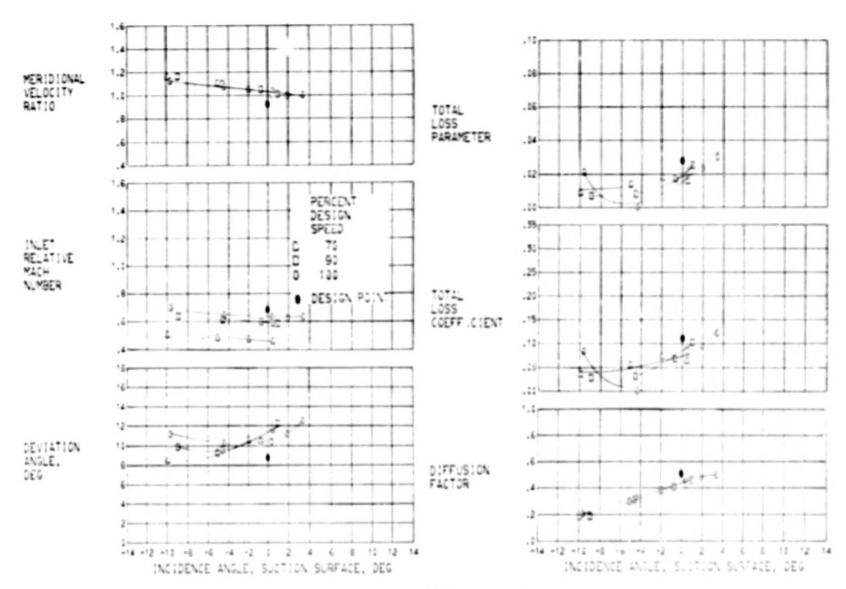
(D) 50 PERCENT SPAN.

FIGURE 12. - CONTINUED.



(E) 70 PERCENT SPAN.

FIGURE 12. - CONTINUED.

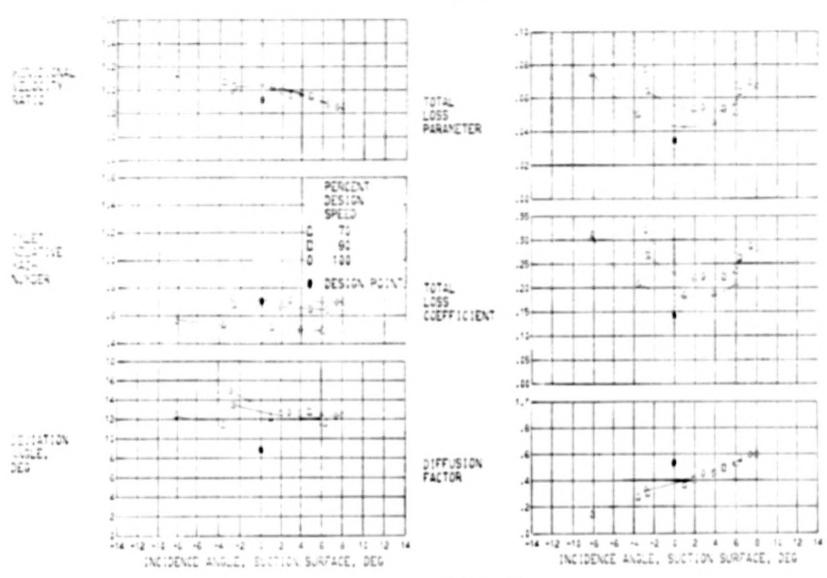


(F) 90 PERCENT SPAN.

FIGURE 12. - CONTINUED.

79

80



(G) 95 PERCENT SPAN.

FIGURE 12. - CONCLUDED.

A LOW MERIDIONAL VELOCITY RATIO  7. Activities Royce D. Moore, George W. Lewis, Jr., and Walter M. Osbora  9. Festiming Organization State and Address National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44125  12. Seaward Agency Sum and Address National Aeronautics and Space Administration Washington, D. C. 20546  13. Type of Report and Prood Course Technical Paper 14. Summoring Agency Sum a Address National Aeronautics and Space Administration Washington, D. C. 20546  15. Sequencetary Notes  16. Address This report presents the aerodynamic performance and design parameters of a transonic fan stage designed for a meridional velocity ratio of 0.8 across the tip of the stage, a pressure ratio of 1.57, a flow of 29.5 kilograms per second, and a tip speed of 426 meters per second.  Radial surveys were obtained over the stable sperating range from 50 to 100 percent of design speed. The measured, peak efficiency (0.81) of the stage occurred at a pressure ratio of 1.58 and a flow of 28.7 kilograms per second.  18. Destidution Statement Unclassified - unlimited STAR Category 07	1	Report No. 2	Government Accessor No		3 Ri-spent's Catal	ing %o		
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National Aeronautics and Space Administration  Lewis Research Center Cleveland, Ohio 44135  12 Second Agrees have and Antons National Aeronautics and Space Administration Washington, D. C. 20546  13 Superint Report and Report and Period Counted Technical Paper  14 Superioring Agrees Code  15 Superimentary Notes  16 Abstract This report presents the aerodynamic performance and design parameters of a transonic fan stage designed for a meridional velocity ratio of 0, 8 across the tip of the stage, a pressure ratio of 1, 57, a flow of 29, 5 kilograms per second, and a tip speed of 426 meters per second.  Radial surveys were obtained over the stable operating range from 50 to 100 percent of design speed. The measured, peak efficiency (0, 81) of the stage occurred at a pressure ratio of 1, 58 and a flow of 28, 7 kilograms per second.  17 Second Superiod by Authorist Compressors Turbomach Superiod by Authorist Compressors Turbomach Superiod of the report  18 Dechdodon Statement Unclassified - unlimited STAR Category 07	9	Performing Organization Name and Address						
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